

A LOAD FLOW AND ECONOMIC DISPATCH COMPUTER CODE
FOR THE TUCSON GAS AND ELECTRIC POWER SYSTEM

by

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ABSTRACT

A computer model of the Tucson Gas and Electric (TGE) power system and a computer code for the analysis of electrical power load flow and economic dispatch through the system was developed for use with the Digital Equipment Corporation System 10 (DEC-10) computer. The DEC-10 provides fast direct on-line response from remote terminals and user timesharing of its large memory storage capacity. The computer code was developed to demonstrate the cost advantages available through computerized control of electrical power distribution in large complex systems such as that owned by the TGE. Although preliminary data of distribution system parameters was provided by TGE, actual system cost and operating data were not available. System transmission lines, power source, bus, and load parameters can be varied to permit analysis of their effect on power flow and system operating costs. System size can be varied from a simple two or three bus system for instructional use to a large complex system such as that serving the Tucson metropolitan area with approximately 50 buses and 100 transmission lines. A unique Newton-Raphson computer code was developed for the complex system load flow calculations to obtain solutions with minimum computational iterations.

CHAPTER 1

INTRODUCTION

The use of digital computers in the analysis of electrical power system performance is well established (see, e.g., Happ, 1977; Sasson et al., 1971; Stott, 1974; Subramanian and Ramachandra Rao, 1969). However, little effort has been made to develop an interactive code to take advantage of current high speed, timesharing computers with large memory storage capabilities. This thesis presents such an interactive code for use with the Digital Equipment Corporation's System 10 (DEC-10) computer installed at The University of Arizona. The code was designed for the analysis of electrical power system performance through economic dispatch and load flow studies. Further, it was designed to give the power systems engineer maximum flexibility and control of computerized solution routines with minimum preparation and response times. In addition, through use of the DEC-10's remote station and timesharing capabilities the code can be used for instructional and demonstration purposes.

The computer code incorporates a unique algorithm for solution of the set of nonlinear load flow equations and uses an iterative Newton-Raphson solution method. Two

codes were developed. EDSP15 was designed for instructional and demonstration use on small systems with no more than 15 buses and 30 transmission lines. This code also includes a successive displacement or Gauss-Seidel iterative solution method for comparison with the more rapid, reliable quadratic convergence rate of the Newton-Raphson method. The other code, EDSP50, is for use with systems serving large metropolitan areas such as Tucson, Arizona and can accept up to 50 buses and 100 transmission lines.

To demonstrate use of the computer code, a model of the Tucson Gas and Electric Company (TGE) power distribution system was developed. Input data used by the code to describe the system physical characteristics were derived and typical operating conditions were analyzed. Unfortunately, cost comparisons with actual operating condition at TGE could not be accomplished since their actual operating and cost data were not available.

The characteristics, capabilities, and limitations of the DEC-10 computer necessary for use of the code are included. Sample problems are also included to familiarize the user with the DEC-10 and the code operation.

Background

The primary function of any electrical power system is to provide the power required by the various loads connected to the system. Simultaneously, the generated

real and reactive power, the bus voltages, and the voltage phase angles throughout the system must be kept within constraints imposed by equipment and system operating limits, while the load demands undergo large, and sometimes unpredictable, changes. Therefore, the most important or certainly the most frequently performed power system study is "load flow" where bus voltages and phase angles are calculated for various transmission network and load configurations.

Prior to the advent of large capacity digital computers, system load flow studies were performed by simulation techniques employing an analog A/C network analyzer. Ward and Hale (1956) provided one of the first practical automatic solution methods for use with the digital computer employing nodal admittance analysis and a Gauss-Seidel iterative process to solve the set of non-linear equations involved. Improvements in solution techniques developed rapidly during the late '50s and early '60s. Among the more significant developments were: Van Ness (1959) proposed the use of Newton's methods for a more reliable and faster solution convergence; Tinney and Hart (1967) and Tinney and Walker (1967) developed techniques to drastically reduce computation time and memory storage requirements in solutions of very large systems, i.e., in excess of 1000 buses. Other efforts have been directed toward further improvements in speed and reliability of

convergence, solution accuracy, reduction of memory storage requirements, and expansion of problem size through algorithms using diakoptics, tearing, and block-iteration techniques (see, e.g., Stott, 1974; Subramanian and Ramachandra Rao, 1969).

Solution of the load flow problem determines the real and reactive power flow, the bus voltages, and the voltage phase angles required to meet each bus or terminal condition, while economic dispatch is concerned with development of an optimum generation strategy to meet the load demands at a minimum or optimum system operating cost. Since there is an infinite number of generation profiles that could meet a specified load requirement, a method must be devised to find the least cost schedule while observing all the equipment and system constraints such as maximum generator or transformer ratings, bus voltage and system reactive power limits.

Prior to the 1930s, various methods were employed to divide the load among the available generation units for the minimum system operating cost. For example: the "Base Load" method loaded the most efficient unit to its maximum capacity first, then loaded the second most efficient unit to its capacity, etc., or the "Best Point Loading" method where units are successively loaded to their lowest heat rate point beginning with the most efficient unit and working down to the least efficient, etc. During the early

1930s, it was recognized that for the most economical operation, the incremental cost of all machines should be equal. In the early 40s, Steinberg and Smith (1943) published their classic book on economic loading of power plants that added understanding and impetus to the equal incremental method. In their approach, the generating unit's incremental cost characteristics were represented by straight line segments for easy applications. Also, George (1943) provided a breakthrough in system transmission loss calculations through the development of his loss formulas. By 1954, a transmission loss penalty computer was developed and used in conjunction with an incremental loading slide rule by American Electrical Power (AEP) to produce daily generation schedules. In 1955, an electronic differential analyzer was developed by Morrill and Blake (1955) for production of daily generation schedules. Early in the '60s, Carpentier (1962a, 1962b) provided a breakthrough in mathematical formulation of the optimum power flow problem using the Kuhn and Tucker (1951) theorems for nonlinear programming and a Gauss-Seidel solution procedure. Later, Dommel and Tinney (1968) supplied a significant advance in digital computer solution techniques by using Newton's methods for the load flow solutions and incorporating a steepest descent or gradient method for finding the optimum or most economical generation profile. They also employed the more lenient "penalty factors" instead of hard limits for equipment and

system constraints and thereby enhanced convergence probability. Current efforts are being extended to system security analysis, reactive power scheduling and allocation, pollution dispatching, maximum interchange, expansion planning, maintenance scheduling, substation switching, and on-line automatic dispatching and control (see, e.g., Sasson and Merrill, 1974).

The initial effort at The University of Arizona to develop an interactive computer code for the solution of economic dispatch problems was developed for use with the PDP-9 mini-computer by Martinez (1973). This code would accommodate a 15 bus power system and used the Gauss-Seidel iterative solution method. Later Stanley Beaver adapted it for use on the DEC-10. This thesis develops a new computer code to take advantage of the large core memory and disc storage capability of the DEC-10 and will accommodate power systems as large as 50 buses and 100 transmission lines. Further, the new code incorporates an iterative Newton-Raphson solution method to provide more rapid and reliable convergence of the solution.

CHAPTER 2

COMPUTER CONSIDERATIONS

The Digital Equipment Corporation System 10 (DEC-10) computer used by the EDSP codes is a third generation, high speed computer with a large capacity central (core) memory of 524K words. It has a model KL10 central processor (CPU) controlled by the timesharing, TOPS-10 operating system. The CPU uses a 36 bit word size and includes double precision arithmetic instructions. Under the TOPS-10 monitor, interactive service for up to 90 customers is provided simultaneously. Fast access disk storage of over one billion characters is available for temporary storage of user files. In addition, three types of magnetic tape can be used with the DEC-10; seven-track, nine-track, or DECTape. DECTape is ideally suited for permanent storage of source codes or low volume data files. Each DECTape reel will store 22 files or approximately 353K characters whichever occurs first. DEC Model VT05, Teleray, or Infoton terminals are available for video input/output display or DECwriter terminals are available for printed (hard copy) input/output products. Remote station operation is available at numerous locations throughout the campus or operation can be set up at any location off campus that has

normal telephone service. An acoustical coupler would be required to connect the terminal to any normal telephone instrument. Several telephone numbers are available for computer service on a 24 hour per day basis. An inter-computer link permits routing of output products to the high speed line printers, card or paper punch machines, or the Calcomp 12 inch plotter. Batch processing is also available for off-line execution of very large programs. Several text editing routines are available for direct input or modification of user files. The most popular and versatile is the SOS (Son of Stopgap) text editor.

Interactive Capabilities

The interactive capability of the code in conjunction with the DEC-10 offers a distinct advantage in reduced problem setup time, and while it is not necessary to maintain a constant dialogue with the computer, the system engineer is free to make decisions during the computational process and implement changes to optimize results without fear of computer hang-ups. Further, data and solution printouts can be controlled to meet specific needs. Data input and modification is straightforward and requires no card punching or formatting. During each run the EDSP code will prompt the user when action or data input is required. The specific prompting messages and the response required is outlined in Chapter 7.

Temporary Files

As stated above, disk storage is available for temporary data files so that subsequent runs of the EDSP code can be made without re-entering all input data. Although the temporary files can be created separately through use of the DEC-10 SOS text editor, the code automatically creates the temporary files as the data are being entered during program execution. Since disk storage is for common use by all users, large data files such as the Y and Z bus matrix, discussed in Chapter 3, should be deleted prior to "logging off" the terminal or they may be transferred to DECTape for permanent storage and recalled for use at a later date. The temporary files created during program execution are shown in Table 2.1.

Table 2.1 Temporary Computer Files

Type Data	File Name
Line Data	FOR20.DAT
Bus Data	FOR21.DAT
Generator Data	FOR22.DAT
Generator Constraints	FOR23.DAT
Y/Z Bus Matrix	FOR24.DAT
Problem Solutions ^a	SOL.DAT

^aTemporary file of the problem solutions is optional and must be requested during program execution.

User Limitations

Users are normally limited to 60 pages (30K words) of central (core) memory use and 500 blocks (61K words) of disk storage while "logged in" and 300 blocks (36.6K words) with "logging off." The difference between "logged on" and "logging off" limits is to permit expanded use of disk storage while programs are being run or edited. Increased core and disk limits are available for large problems such as the TGE system but operation may be restricted to other than peak student use periods. Memory storage requirements to run the computer code EDSP50 are 188 pages of central (core) memory and 540 blocks of disk memory. The core memory requirements vary with the number of buses in the system as shown in Figure 2.1.

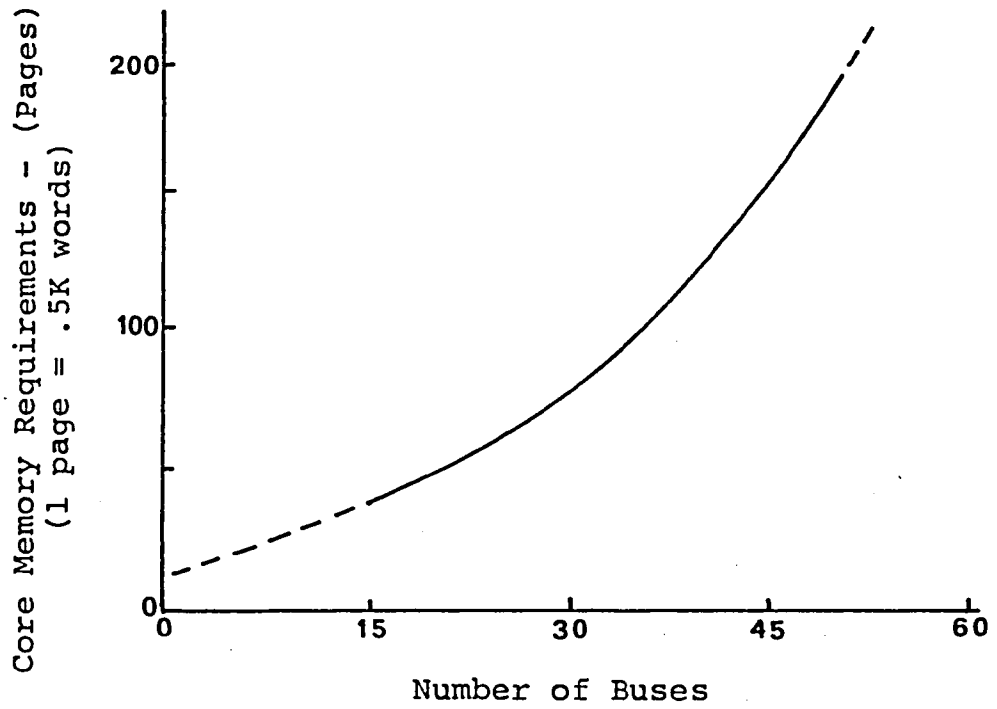


Figure 2.1 Computer Code Memory Requirements

CHAPTER 3

POWER SYSTEM MODEL

Most power systems consist of a generation capability, a distribution network which transports electrical power to the customer loads, and a monitoring and control system to operate the system under normal or emergency conditions. The objective of this chapter is to obtain a mathematical model of a power system for study of electrical power distribution and generation under normal operating conditions. Mathematical expressions are derived to describe the physical characteristics of the transmission line network, the bus or power load centers, the generator operating costs, and the system and equipment operating limits.

In developing the mathematical model, a nodal admittance form was selected since this form is more economical in the use of computer time and it requires less memory storage (see, e.g., Stagg and El-Abiad, 1968:258). In addition, the mathematical notation closely follows the transmission line network topography, making it easier to apply to computer programming techniques. Further, since only normal operating conditions are considered, a balanced

three phase power system with a constant 60Hz frequency is assumed.

Transmission Line Characteristics

In a normal balanced three-phase system, the transmission line characteristics of each phase are considered identical. Thus, the computer model represents a single phase of the three phase system, i.e., the positive sequence network. Each transmission line used in the system can be represented by the following four electrical parameters per unit length of line: series resistance (R_i), series reactance (X_i), shunt conductance (G_i), and shunt susceptance (B_i). In the metropolitan areas served, the transmission lines are usually less than 100 miles long and consequently are considered "electrically short." Thus, the distributed electrical parameters can be "lumped" into an equivalent π circuit as shown in Figure 3.1 (see, e.g., Elgerd, 1971:193). In this equivalent circuit, the series impedance (z_{ik}) is complex,

$$z_{ik}^{ser} = z_{ki}^{ser} = (R + jX)\ell \text{ ohms} \quad (3.1)$$

R = line resistance per unit length in ohms

X = line inductive reactance per unit length in ohms

ℓ = line length in feet, meters, or miles

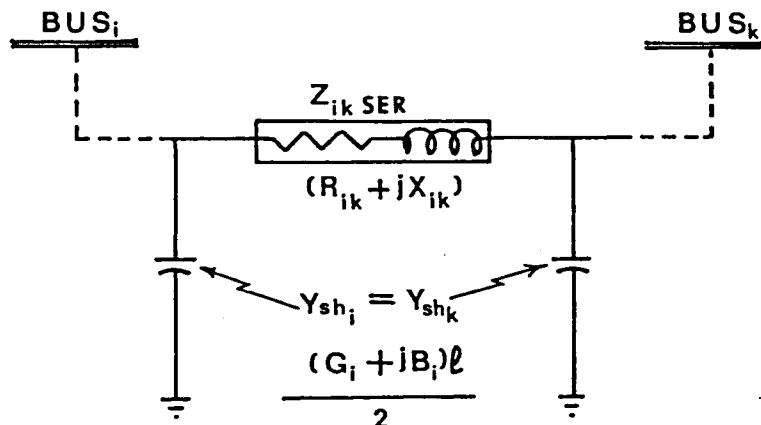


Figure 3.1 Transmission Line Equivalent Circuit

The equivalent shunt admittance is also complex and one-half of the total distributed admittance is applied to each leg of the equivalent π network.

$$Y_{shi} = Y_{shk} = \frac{(G + jB)l}{2} \text{ mhos} \quad (3.2)$$

G = line conductance per unit length in mhos

B = line susceptance per unit length in mhos

l = line length in feet, meters, or miles

As shown by Elgerd (1971:170), the series elements, of which the inductive reactance is often dominant, set the limit of the current flowing through the line and thereby determine the power transmittability or capacity of the transmission line. The series resistance is usually much smaller than the series reactance (see, e.g., Table 3.1) but

Table 3.1 Typical Transmission Line Parameters

Type Conductors	Shunt admittance (B+jG) mhos/1000'	Series Impedance (R+jX) ohms/1000'
Copper #4/0	0.0 + j0.0	0.0574 + j0.1282
Aluminum AA #477MCM	0.0 + j0.0	0.0409 + j0.1195
Aluminum ACSR #366MCM	0.0 + j0.0	0.0580 + j0.1196
Aluminum AA #750 UG	0.0 + j4.3731x10 ⁻⁵	0.0320 + j0.0380

is important in that it determines the system real losses. The shunt elements represent a "leakage" path for the line current between the phases and ground. These leakage currents are influenced by the geometry of the transmission line, the physical characteristics of the transmission cable, and are proportional to the line voltage. The shunt conductance G_i is extremely small and, if leakage occurs at all, it usually takes place along the insulator strings. It is strongly affected by the weather, atmospheric conditions, and the salt content in the air. It is customary to neglect this parameter under normal operating conditions. The shunt susceptance B_i is also negligible except for underground cables and overhead transmission lines where the line voltage exceeds 300KV and/or the line length exceeds 200 miles. Typical values for these parameters are shown in Table 3.1 for the type lines indicated. The EDSP

computer code requires these line parameters to be entered as "Line Data" in per unit values per unit length of transmission line. For example, consider the 4-bus power system shown in Figure 3.2. The typical line parameters were used as indicated and are shown in Table 3.2 in per unit values required by the code. The impedance base Z_b used for the system was 21.16 ohms, i.e., $Z_b = V_b^2 / S_b$. It should be noted that a "starting bus" or "ending bus" shown in Table 3.2 does not exist in an actual system. These terms are used for the expediency of describing components of current and power in particular transmission lines and should not be interpreted as limiting the actual flow of current or power to a particular direction. Also, the numbering of buses and transmission lines is completely arbitrary and used to facilitate network description only.

Transformers used to step-up or step-down the level of voltage between buses are included by the computer code as transmission lines. Since the transformer characteristics can be represented by an equivalent π network like the one shown in Figure 3.1 for transmission lines (Elgerd, 1971:126), the appropriate equivalent impedance and admittance values are included by the code as "Line Data" to represent these transformer parameters. Problem #2 in Appendix A includes an example of how transformers are represented in the system.

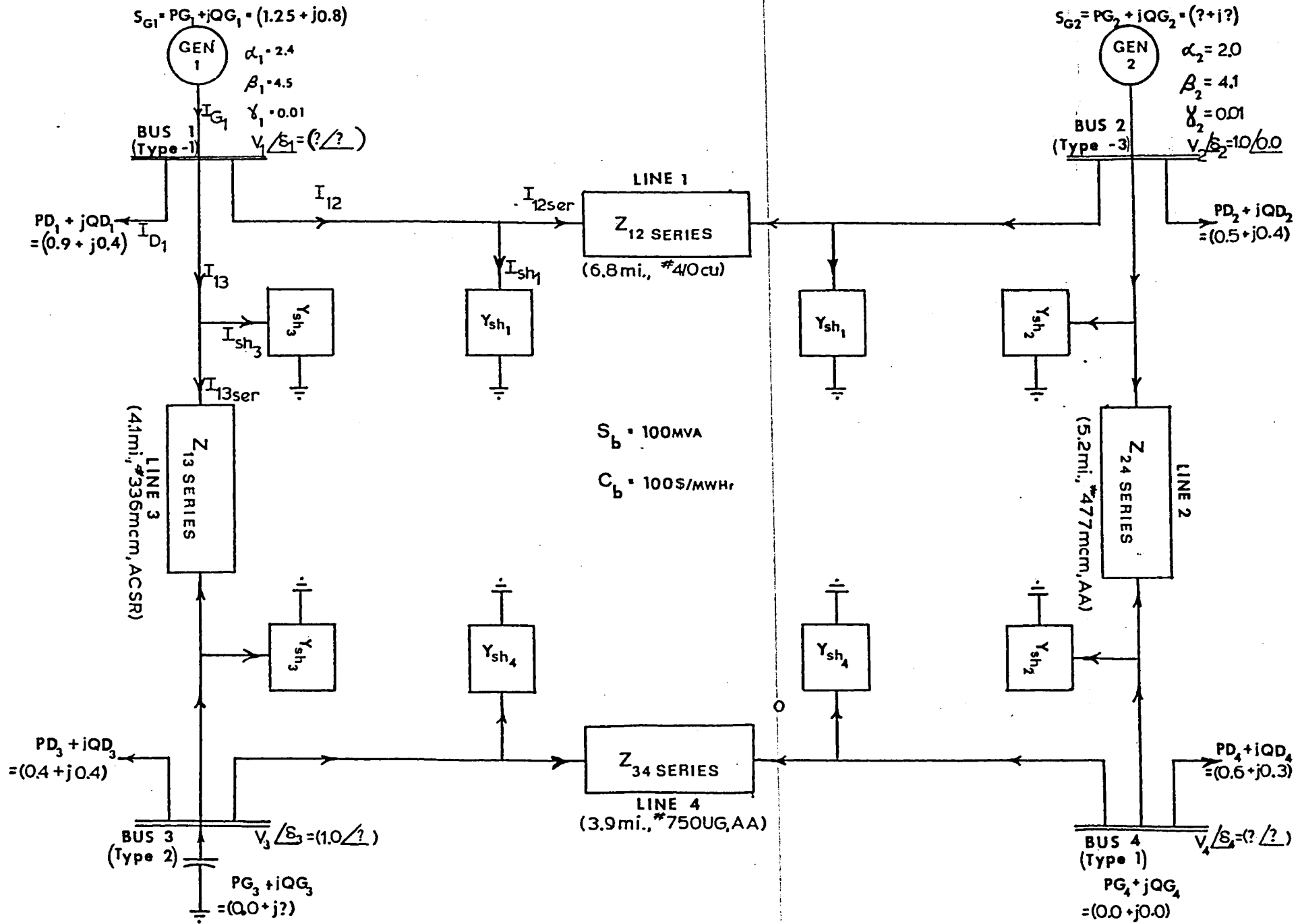


Figure 3.2 Typical 4-Bus Power System

Table 3.2 Line Data

Line No.	Starting Bus	Ending Bus	Length (1000')	Shunt Admittance (G+jB) per unit	Series Impedance (R+jX) per unit
1	1	2	35.904	0.0 + j0.0	$0.27127 \times 10^{-2} + j0.6059 \times 10^{-2}$
2	2	4	27.456	0.0 + j0.0	$0.19329 \times 10^{-2} + j0.5648 \times 10^{-2}$
3	1	3	21.648	0.0 + j0.0	$0.2741 \times 10^{-2} + j0.5652 \times 10^{-2}$
4	3	4	20.592	$0.0 + j9.2531 \times 10^{-4}$	$0.15123 \times 10^{-2} + j0.17958 \times 10^{-2}$

The Load Flow Problem

In the nodal admittance model used to represent the power system, nodes are buses or load centers to which the various loads and generators are connected. Transmission lines interconnect these nodes (buses) to transport power between buses as required. Power provided by the generators S_{Gi} and power consumed by the loads S_{Di} at bus i are complex. That is, they have the following real and reactive components: $S_{Gi} \equiv PG_i + jQG_i$ and $S_{Di} \equiv PD_i + jQD_i$. To establish a sign convention, power into a node was considered positive. Also, phasor quantities are represented by capital letters. Thus, the net injected complex power S_i available at bus i is defined as the difference between the generated power input and the power consumed by the loads.

$$S_i \equiv P_i + jQ_i \equiv (PG_i - PD_i) + j(QG_i - QD_i) \quad (3.3)$$

Any power shortage or excess at each bus must be transported by the interconnecting transmission lines. These line powers can be expressed in terms of the bus voltages and currents as follows. Using phasor notation, let V_i or $|V_i|e^{j\delta_i}$ represent the i th bus phase to ground voltage with the magnitude $|V_i|$ obtained with respect to the reference or ground node and the phase angle δ_i representing the angle between the reference "slack" bus voltage and the i th bus voltage. Also, let I_i or $|I_i|e^{j\psi_i}$ represent the net injected current (current into a bus is considered positive)

at bus i with ψ_i representing the angle between the reference "slack" bus voltage and the i th bus current.

Then the net complex bus power S_i at bus i is defined as:

$$\begin{aligned} S_i &\equiv P_i + jQ_i \equiv V_i I_i^* = |V_i| e^{j\delta_i} |I_i| e^{-j\psi_i} \\ &= |V_i| |I_i| e^{j\theta_i} \end{aligned} \quad (3.4)$$

with the complex power angle $\theta_i = (\delta_i - \psi_i)$. Also, in a nodal analysis, the currents entering and leaving the node must obey Kirchhoff's current law, that is, their algebraic sum must equal zero. As an example, consider bus 1 in Figure 3.2. It can be seen that the generated current I_{D1} that is not consumed in the load I_{D1} must flow through the transmission lines 1 and 3, or as stated above $I_{G1} - I_{D1} - I_{12} - I_{13} = 0$. Clearly, the net injected current at bus 1 is:

$$\begin{aligned} I_1 = I_{G1} - I_{D1} = I_{12} + I_{13} &= V_1 y_{sh1} + \frac{V_1 - V_2}{z_{12ser}} \\ &+ V_1 y_{sh3} + \frac{V_1 - V_3}{z_{13ser}} \end{aligned} \quad (3.5)$$

This equation can be rewritten in terms of the bus powers and voltages using (3.4).

$$\frac{S_1^*}{V_1^*} = V_1 (y_{sh1} + y_{sh3}) + (V_1 - V_2) y_{12} + (V_1 - V_3) y_{13} \quad (3.6)$$

where from Equation (3.1),

$$Y_{ik} = \frac{1}{z_{ikser}} = \frac{1}{R + jX} \text{ mhos} \quad (3.7)$$

Thus, the power flow equations for the 4-bus system in Figure 3.2 are:

$$S_1^* = P_1 - Q_1 = V_1^* [(y_{sh1} + y_{sh3} + y_{12} + y_{13})V_1 - y_{12}V_2 - y_{13}V_3] \quad (3.8)$$

$$S_2^* = P_2 - Q_2 = V_2^* [(-y_{12}V_1 + (y_{sh1} + y_{sh2} + y_{12} + y_{24})V_2 - y_{24}V_4] \quad (3.9)$$

$$S_3^* = P_3 - Q_3 = V_3^* [(-y_{13}V_1 + (y_{sh1} + y_{sh4} + y_{13} + y_{34})V_3 - y_{34}V_4] \quad (3.10)$$

$$S_4^* = P_4 - Q_4 = V_4^* [(-y_{24}V_2 - y_{34}V_3 + (y_{sh2} + y_{sh4} + y_{24} + y_{34})V_4] \quad (3.11)$$

Now the general form of the static load flow equation (SLFE) becomes apparent.

$$S_i^* = V_i^* I_i = V_i^* \sum_{k=1}^n V_k Y_{ik} \quad \begin{array}{l} i = 1, 2, \dots, n \\ n = \text{number of buses} \end{array} \quad (3.12)$$

In this equation $[Y]$ is defined as the complex admittance matrix representing the transmission line parameters in the distribution network. The diagonal elements $|Y_{ii}| e^{j\theta_{ii}}$ of this matrix are the sum of all shunt and series admittances terminating at bus i . The off-diagonal elements $|Y_{ik}| e^{j\theta_{ik}}$ are equal to the negative of the series admittance y_{ik} between buses i and k . The angle θ_{ik} is the admittance

angle of the resulting elements. As an example, the admittance matrix for the 4-bus system in Figure 3.2 would be:

$$[Y] = \begin{bmatrix}
 (y_{sh1} + y_{sh3} + y_{12} + y_{13}) & -y_{12} & -y_{13} & 0 \\
 -y_{21} & (y_{sh1} + y_{sh2} + y_{21} + y_{24}) & -0 & -y_{24} \\
 -y_{31} & 0 & (y_{sh1} + y_{sh3} + y_{31} + y_{34}) & -y_{34} \\
 0 & -y_{42} & -y_{43} & (y_{sh2} + y_{sh4} + y_{42} + y_{43})
 \end{bmatrix}$$

This is a symmetrical matrix of complex elements and in its general form is:

$$[Y] \equiv \begin{bmatrix}
 Y_{ii} & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & Y_{in} \\
 \cdot & \cdot & & & & & & & \cdot \\
 \cdot & \cdot & \cdot & & & & & & \cdot \\
 \cdot & & \cdot & & & & & & \cdot \\
 \cdot & & & \cdot & & & & & \cdot \\
 \cdot & & & & \cdot & & & & \cdot \\
 \cdot & & & & & \cdot & & & \cdot \\
 \cdot & & & & & & \cdot & & \cdot \\
 Y_{ni} & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & Y_{nn}
 \end{bmatrix} \quad \begin{array}{l}
 i=1,2,\dots,n \\
 k=1,2,\dots,n \\
 n=\text{number of buses}
 \end{array} \quad (3.13)$$

Equation (3.12) can be rewritten into two real equations as follows:

$$P_i = PG_i - PD_i = \sum_{k=1}^n |V_i V_k Y_{ik}| \cos(\theta_{ik} + \delta_k - \delta_i) \quad i=1,2,\dots,n \quad (3.14)$$

$$Q_i = QG_i - QD_i = -\sum_{k=1}^n |V_i V_k Y_{ik}| \sin(\theta_{ik} + \delta_k - \delta_i) \quad i=1,2,\dots,n \quad (3.15)$$

An examination of Equations (3.14) and (3.15) shows that only four of the eight variables PG , QG , PD , QD , V , δ , Y , and θ are known. That is, Y and θ are specified by the transmission network parameters and PD and QD are the known load requirements imposed on the system. Consequently, a method must be devised to reduce the number of unknowns to two per bus since there are only two independent equations in (3.14) and (3.15) per bus. The problem is resolved by classifying the buses into three types according to the function they serve in the system. The three classifications are: type 1--a load bus, type 2--a voltage control bus, and type 3 is the slack bus. These types are discussed below and allow two of the four unknowns at each bus to be fixed or specified according to the type bus.

The slack bus, as indicated earlier, is used as the voltage reference for the system. Therefore, there is only one slack bus per system and the voltage magnitude $|V_i|$ and phase angle δ_i at this bus can be set arbitrarily, usually at a per unit value of 1.0 and 0.0 respectively. Although the load requirements $PD_i + jQD_i$ are known throughout the system, the total generated power requirements can not

be specified because the total system losses (TPL) are unknown. That is, the total generated power must equal the sum of the various loads plus the total system losses.

$$\sum_{i=1}^n (PG_i + jQG_i) = \sum_{i=1}^n (PD_i + jQD_i) + TPL \quad i=1,2,\dots,n \quad (3.16)$$

Consequently, the real and reactive powers are the unknowns at the slack bus so that the extra power needed to compensate for the system losses can be included in the solution for generated power at this bus.

At other buses it is often desirable to control the voltage magnitude at a specific value for better control and service throughout the system. At these "voltage control" buses the generated real power PG_i and the voltage magnitude $|V_i|$ are specified while the phase angle δ_i and the required reactive power QG_i are the unknowns. In this case, the necessary reactive power to maintain the specified bus voltage may be supplied by a generator or a compensating capacitor bank connected to the bus as shown on bus 3 in Figure 3.2. Inductor banks are also used to consume excess reactive power such as often occurs on long distance very high voltage transmission lines. At the remaining "load" type buses, the generated real and reactive power is specified and the voltage magnitude and phase angles are the unknowns.

Solution of the load flow problem is now possible since with an n bus system there will be $2n$ unknowns and $2n$ real equations given in (3.14) and (3.15). Table 3.3 illustrates this by showing the "Bus Data" in per unit values for the 4-bus system shown in Figure 3.2. In the EDSP code, a negative number is used for the bus type to indicate those buses with generators attached. As shown, there are now 8 unknowns in the system of 8 independent real load flow equations. They are:

$$1.25 - 0.9 = |V_1^2 Y_{11}| \cos(\theta_{11}) \\ + |V_1 Y_{12}| \cos(\theta_{12} - \delta_1) + |V_1 Y_{13}| \cos(\theta_{13} + \delta_3 - \delta_1)$$

$$PG_2 - 0.5 = |V_1 Y_{21}| \cos(\theta_{21} + \delta_1) \\ + |Y_{22}| \cos(\theta_{22}) + |V_4 Y_{24}| \cos(\theta_{24} + \delta_4)$$

(3.17)

$$0.0 - 0.4 = |V_1 Y_{31}| \cos(\theta_{31} + \delta_1 - \delta_3) \\ + |Y_{33}| \cos(\theta_{33}) + |V_4 Y_{34}| \cos(\theta_{34} + \delta_4 - \delta_3)$$

$$0.0 - 0.6 = |V_4 Y_{42}| \cos(\theta_{42} - \delta_4) \\ + |V_4 Y_{43}| \cos(\theta_{43} + \delta_3 - \delta_4) + |V_4^2 Y_{44}| \cos(\theta_{44})$$

Table 3.3 Bus Data

Bus No.	Bus Type	PG	QG	PD	QD	V	S
1	-1	1.25	0.8	0.9	0.4	?	?
2	-3	?	?	0.5	0.4	1.0	0.0
3	2	0.0	?	0.4	0.4	1.0	?
4	1	0.0	0.0	0.6	0.3	?	?

$$0.8 - 0.4 = -|V_1^2 Y_{11}| \sin(\theta_{11})$$

$$- |V_1 Y_{12}| \sin(\theta_{12} - \delta_1) - |V_1 Y_{13}| \sin(\theta_{13} + \delta_3 - \delta_1)$$

$$QG_2 - 0.4 = -|V_1 Y_{21}| \sin(\theta_{21} + \delta_1)$$

$$- |Y_{22}| \sin(\theta_{22}) - |V_4 Y_{24}| \sin(\theta_{24} + \delta_4)$$

(3.18)

$$QG_3 - 0.4 = - |V_1 Y_{31}| \sin(\theta_{31} + \delta_1 - \delta_3)$$

$$- |Y_{33}| \sin(\theta_{33}) - |V_4 Y_{34}| \sin(\theta_{34} + \delta_4 - \delta_3)$$

$$0.0 - 0.3 = - |V_4 Y_{42}| \sin(\theta_{42} - \delta_4)$$

$$- |V_4 Y_{43}| \sin(\theta_{43} + \delta_3 - \delta_4) - |V_4^2 Y_{44}| \sin(\theta_{44})$$

Note that the $|Y|$ s and θ s are known quantities and the remaining 8 unknowns are: $|V_1|$, δ_1 , PG_2 , QG_2 , QG_3 , δ_3 , $|V_4|$, and δ_4 .

The Economic Dispatch Problem

Today fuel costs exceed 87 per cent of the total plant operating expense (see, e.g., Friedlander, 1977:48). Thus, for the solution of the economic dispatch problem (i.e., to determine the minimum cost power generation profile that satisfies the total system load), a relationship between the cost of fuel input and electrical power output is required. The plant input-output curves are used for this purpose. The curves define the heat input required to produce the net electrical power output, usually expressed in BTU per Kilowatt hour (see, e.g., Skrotzki and Vopat, 1960:612-617). These curves are not linear and are determined empirically. For steam power plants, they are usually obtained by steady state operation of the generator prime mover at "valve points," point just prior to the next steam control valve opening, from generator no-load up to the generator peak rated output. The fuel required at each valve point is multiplied by the fuel cost to obtain the generator cost curves. Starting fuel and boiler banking fuel is not included since these fuel expenditures are independent of system loads. Thus, the cost function C_i used for generator i is defined as the cost in dollars per

hour to produce its net electrical power output S_{Gi} , e.g., see Figure 3.3.

$$C_i \equiv C_i(PG_i) \quad \$/\text{Hr} \quad (3.19)$$

The cost function C_i is assumed to be a function of the real power output PG_i only since the real power is controlled by the prime mover torque (Elgerd, 1971:276). However, the generated reactive power QG_i does have an indirect influence on operating cost. That is, the reactive power is controlled by varying the generator field current thereby varying the bus voltages throughout the system. Since the transmission losses are a function of these bus voltage levels, the reactive power implicitly influences the system operating cost through its effect on system losses and their demand for increased real power output. It is recognized that the use of these "smooth" cost curves ignores the detrimental effects of operating the steam turbines between "valve points" where steam throttling losses are incurred. However, studies by Ringlee and Williams (1962) and Happ, Ille, and Reisinger (1962) indicate that a total system cost savings of only 0.1 to 0.2 per cent could be obtained by use of dispatching criteria that includes these valve throttling effects. Therefore, incorporation of these refinements was left for further study when actual operating and cost data become available for comparison.

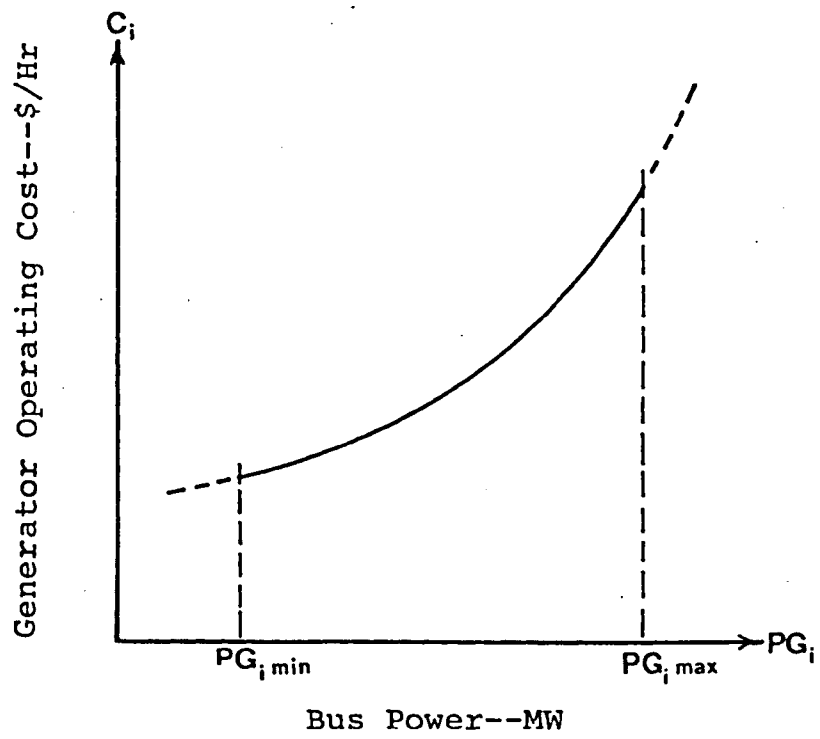


Figure 3.3 Typical Generator Cost Curve

The first derivative of the cost curve C_i is defined as the incremental generator operating cost IC_i in dollars per megawatt hour. The incremental cost curves represent the slope of the cost curve at any point and can be obtained by graphical differentiation or curve fitting techniques. They are then approximated by the following second order polynomial:

$$IC_i \equiv \frac{\partial C_i}{\partial PG_i} = \alpha_i + \beta_i (PG_i) + \gamma_i (PG_i)^2 \quad \$/MWhr \quad (3.20)$$

The EDSP computer code stores the incremental cost curve coefficients α_i , β_i , γ_i , normalized in per unit values for use in developing an equal incremental cost generation schedule for all generators. The normalized form is obtained by,

$$IC_i \text{ p.u.} = \frac{IC_i \times S_b}{C_b} \quad (3.21)$$

where S_b and C_b are the arbitrarily chosen system power base in MVA and the system operating cost base in dollars per hour, respectively. Figure 3.4 shows the cost and incremental cost curves in per unit values used for the 4-bus system in Figure 3.2 and Table 3.4 shows the cost curve coefficients and generator constraints used in per unit values.

Equipment such as generators, capacitor banks, transformers, etc., have operating limits beyond which

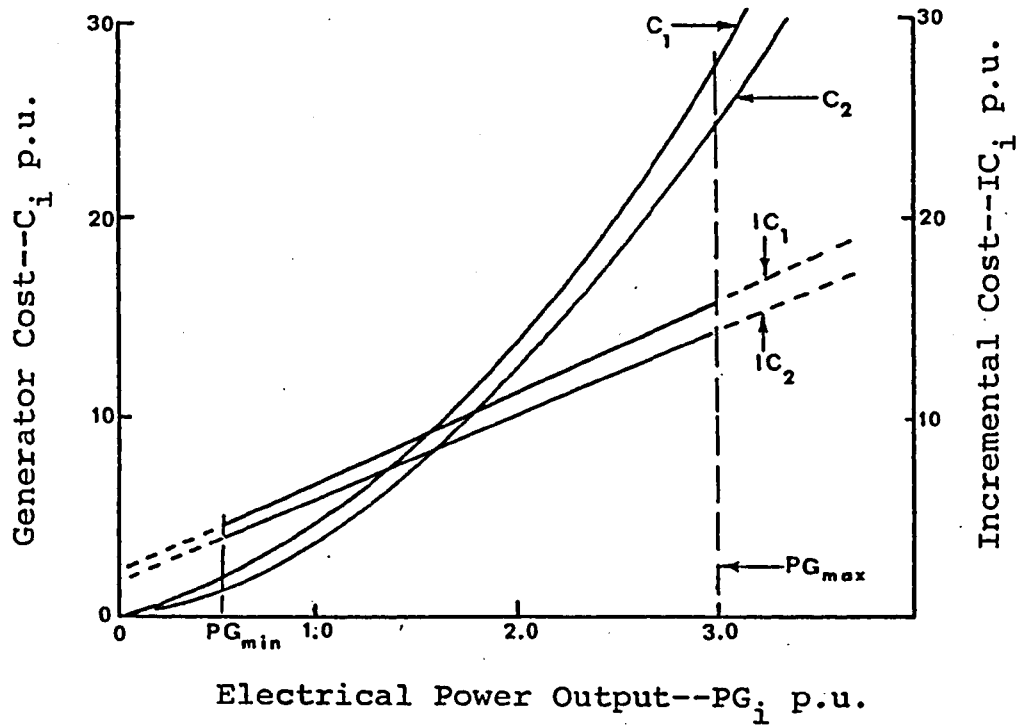


Figure 3.4 Cost and Incremental Cost Curves for Typical 4-Bus System

Table 3.4 Generator Data and Constraints

<u>Bus No.</u>	<u>Alpha</u>	<u>Beta</u>	<u>Gamma</u>
1	2.4	4.5	0.01
2	2.0	4.1	0.01

<u>Generator Constraints</u>				
<u>Bus No.</u>	<u>PG_i.max</u>	<u>PG_i.min</u>	<u>QG_i.max</u>	<u>QG_i.min</u>
1	3.0	0.5	--	--
2	3.0	0.5	--	--
3	--	--	2.0	0.0

operation of the equipment will result in reduced service life, unpredictable operation, or possible complete destruction of the equipment. The code accepts these operating limits as "Generator Constraints" during problem solution. When a limit is reached the variable is held at the limit value and the solution continued with remaining unconstrained generators sharing the remaining load. The following variables are kept within the limits indicated:

$$PG_{i,\min} \leq PG_i \leq PG_{i,\max} \quad (3.22)$$

$$QG_{i,\min} \leq QG_i \leq QG_{i,\max} \quad (3.23)$$

The EDSP computer code treats capacitor banks used for reactive power compensation to control the bus voltage magnitude at type 2 buses as generators without real power output capability. Also, when the capacitor bank or generator reactive power QG_i reaches its limit in an attempt to control the voltage at its specified level, the reactive power is held at its limit value and the bus is changed to a type 1 bus. From this point on the voltage is varied until a solution is obtained. During economic dispatch solutions where successive load flow solutions are performed, as discussed in Chapter 5, the bus type is returned to a type 2 between load flow solution iterations to permit "backoff" from the limits during power excursions in the economic dispatch calculations. An example of the input

generator incremental cost data and constraint required by the computer code is shown in Table 3.4 for the 4-bus system in Figure 3.2. All entries are in per unit values. Note that reactive power constraints are required for type 2 voltage control buses only.

With the incremental cost functions and operating constraints of each generator defined, the economic dispatch or optimum load flow problem is to develop a process whereby the total power generated within the system is allocated among the available generating units in such a way as to minimize the total system operating cost.

An iterative solution method is indicated since an infinite number of generator settings could satisfy the system load demands. Also, it is clear that the three functions: the generator cost curves (3.19) and (3.20), the system power balance equation (3.16), and the equipment constraints in equations (3.22) and (3.25) must be related in such a way that an optimum solution can be found.

The nonlinear programming theorem developed by Kuhn and Tucker (1951) and first applied to the economic dispatch problem by Carpentier (1962a, 1962b) provides the method for obtaining the optimum cost generation profile. To apply this theorem to the economic dispatch problem, we first define the total system operating cost as the sum of the individual cost functions.

$$C \equiv \sum_{i=1}^n C_i(PG_i) \quad i = 1, 2, \dots, n \quad (3.24)$$

Then using the power balance equation (3.16), we define the function $h(PG_i)$ as the system real power balance,

$$h(PG_1, PG_2, \dots, PG_n) \equiv \sum_{i=1}^n (PG_i - PD_i) - TPL = 0 \quad i=1, 2, \dots, n \quad (3.25)$$

Now Equations (3.24) and (3.25) are combined to form an augmented cost function defined as,

$$C^* \equiv \sum_{i=1}^n C_i - \lambda \left(\sum_{i=1}^n PG_i - \sum_{i=1}^n PD_i - TPL \right) \quad i=1, 2, \dots, n \quad (3.26)$$

The partial derivative of C^* with respect to PG provides the optimum dispatch equation,

$$\frac{\partial C^*}{\partial PG_i} = \frac{\partial \sum_{i=1}^n C_i}{\partial PG_i} - \lambda \left(\frac{\partial \sum_{i=1}^n (PG_i - PD_i)}{\partial PG_i} - \frac{\partial TPL}{\partial PG_i} \right) = 0 \quad (3.27)$$

In this equation the partial derivative of the total transmission losses TPL with respect to PG_i is defined as the "Incremental Transmission Loss" ITL_i associated with the generating unit i . Elgerd (1971:296-299) has developed the following good approximation of ITL in terms of the variables already obtained by the load flow solution:

$$\frac{\partial TPL}{\partial PG_i} \equiv ITL_i \equiv 2 \sum_{k=1}^n (P_k \alpha_{ik} - Q_k \beta_{ik}) \quad i=1, 2, \dots, n \quad (3.28)$$

where the terms α_{ik} and β_{ik} are defined as follows:

$$\alpha_{ik} \equiv \frac{r_{ik}}{|V_i V_k|} \cos(\delta_i - \delta_k) \quad (3.29)$$

$$\beta_{ik} \equiv \frac{r_{ik}}{|V_i V_k|} \sin(\delta_i - \delta_k) \quad (3.30)$$

and r_{ik} is the real part of the inverse Y admittance matrix element.

$$r_{ik} \equiv \text{Re: } (|Y_{ik}| \angle \theta_{ik})^{-1} \quad (3.31)$$

When the differentiation indicated by (3.27) is performed, an expression is obtained for the incremental operating cost of each generating unit in terms of the transmission losses associated with the distribution of its power output.

$$IC_i = \lambda(1-ITL_i) \quad i=1,2,\dots,n \quad (3.32)$$

Thus, as shown by Elgerd (1971:294), the concept of scheduling power production by equal incremental cost of each generating unit can now be modified to account for the losses incurred by dispatching it through the transmission network to the load. Figure 3.5 gives a graphic representation of how Equation (3.32) obtains the optimum incremental cost profile using the family of individual generator incremental cost curves. It can be seen that an iterative process where the value of λ is varied until the

power balance equation (3.25) is satisfied will produce the optimum incremental cost schedule for each generator.

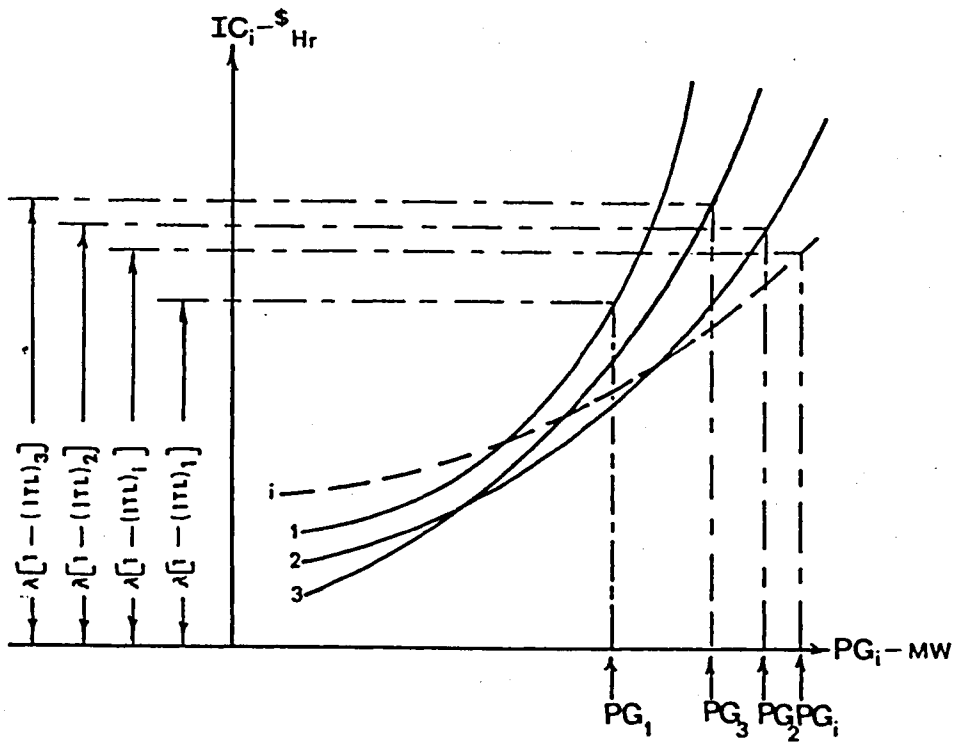


Figure 3.5 Graphical Economic Dispatch Solution

CHAPTER 4

LOAD FLOW ANALYSIS

The objective of the load flow study is to determine the bus voltages and phase angles associated with a selected schedule of power generation that meets the given set of load demands. With the voltages known, the line flows and system power losses can be calculated directly. Since the losses are not known, a priori, an iterative solution method with the nonlinear load flow equations (3.14) and (3.15) is indicated. In this chapter the iterative Newton-Raphson solution method used will be developed to assist the system engineer in the analysis of problem areas in power system load flow studies.

The main difficulty with successive displacement or Gauss-Seidel solution methods are their inability to solve some types of problems, such as those involving negative reactances that may arise in the equivalent circuits for 3-winding transformers or problems in which high and low impedance branches terminate at the same bus. The Newton-Raphson solution method was selected for use in the computer code because, as outlined by Tinney and Hart (1967:1450), it is not affected by these and most other ill-conditioned situations. Also, the Newton-Raphson method

provides a more rapid convergence rate, usually not more than 3 to 5 iterations, and the number of iterations is relatively independent of the problem size. However, this method is extremely sensitive to the initial starting conditions (see, e.g., Gross and Luini, 1971:41-48).

Fortunately, in power system problems, the use of a flat voltage profile, $V_i/\delta_i = 1.0/0.0$ per unit, as the initial starting point is sufficiently near the final solution point to preclude a false solution or divergence.

The iterative Newton-Raphson solution method used is summarized as follows:

Given the set of n nonlinear equations,

$$f_i(x_1, x_2, \dots, x_n) = 0 \quad i=1, 2, \dots, n \quad (4.1)$$

and let,

$$\bar{f} \equiv \begin{bmatrix} f_1 \\ \vdots \\ f_n \end{bmatrix}, \quad \bar{x} \equiv \begin{bmatrix} x_1 \\ \vdots \\ x_n \end{bmatrix}, \quad \overline{\Delta x} \equiv \begin{bmatrix} \Delta x_1 \\ \vdots \\ \Delta x_n \end{bmatrix}$$

In order to solve this set of n nonlinear simultaneous equations we make an initial estimate of \bar{x} . Call the estimated value $\bar{x}^{(0)}$, then let $\Delta x_1^{(0)}, \dots, \Delta x_n^{(0)}$ be the difference between $x_i^{(0)}$ and the exact value x_i , i.e., $x_i^{(0)} + \Delta x_i^{(0)} = x_i$. If the estimated value $x_i^{(0)}$ is close to the exact value x_i , then the differential df_i is:

$$df_i = \sum_{j=1}^n \left. \frac{\partial f_i}{\partial x_j} \right|_{\bar{x}^{(0)}} \overline{\Delta x}_j^{(0)} = f_i(\bar{x}) - f_i(\bar{x}^{(0)}) \quad i=1,2,\dots,n \quad (4.2)$$

and if,

$$d\bar{f} \equiv \begin{bmatrix} f_1(\bar{x}) - f_1(\bar{x}^{(0)}) \\ \vdots \\ f_n(\bar{x}) - f_n(\bar{x}^{(0)}) \end{bmatrix},$$

then

$$d\bar{f} = [J](\overline{\Delta x}^{(0)}) = \bar{f}(\bar{x}) - \bar{f}(\bar{x}^{(0)})$$

where $[J]$ is a matrix with elements $J_{ij} = \left. \frac{\partial f_i}{\partial x_j} \right|_{\bar{x}^{(0)}}$ $i,j=1,2,\dots,n$. Solving for $\overline{\Delta x}^{(0)}$ and recognizing from (4.1) that $\bar{f}(\bar{x}) = 0$, we obtain the general Newton-Raphson form:

$$\overline{\Delta x}^{(0)} = -[J]^{-1} \bar{f}(\bar{x}^{(0)}) \quad (4.3)$$

Thus, we may determine \bar{x} approximately by,

$$\bar{x}^{(1)} = \bar{x}^{(0)} + \overline{\Delta x}^{(0)}$$

where $\bar{x}^{(1)}$ may not be exactly equal to \bar{x} since the Taylor expansion of $d\bar{f}$ in (4.2) only retains the first order terms. However, $\bar{x}^{(1)}$ is a better approximation of \bar{x} than the initial estimate $\bar{x}^{(0)}$, and so the process is repeated to obtain an even better approximation, $\bar{x}^{(2)}$. The iterative procedure is continued until $\overline{\Delta x}^{(p)}$ is equal to or less than some acceptable solution tolerance. In the EDSP computer

codes, this solution tolerance (TOL) is preset at 0.0001, but can be changed by the user during program execution.

To apply Newton's method to the load flow problem, let two functions $g_i(P, V, \delta)$ and $h_i(Q, V, \delta)$ be defined so that they approach zero as the estimated values of real and reactive power approach the exact values.

$$g_i(P, V, \delta) = P_i^{\text{exact}} - P_i^{\text{estimated}} \rightarrow 0 \quad (4.4)$$

$$h_i(Q, V, \delta) = Q_i^{\text{exact}} - Q_i^{\text{estimated}} \rightarrow 0 \quad (4.5)$$

If the load flow equations (3.14) and (3.15) are substituted into (4.4) and (4.5) for the estimated values of P_i and Q_i , expressions in terms of the four variables P, Q, V, δ , are obtained.

$$g_i = P_i^{\text{exact}} - \sum_{k=1}^n |V_i V_k Y_{ik}| \cos(\theta_{ik} + \delta_k - \delta_i) \quad i=1, 2, \dots, n \quad (4.6)$$

$$h_i = Q_i^{\text{exact}} + \sum_{k=1}^n |V_i V_k Y_{ik}| \sin(\theta_{ik} + \delta_k - \delta_i) \quad i=1, 2, \dots, n \quad (4.7)$$

Now if the estimated value g_i^P is close to the final solution, the differential dg_i is:

$$\begin{aligned} dg_i &= g_i^{\text{exact}} - g_i^P \\ &= \frac{\partial g_i^P}{\partial P_i} dP_i + \sum_{k=1}^n \frac{\partial g_i^P}{\partial \delta_k} d\delta_k + \sum_{k=1}^n \frac{\partial g_i^P}{\partial V_k} dV_k \end{aligned} \quad (4.8)$$

$i=1, 2, \dots, n$

n =number of buses

However, from (4.4) g_i^{exact} is equal to zero, therefore the estimated value g_i^P is equal to,

$$g_i^P = - \frac{\partial g_i^P}{\partial P_i} dP_i - \sum_{k=1}^n \frac{\partial g_i^P}{\partial \delta_k} d\delta_k - \sum_{k=1}^n \frac{\partial g_i^P}{\partial V_k} dV_k \quad (4.9)$$

and similarly,

$$h_i^P = - \frac{\partial h_i^P}{\partial P_i} dP_i - \sum_{k=1}^n \frac{\partial h_i^P}{\partial \delta_k} d\delta_k - \sum_{k=1}^n \frac{\partial h_i^P}{\partial V_k} dV_k \quad (4.10)$$

Thus, in Newton-Raphson form the solution is:

$$(\Delta \bar{g}_i^P) = - [J(\bar{g}_i^P)]^{-1} f(\bar{g}_i^P) \quad (4.11)$$

and

$$(\Delta \bar{h}_i^P) = - [J(\bar{h}_i^P)]^{-1} f(\bar{h}_i^P) \quad (4.12)$$

Where $[J]$ is the jacobian matrix of $f(\bar{g}_i^P)$ and $f(\bar{h}_i^P)$ respectively. The next estimate of the independent variables, P , Q , V , and δ is obtained by solving (4.11) and (4.12) for Δg_i^P and Δh_i^P respectively and adding them to the original estimated values,

$$g_i^{P+1} = g_i^P + \Delta g_i^P \quad (4.13)$$

and

$$h_i^{P+1} = h_i^P + \Delta h_i^P \quad (4.14)$$

The solution continues until the changes in P , Q , V , δ are less than or equal to the acceptable solution tolerance, i.e., TOL.

In Chapter 3 it was established that the unknown variables depend on the bus type. Consequently, the solution matrix will be modified based on the type buses in the system. That is, the elements of the jacobian will be 0, -1, or the partial derivative of the function g_i or h_i depending on the bus type.

Consider the following example based on the 4-bus system shown in Figure 3.2. The bus types and corresponding unknown variables are shown in Table 4.1. In the solution method, the unknown variables V_1 , δ_1 , P_2 , Q_2 , Q_3 , δ_3 , and V_4 are given initial estimated values and then Equations (4.11) and (4.12) are solved for ΔP , ΔQ , ΔV , $\Delta\delta$. The first iteration is shown in (4.15) and is solved for the changes in P , Q , V , δ .

Table 4.1 Bus Characteristics

Bus type	PG_i	QG_i	V_i	δ_i
Load (Type 1)	Specified	Specified	?	?
Control (Type 2)	Specified	?	Specified	?
Slack (Type 3)	?	?	Specified	Specified

$$\begin{bmatrix} g_1 \\ g_2 \\ g_3 \\ g_4 \\ \dots \\ h_1 \\ h_2 \\ h_3 \\ h_4 \end{bmatrix} = \begin{bmatrix} \frac{\partial g_1}{\partial \delta_1} & 0 & \frac{\partial g_1}{\partial \delta_3} & \frac{\partial g_1}{\partial \delta_4} & \frac{\partial g_1}{\partial V_1} & 0 & 0 & \frac{\partial g_1}{\partial V_4} \\ \frac{\partial g_2}{\partial \delta_1} & -1 & \frac{\partial g_2}{\partial \delta_3} & \frac{\partial g_2}{\partial \delta_4} & \frac{\partial g_2}{\partial V_1} & 0 & 0 & \frac{\partial g_2}{\partial V_4} \\ \frac{\partial g_3}{\partial \delta_1} & 0 & \frac{\partial g_3}{\partial \delta_3} & \frac{\partial g_3}{\partial \delta_4} & \frac{\partial g_3}{\partial V_1} & 0 & 0 & \frac{\partial g_3}{\partial V_4} \\ \frac{\partial g_4}{\partial \delta_1} & 0 & \frac{\partial g_4}{\partial \delta_3} & \frac{\partial g_4}{\partial \delta_4} & \frac{\partial g_4}{\partial V_1} & 0 & 0 & \frac{\partial g_4}{\partial V_4} \\ \dots & \dots & \dots & \dots & \dots & \dots & \dots & \dots \\ \frac{\partial h_1}{\partial \delta_1} & 0 & \frac{\partial h_1}{\partial \delta_3} & \frac{\partial h_1}{\partial \delta_4} & \frac{\partial h_1}{\partial V_1} & 0 & 0 & \frac{\partial h_1}{\partial V_4} \\ \frac{\partial h_2}{\partial \delta_1} & 0 & \frac{\partial h_2}{\partial \delta_3} & \frac{\partial h_2}{\partial \delta_4} & \frac{\partial h_2}{\partial V_1} & -1 & 0 & \frac{\partial h_2}{\partial V_4} \\ \frac{\partial h_3}{\partial \delta_1} & 0 & \frac{\partial h_3}{\partial \delta_3} & \frac{\partial h_3}{\partial \delta_4} & \frac{\partial h_3}{\partial V_1} & 0 & -1 & \frac{\partial h_3}{\partial V_4} \\ \frac{\partial h_4}{\partial \delta_1} & 0 & \frac{\partial h_4}{\partial \delta_3} & \frac{\partial h_4}{\partial \delta_4} & \frac{\partial h_4}{\partial V_1} & 0 & 0 & \frac{\partial h_4}{\partial V_4} \end{bmatrix} \begin{bmatrix} \Delta \delta_1 \\ \Delta P_2 \\ \Delta \delta_3 \\ \Delta \delta_4 \\ \dots \\ \Delta V_1 \\ \Delta Q_2 \\ \Delta Q_3 \\ \Delta V_4 \end{bmatrix}$$

(4.15)

To solve for the new estimated values of P , Q , V , and δ , the jacobian matrix must be inverted. That is,

$$\bar{g}_i^{p+1} = \bar{g}_i^p - [J(g_i^p)]^{-1} \bar{f}(\bar{g}_i^p)$$

$$\bar{h}_i^{p+1} = \bar{h}_i^p - [J(h_i^p)]^{-1} \bar{f}(\bar{h}_i^p)$$

(4.17)

The jacobian matrix is partitioned with the elements of the partitioned sub-matrices defined as follows:

$$[J] = \begin{bmatrix} A_1 & | & A_2 \\ \hline A_3 & | & A_4 \end{bmatrix} \quad (4.18)$$

$$[A_1] \equiv \left[\begin{array}{l} \text{On Diagonal Elements (i=k)} \\ \\ \text{Bus Types 1 and 2} \\ \\ J_{ii} = \sum_{\substack{k=1 \\ k \neq i}}^n |V_i V_k Y_{ik}| \sin(\theta_{ik} + \delta_k - \delta_i) \quad i=1,2,\dots,n \\ \\ \text{Bus Type 3} \\ \\ J_{ii} = -1 \\ \\ \text{Off Diagonal Elements (i \neq k)} \\ \\ \text{Bus Types 1 and 2} \\ \\ J_{ik} = -|V_i V_k Y_{ik}| \sin(\theta_{ik} + \delta_k - \delta_i) \quad i=1,2,\dots,n \\ \\ \text{Bus Type 3} \\ \\ J_{ik} = 0 \end{array} \right] \quad (4.19)$$

$$\begin{aligned}
 & \text{On Diagonal Elements (i=k)} \\
 & \text{Bus Type 1} \\
 & J_{ii} = 2|V_i Y_{ik}| \cos(\theta_{ii}) \\
 & + \sum_{\substack{k=1 \\ k \neq i}}^n |V_k Y_{ik}| \cos(\theta_{ik} + \delta_k - \delta_i) \quad i=1,2,\dots,n \\
 & \text{Bus Types 2 and 3} \\
 & J_{ii} = 0 \\
 & \text{Off Diagonal Elements (i \neq k)} \\
 & \text{Bus Type 1} \\
 & J_{ik} = |V_i Y_{ik}| \cos(\theta_{ik} + \delta_k - \delta_i) \\
 & \text{Bus Types 2 and 3} \\
 & J_{ik} = 0
 \end{aligned}$$

(4.20)

$$\begin{array}{l}
 \text{On Diagonal Elements (i=k)} \\
 \text{Bus Types 1 and 2} \\
 J_{ii} = \sum_{\substack{k=1 \\ k \neq i}}^n |V_i V_k Y_{ik}| \cos(\theta_{ik} + \delta_k - \delta_i) \quad i=1,2,\dots,n \\
 \text{Bus Type 3} \\
 J_{ii} = 0 \\
 \text{Off Diagonal Elements (i \neq k)} \\
 \text{Bus Types 1 and 2} \\
 J_{ik} = -|V_i V_k Y_{ik}| \cos(\theta_{ik} + \delta_k - \delta_i) \quad i=1,2,\dots,n \\
 \text{Bus Type 3} \\
 J_{ik} = 0
 \end{array}$$

(4.21)

$[A_3] \equiv$

$$\begin{aligned}
 & \text{On Diagonal Elements (i=k)} \\
 & \text{Bus Type 1} \\
 & J_{ii} = -2|V_i Y_{ii}| \sin(\theta_{ii}) \\
 & - \sum_{\substack{k=1 \\ k \neq i}}^n |V_k Y_{ik}| \sin(\theta_{ik} + \delta_k - \delta_i) \quad i=1,2,\dots,n \\
 & \text{Bus Types 2 and 3} \\
 & J_{ii} = -1 \\
 [A_4] = & \\
 & \text{Off Diagonal Elements (i \neq k)} \\
 & \text{Bus Type 1} \\
 & J_{ik} = -|V_i Y_{ik}| \sin(\theta_{ik} + \delta_k - \delta_i) \\
 & \text{Bus Types 2 and 3} \\
 & J_{ik} = 0
 \end{aligned} \tag{4.22}$$

The inverse of the partitioned jacobian is obtained as follows:

$$[J]^{-1} = \begin{bmatrix} B_1 & & & B_2 \\ & \vdots & & \vdots \\ & & \vdots & \\ & & & B_4 \\ B_3 & & & \vdots \end{bmatrix} \tag{4.23}$$

where the partitioned sub-matrices are obtained using (4.19) to (4.22) as outlined by Stagg and El-Abiad (1968: 19).

$$B_1 = (A_1 - A_2 A_4^{-1} A_3)^{-1}$$

$$B_2 = -B_1 A_2 A_4^{-1}$$

$$B_3 = -A_4^{-1} A_3 B_1$$

$$B_4 = A_4^{-1} - A_4^{-1} A_3 B_2$$

This allows Equation (4.15) to be solved for the right hand column vector and then with (4.16) and (4.17) obtain the first order approximation of the solution. Further iterations will improve the approximations until the solution is obtained within the desired accuracy tolerance.

Solution Method and Flow Chart

The overall strategy of the solution method can be summarized as follows:

1. All system parameters are input, generator constraints established, and convergence criteria specified. These include the transmission line data, bus data, generator data and limits, solution tolerance and maximum number of iterations desired, and the initial estimated values for the unknowns.
2. The system transmission network admittance matrix [Y] is calculated. This calculation need be performed only once for each network configuration. The results are stored in the temporary SOS file

FOR24.DAT for subsequent studies using the same distribution network.

3. Using the initial voltage and phase angle estimates at each bus, calculate the resulting net real and reactive power at each bus using the load flow equations (3.14) and (3.15).
4. Test for convergence. The specified values of real and reactive power are compared with the values calculated in 3 above using Equations (4.4) and (4.5). When the difference becomes less than the desired solution tolerance "TOL" the final solution has been attained and the power balance equation (3.16) has been satisfied.
5. If the desired tolerance is exceeded at any bus, the solution continues using Equations (4.16) and (4.17) to determine the new estimated values of the unknown variables P , Q , V , and δ . The new estimated values of reactive power at type 2 buses are then checked against the limits designated. If any limit is exceeded the limit values are substituted and the solution continued changing the type 2 bus into a type 1 bus so that convergence can be attained.
6. Steps 3 through 5 are repeated using the new estimated values of P , Q , V , and δ after each iteration until the solution is obtained or the maximum number of iterations has been reached.

7. When a final solution is reached, the power flow in each transmission line is calculated where,

$$P_{ik} = |V_i^2 Y_{ik}| \cos(\theta_{ik}) - |V_i V_k Y_{ik}| \cos(\delta_i - \delta_k - \theta_{ik}) - |V_i V_k Y_{shi}| \cos(\theta_{shi}) \quad (4.24)$$

$$Q_{ik} = -|V_i^2 Y_{ik}| \sin(\theta_{ik}) - |V_i V_k Y_{ik}| \sin(\delta_i - \delta_k - \theta_{ik}) + |V_i V_k Y_{shi}| \sin(\theta_{shi}) \quad (4.25)$$

8. Calculate the total system load and transmission losses as follows:

$$\text{Total system load TPD} = \sum_{i=1}^n PD_i \quad i=1,2,\dots,n \quad (4.26)$$

$$\text{Total system losses TPL} = \sum_{i=1}^n P_i \quad i=1,2,\dots,n \quad (4.27)$$

9. Print desired output.

Sample problems are included in Appendix A showing input/output options and format. Figure 4.1 contains a flow chart showing the principal steps and sequence of each step in the load flow solution.

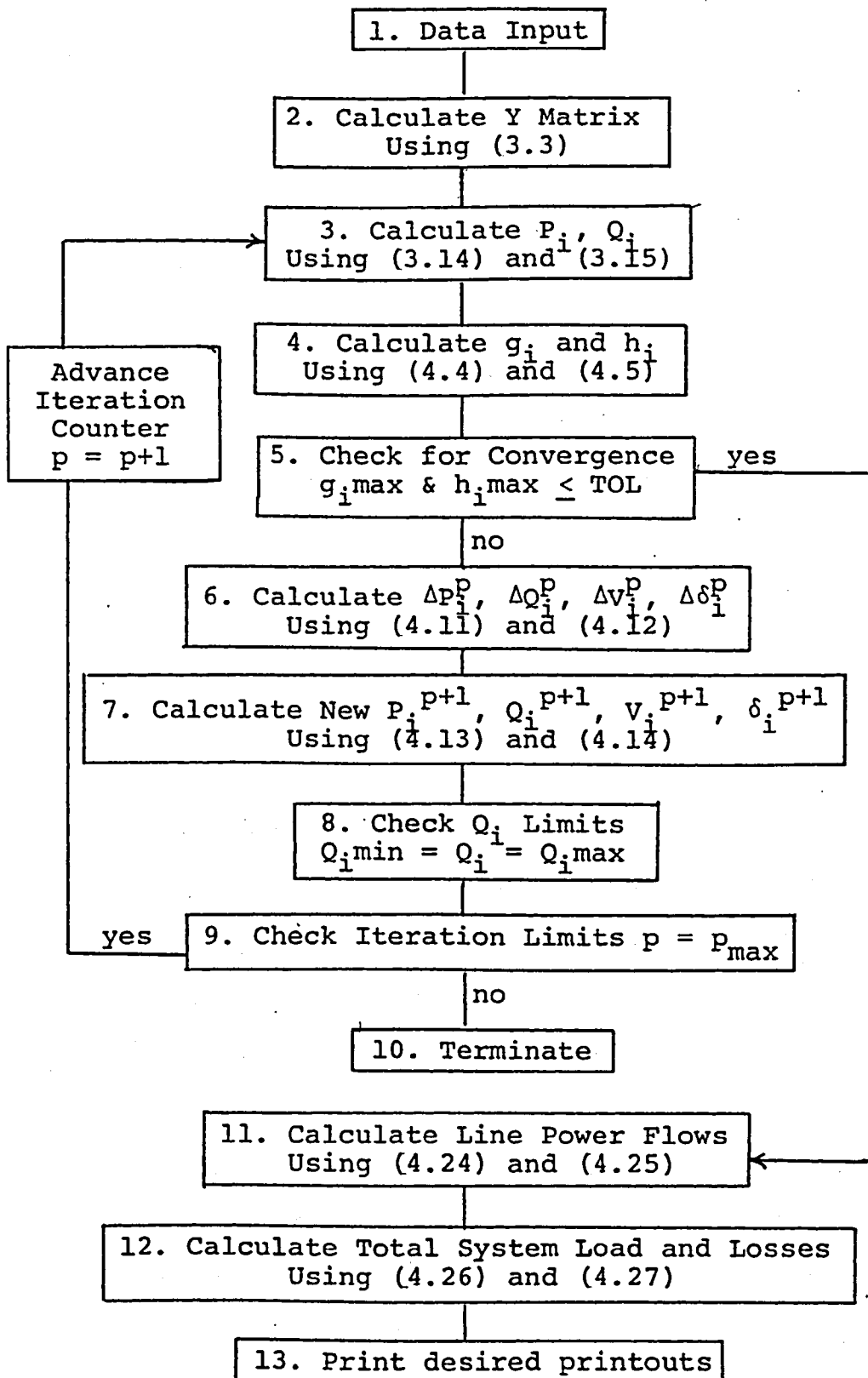


Figure 4.1 Load Flow Solution Flow Chart

CHAPTER 5

ECONOMIC DISPATCH ANALYSIS

In the previous chapter a method was developed for determining the power distribution throughout the system when the system engineer specified two of the four variables at each bus, i.e., Table 4.1. In this load flow solution, the specified variables were selected arbitrarily by the system engineer as an "educated guess." To obtain the optimum or most economical power generation profile, the total system power generation requirement, as calculated by the load flow solution, is re-scheduled among the available generating units using the incremental production cost characteristics of each generator in such a way as to minimize the total system operating cost in dollars per hour \$/Hr. In Chapter 3 it was shown that the optimum generation profile is obtained by an iterative process varying the Lagrangian multiplier λ in Equation (3.32) and using the incremental cost IC_i of each generator in Equation (3.20) to obtain the real power generated PG_i by each generating unit. λ is varied until the sum of the individual power generation PG_i satisfies the total system requirement, Equation (3.25), within an acceptable tolerance $ESP1$. This process is constrained by the operating limits

of each generator. That is, if a generator output limit is reached, its output is fixed at the limit value and the remaining unconstrained generators will share the balance of the system load on an equal incremental cost basis. The final solution is obtained when successive solutions for each generator output PG_i vary less than the specified tolerance $ESP2$. The solution tolerances $ESP1$ and $ESP2$ are preset in the code to 0.001 but may be changed by the user.

Solution Method and Flow Chart

The steps used by the EDSP computer code to obtain the economic dispatch solution are as follows:

1. Input all data required for the load flow solution and add the normalized incremental cost curve coefficients for each generator and the individual generator power output limits.
2. Calculate the system transmission network admittance matrix $[Y]$. If a load flow analysis was previously performed, this admittance matrix will already be calculated and stored as "Y Bus Matrix." For the economic dispatch solution, the Y admittance matrix is inverted to obtain the "Z Bus Matrix." The Z Bus Matrix is also stored for subsequent runs and the real part of each element is used to determine r_{ik} in calculating the ITL_i s.

3. Perform the load flow solution to obtain all bus parameters P_i , Q_i , V_i , and δ_i .
4. Calculate the individual incremental transmission losses ITL_i using the variables obtained from the load flow solution.
5. Select a starting value for lambda. The computer code arbitrarily sets the initial value of λ equal to the smallest incremental cost curve coefficient α .
6. Using the incremental cost curves, obtain the incremental cost and real power output of each generating unit corresponding to the selected value of λ .
7. Check that the real power output of each generator is within limits, i.e., $PG_{imin} \leq PG_i \leq PG_{imax}$.
8. Using Equation (3.25), check to see if the system real power balance is satisfied within the designated tolerance ESP1. If Equation (3.25) is not satisfied, the value of λ is adjusted and steps 6 and 7 repeated until a balance is obtained or the maximum number of iterations designated is reached.
9. Solution convergence has occurred when two successive power generation profiles vary less than the tolerance designated, i.e., ESP2.

$$PG_i^{p+1} - PG_i^p \leq ESP2 \quad i=1,2,\dots,n \quad (5.1)$$

If Equations (5.1) is not satisfied, the solution returns to step 3 for another load flow solution and rerun of steps 3 through 8 until the real power output at each generator varies less than ESP_2 between iterations or the maximum number of iterations designated has been reached.

10. Calculate the individual transmission line power flow, the total system load and transmission losses, the individual generator operating costs and the total system operating cost using Equations (4.24) through (4.27), (3.20), and (3.24) respectively.

Figure 5.1 is a flow chart showing the principal steps in the economic dispatch solution method.

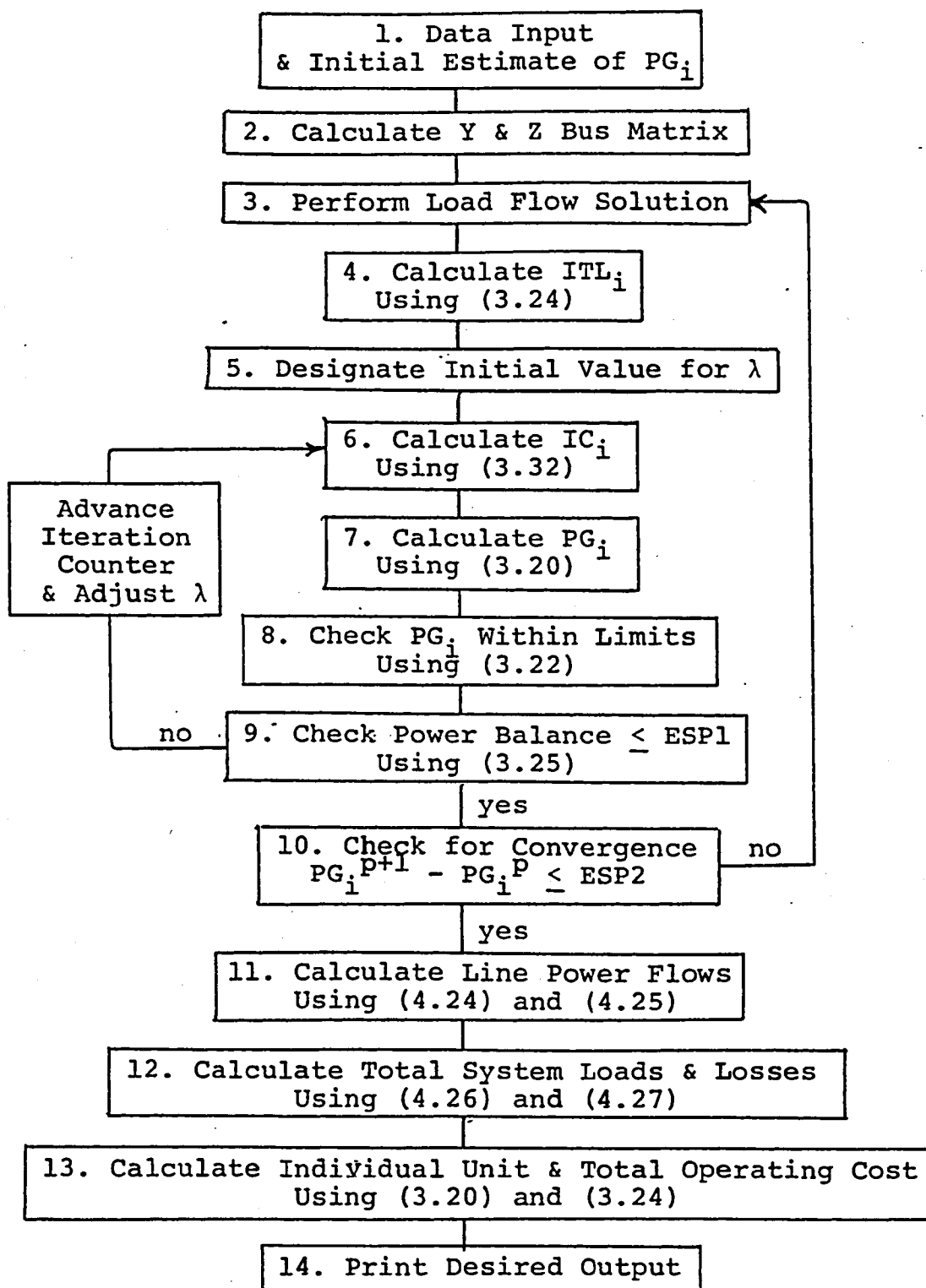


Figure 5.1 Economic Dispatch Solution Flow Chart

CHAPTER 6

TGE POWER SYSTEM

The parameters representing a power system transmission line network, bus or load center characteristics, and generator output cost curves have been derived. The computer code for load flow and economic dispatch solution methods has been developed. In this chapter the computer model will be applied to an actual power system, i.e., the TGE power system. The entire TGE system is described in terms of the parameters defined and computerized solutions of typical load flow and economic dispatch problems are obtained. The computer outputs of solution data for the sample problems are shown in Appendix A.

A single line schematic of the TGE system is shown in Figure 6.1. The network is divided into districts or load centers encircling the city of Tucson, Arizona and interconnected by 138KV high voltage transmission lines, i.e., North Loop, Northeast Loop, East Loop, Vail Loop, Ft. Huachuca Sub-station, South Loop, Tucson Loop, and the DeMoss Petrie and Irvington Generating Stations. The system is represented by 48 buses and 59 transmission lines with the control center and main generating plant located at the Irvington area. This generating station also

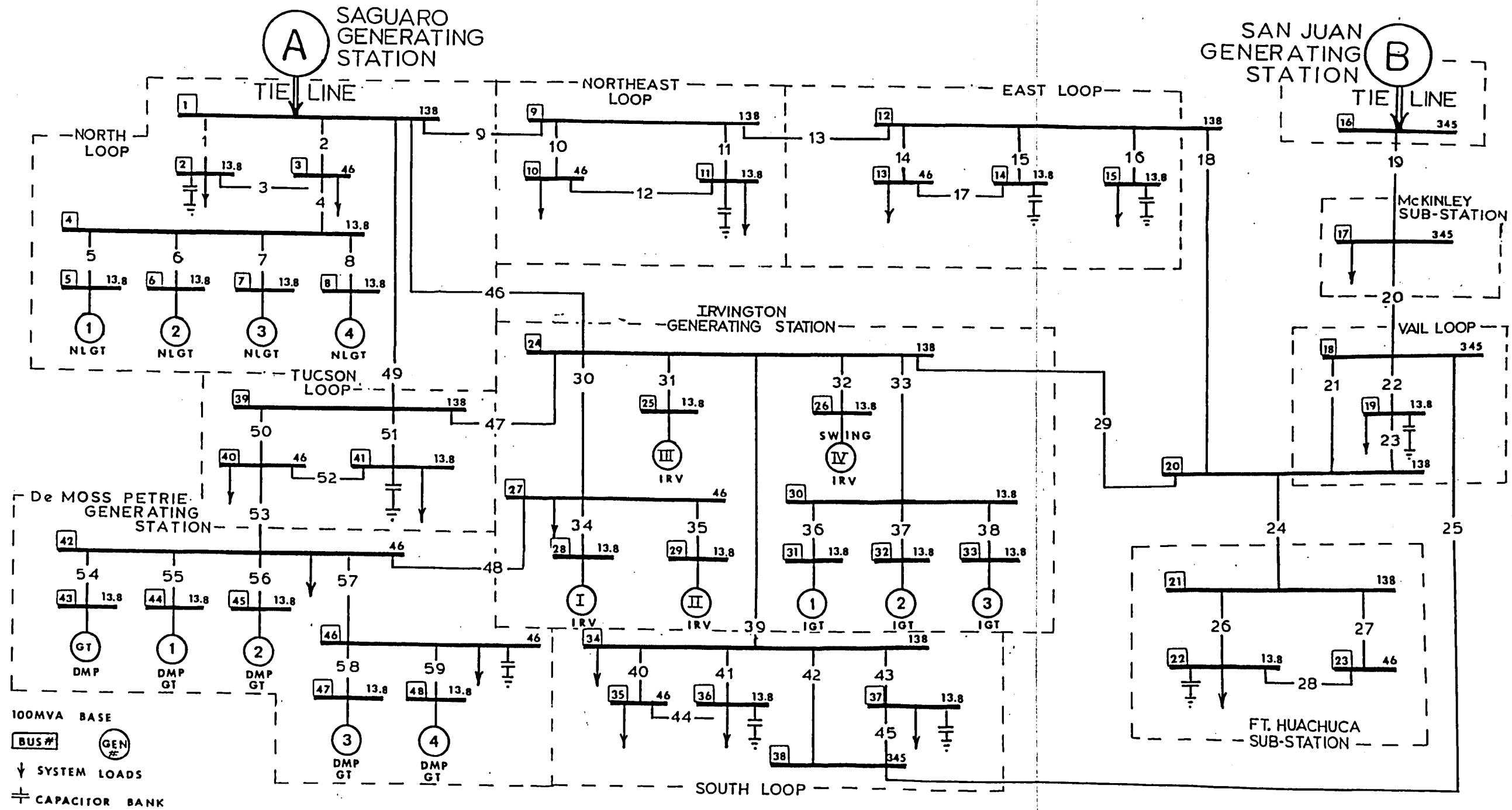


Figure 6.1 TGE Transmission System

contains the "slack" bus for the system. Two intra-area 345KV tie lines connect the TGE system with the Arizona Power System (APS) Saguaro generating station A and the joint owned San Juan generating station B as shown in Figure 6.1.

Each load center generally has three buses interconnected by a three winding transformer to provide three voltage levels as indicated on the right end of each bus, i.e., 138KV, 46KV, and 13.8KV. The transformers interconnecting these buses are usually a Y-Delta-Y configuration with the delta winding at 13.8KV. The transformers are not shown on the schematic but are represented as transmission lines with their equivalent network impedances shown as line data, e.g., lines 1, 2, and 3 at North Loop are transformer equivalent circuits. Bus numbers shown in the boxes at the left end of each bus and the transmission line numbers were assigned arbitrarily. Voltage compensating capacitor banks are shown as shunt capacitors to ground on the affected buses.

Since each area contains only one bus at each voltage level, the arrows attached to these buses represent a composite of all the loads in the area connected radially to the indicated bus. Lumping the individual loads and transmission losses together as one composite load does not give a true picture of total system transmission losses. However, power distribution at this level in the system is

fixed and is not the primary concern of our economic dispatch study, i.e., there is no alternate routing to these loads to service them more economically. Planning studies where the economic advantages of adding additional alternate transmission lines to satisfy large power users would require the model to be expanded below the load center level in these areas.

Topping or peaking gas turbine generators are used in the North Loop, DeMoss Petrie, and Irvington areas to supply additional power during peak demand periods. They are shown as circles in the schematic. The generators shown as I, II, III, and IV are the main boiler fired generators at the Irvington plant. A 100MVA power base is used for the system with all parameters shown in per unit values.

TGE Line Data

Only lumped distribution network parameters were available from TGE; therefore, the length of all lines is shown as unity. However, the following cable types are typical of those used throughout the TGE system: ACSR #795MCM for 138KV lines, ACSR #477MCM or AA #4/0 for 46KV lines, and AA #1/0 or AA #4/0 for the 13.8 KV lines. The values used to represent the TGE transmission line distribution network are shown in Problem 3, Appendix A.

TGE Bus Data

A moderate total load for the system of 6.85 per units was assumed and distributed as shown in Problem 3 of Appendix A "Bus Data." The initial estimate for the generator power settings was arbitrarily selected and a flat voltage profile was used for each bus except 1 and 16. These buses receive tie line power and consequently were fixed at their maximum voltage levels. As explained in Chapter 7 tie line power at a fixed cost is used prior to local generation. All buses with compensating capacitor or inductor banks are designated type 2 buses to determine the amount of compensation required. Bus 26 at the Irvington Generating Station is the "slack" bus for the system. A negative bus type is used to indicate those buses with generators attached. The values used to represent the TGE bus data are shown in Problem 3, Appendix A.

Generator Data

Incremental heat rates for 9 typical generating units were obtained for the TGE system shown in Figure 6.1 in lieu of actual TGE performance data. The equation representing each heat curve and the location of each type turbine generator used is shown in Table 6.1. Y_i represents the i th turbine generator incremental heat rate in BTU per kilowatt hour and PG_i represents its net electrical output in megawatts. To convert these curves into incremental

Table 6.1 Typical Generator Incremental Heat Rates

Boiler Fired IRV I generator at Bus 28		
$Y_{28} = 8,809.36 + 10.01PG_{28} + 0.0441PG_{28}^2$		BTU/KWHR
Boiler Fired IRV II generator at Bus 29		
$Y_{29} = 7,948.05 + 27.8PG_{29} + 0.017PG_{29}^2$		BTU/KWHR
Boiler Fired IRV III generator at Bus 25		
$Y_{25} = 8,708.21 + 12.4PG_{25} + 0.0089PG_{25}^2$		BTU/KWHR
Boiler Fired IRV IV generator at Bus 26		
$Y_{26} = 8,399.7 + 4.205PG_{26} + 0.013PG_{26}^2$		BTU/KWHR
Gas Turbine Peaking generator at Buses indicated		
$Y_{43} = 9,461.7 + 45.22PG_{43} - 0.212PG_{43}^2$		BTU/KWHR
$Y_{44} = 9,209.8 + 138.7PG_{44} + 1.933PG_{44}^2$		BTU/KWHR
$Y_{45} = 9,209.8 + 128.7PG_{44} + 1.833PG_{45}^2$		BTU/KWHR
$Y_{48} = 9,511.74 + 52.22PG_{48} - 0.212PG_{48}^2$		BTU/KWHR
$Y = 9,561.74 + 55.22PG - 0.212PG^2$		BTU/KWHR
at Buses 5-8, 31-33, and 47		

cost curves, the fuel heating value (BTU per pound) and the cost (dollars per pound) of the fuel used is required.

Current values of three types of fossile fuels are shown below so that a comparison of system operating cost can be made by type fuel (see, e.g., Friedlander, 1977; The Oil and Gas Journal, May 1, 1978:32; June 12, 1978:100-101)

Delivered Coal (e.g., Four Corners Coal)	112.0¢/10 ⁶ BTU
Natural Gas (e.g., West South Central Gas)	147.4¢/10 ⁶ BTU
Oil (e.g., West South Central Oil)	155.0¢/10 ⁶ BTU

The normalized incremental cost curves are obtained by multiplying the incremental heat rate curve coefficients by the selected fuel cost in dollars per BTU and then using Equation (3.21) for the per unit value. A power base S_b of 100MVA was arbitrarily chosen for the system and three system cost bases C_b were used depending on the type fuel used. They are: \$112.0/Hr for Coal, \$147.4/Hr for natural gas, and \$155.0/Hr for oil. The normalized incremental cost curve coefficients used for each generator and an arbitrarily selected set of generator constraints for each generator and type 2 bus are shown in Problem 3 of Appendix A.

A load flow and economic dispatch solution has been included in Problem 3 using the parameters shown as input data to describe the system shown in Figure 6.1. Actual

performance data were not available for comparison at this time.

CHAPTER 7

COMPUTER CODE DESCRIPTION AND OPERATION

The computer code is a series of FORTRAN 10 statements for use with the DEC-10 FORTRAN 10 optimizing compiler. It has a main program and a series of subroutines to perform special repetitive functions. Two codes were developed: EDSP50 to accommodate a maximum of 50 buses and 100 transmission lines, and EDSP15 to accommodate 15 buses and 30 transmission lines. EDSP15 includes an accelerated Gauss-Seidell load flow solution method for instructional and demonstration purposes. The code can be changed easily to accommodate any size system by expanding the dimension statements. Both computer code listings are shown in Appendix B.

The computer code is designed as an interactive program and will prompt the user when action or input is required. The prompting messages are explained below.

))ENTER TYPE PROBLEM. A response of 0 or 1 is required for selection of a load flow or economic dispatch study respectively.

))ENTER LOAD FLOW SOLUTION METHOD. This message is received on the EDSP15 code only and permits load flow studies by Newton-Raphson or accelerated Gauss-Seidel

methods. The EDSP50 code solves the load flow problem by Newton-Raphson methods only.

) ENTER THE TOTAL NUMBER OF (LINES, & BUSES).

) WANT TO TYPE IN NEW (LINE DATA, BUS DATA,
GENERATOR DATA, OR OR CALCULATE Y/Z BUS MATRIX)?

A response of Y or N is required for each data group, i.e., "NYNN" would indicate you wish to enter new bus data only. Note that there are no spaces or commas between letters in the response. Also note that the letters must be capitalized. If the response is N for any data group, the necessary data must be stored in their respective temporary SOS files, i.e., for each N response the code looks in the respective SOS file as outlined in Chapter 2 for the necessary input data. When entering new data for the first time, the entries must be in the order prompted and each data entry must be separated by a space or a comma. Non-integer numbers such as any system parameter may be entered in floating point or exponential form but must be in per unit values. If the data are entered during program execution, temporary SOS data files as outlined in Chapter 2 are automatically created so that subsequent runs may be made using the same data without having to re-enter it for each run. For large programs it will probably be easier to enter data directly into the temporary SOS data files prior to execution of the code since editing or error corrections are easier and quicker with the SOS text editor.

If an entry is unacceptable, the code will so indicate and a corrected entry will be accepted. However, erroneous data will not be detected and correction of the error must wait until after the data group is completed.

When entering "Line Data," the transmission line parameters should be in per unit value per unit length.

When entering "Bus Data," the bus type must be negative to indicate the presence of a generator. Also, an initial estimate is required for each generator power P_{G_i} and Q_{G_i} and the bus voltage V_i and δ_i not given. These initial estimated values are usually not critical but for very large problems, a poor initial estimate could increase the computation time or even cause divergence of the solution. The best guide is to use a flat voltage profile where $|V_i| \frac{\delta_i}{\sum Q_{D_i}}$ equals $1.0/0.0$ for the unknown voltages and $\frac{\sum P_{D_i}}{\text{No. of Gen.}}$ and $\frac{\sum Q_{D_i}}{\text{No. of Gen.}}$ equals the estimated real and reactive powers respectively. The EDSP15 code automatically sets δ_i to 0.0 initially while the user must specify $|V_i|$.

When entering "Generator Data," provisions have been included for accepting "Tie Line" power where the generator cost curves are not applicable. In this case, the generator cost curve coefficients should be entered as 0.0 for each coefficient alpha, beta, and gamma indicating constant cost tie line power. The code schedules the use of this power prior to use of locally generated power.

When entering "Generator Constraints," the code requires the following:

1. For load flow problems only: reactive power limits are required for Type ± 2 , voltage control buses, i.e., QG_{imax} and QG_{imin} . Real power limits PG_{imax} and PG_{imin} are not used.
2. For economic dispatch problems: the real power limits PG_{imax} and PG_{imin} are required for all generators including "Tie Line" power. The reactive power limits QG_{imax} and QG_{imin} are also required for each Type ± 2 , voltage control bus.

The real and reactive power limits can be used to fix the generated power at a specific level by setting the maximum and minimum limits at the same value.

No entries are required for convergence criteria.

They are pre-set in the computer code as follows:

1. The maximum number of load flow iteration permitted for the Newton-Raphson solution method is 5. In the EDSP15 code the maximum number of iterations permitted for the Gauss-Seidel solution method is 30.
2. The load flow solution tolerance TOL is set at 0.0001.
3. The maximum number of economic dispatch iterations ITER for determination of λ and to obtain a power balance in the system is set at 50.

4. The economic dispatch tolerance ESP1 for the system power balance, Equation (3.25), is set at 0.001.
5. The economic dispatch solution tolerance ESP2 for convergence is set at 0.001, i.e., Equation (5.1).

If values other than these "pre-set" values are desired, they may be revised when prompted during data change requests.

))WANT A COPY OF (LDATA, BDATA, GDATA, OR SYSTEM CONVERGENCE CRITERIA?) A response of N or Y is required for each data group for which a printout is desired, i.e., YNNN will cause printout of "Line Data" only.

))WANT TO CHANGE (LDATA, BDATA, GDATA, OR CONVERGENCE CRITERIA)? Again a response of N or Y is required for each data group where data changes are desired, i.e., YNNY would permit changes to both "Line Data" and "Convergence Criteria." In this mode, entries may be corrected as many times as desired. Further, the changes may be posted to the temporary SOS files if desired. The EDSP15 code automatically updates the SOS file with the changes when the data group is exited by typing 0.

It should be realized that changes in one data group may require changes in another. For instance, a change of a bus type from 1 to 2 in "Bus Data" would require the addition of reactive power limits at this bus in the

"Generator Data" group. Another example is shown in Problem 2, Appendix A, when changing from a load flow study to an economic dispatch analysis, the generator cost curve coefficients must be added and the Z bus matrix calculated. Also, if the total number of buses or lines is increased, the additional line, bus, and generator parameters may be added by requesting a change in their respective data groups.

)) WANT A COPY OF (Y BUS MATRIX, OR Z BUS MATRIX)?
A Y or N is required for each data group. If a load flow problem is being performed the Z Bus matrix is not calculated and therefore will not print out.

)) TYPE CODE # FOR DESIRED ACTION
1=PRINT BUS & GEN SOLUTIONS ONLY
2=PRINT LINE POWERS, BUS & GEN SOLUTIONS
3=CREAT SOS FILE OF SOLUTIONS
4=CHANGE DATA OR TOLERANCES AND RERUN
5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
RERUN WITH EXISTING DATA
6=NEW PROBLEM
7=TERMINATE

An entry of 1 or 2 will obtain a printout of the solution data indicated at the user's terminal. An entry of 3 will create a temporary SOS data file of bus, generator, and line power flow solutions so that all or part of the data may be printed on the high speed line printer. Also, the temporary data and solution files may be transferred to magnetic tape for permanent storage. Entering 4 or 5 will permit changes of type problem or input data using the previous solution as an initial starting point for the new

calculations. For large programs this permits considerable savings in computer calculation time when only small changes to the input data are desired. Since this is less significant for small size systems, EDSP15 re-enters the original input data from the SOS files prior to each rerun. Items 6 and 7 are self explanatory.

Diagnostics

During load flow calculations the following messages may be transmitted to inform the user when programmed limits have been reached:

"Bus # ____ exceeds QGMAX/QGMIN, bus changed to type 1." This message applies to Type 2 control buses only. As indicated, it informs the user that the specified reactive power limits have been reached. The type bus is then changed to a Type 1 and the solution continues letting the voltage magnitude vary until a solution is obtained or the maximum number of iterations has been reached. The buses that were changed to Type 1 are returned to a Type 2 and the bus voltage magnitudes are reset to 1.0 if a rerun of the problem is requested, i.e., action 4 or 5. Also, the bus type and voltage magnitude are reset to type 2 and 1.0 respectively between economic dispatch iterations. This permits "back-off" from limits at these buses during solution for the optimum power settings.

"No convergence in ___ iterations." This message indicates the specified solution tolerance could not be obtained within the number of iterations permitted. The calculations to this point in the solution should be printed for study before a rerun is accomplished with an increased number of iterations.

During economic dispatch calculations the following messages may be received:

"System power loss is negative, check total system power generation." This is a check to see that the power balance equation (3.25) was satisfied during load flow calculations.

"Maximum constant cost power not used, load flow problem only." This indicates that the total system load plus losses is less than the amount of power available from the tie line power. As stated earlier, constant cost tie line power is used prior to locally generated power.

"Power balance equation not satisfied in ___ iterations." This indicates that the maximum number of economic dispatch iterations was reached before Equation (3.25) could be satisfied by varying Λ . The real power generation limits, cost curve coefficients, and convergence criteria should be reviewed before a rerun is accomplished. Again a printout of the bus and generator solutions will reveal calculation results to that point in

the solution process and will probably indicate the problem area.

CHAPTER 8

RESULTS AND CONCLUSIONS

Results

This chapter will include the findings and significant observations made during the use of the computer code. While space considerations preclude the inclusion of machine runs to demonstrate each of our observations, sample problems were provided in Appendix A for familiarization with the computer code mechanics. Hopefully, the users will then develop their own power system analysis techniques with the observations included.

As stated in Chapter 4, the Newton-Raphson solution method was chosen for the large computer code EDSP50. Initial evaluation of load flow solution methods showed that the Gauss-Seidel or successive displacement method had many conditions for which a solution could not be obtained, i.e., the solution would diverge, oscillate, or converge to a point and go no further. Also, the number of iterations increased rapidly as the problem size increased. Therefore, the Gauss-Seidel solution method was retained in the smaller code EDSP15 only. It contains an acceleration factor of 1.5 in the solution algorithm to increase the speed of convergence. That is, the change in voltage magnitude and

phase angle between each iteration is multiplied by the acceleration factor of 1.5. Since speed of convergence is influenced by the size of the system, impedance characteristics of the transmission network, and how heavily the system is loaded, there may not be an optimum acceleration factor for this solution method. Further study may develop a non-linear acceleration factor to improve this method but since the Newton-Raphson methods proved superior in convergence reliability, no further effort was expended on the Gauss-Seidel method.

The computer code description in Chapter 7 along with the sample problems should familiarize the user with the operation of the code and its options for the control of power system studies. To enhance the utility of the code to the power system engineer, a few of the more significant results of power system studies are included below. They become important as the size of the system increases, e.g., above 25 buses.

1. The "slack" bus should be near the electrical center of the system.
2. In larger systems, as the load increases, voltage control at certain buses becomes critical. Therefore, numerous type 2 buses should be used throughout the system. This in effect places additional reactive power "slack" buses in the system.

3. Depending on the load conditions, electrical characteristics of the transmission network, and the generator cost curve characteristics, the lowest total system operating cost may not be the lowest total transmission loss operating point, e.g., problems 1 and 2 in Appendix A.
4. If convergence fails, the bus, generator, and line power flow calculations at the point of solution termination should be printed out for study before reruns with lower solution tolerances or increase iteration limits are accomplished. The area of difficulty can usually be detected. For example, if the phase angle at a particular bus exceeds 1.5, the maximum transmission line capacity is being exceeded and system convergence will fail due to the inability to satisfy the power balance equation (3.16). Also, if bus voltage is too low or too high the reactive power generation and limits should be checked. If during economic dispatch analysis, the load flow calculations converge but the economic dispatch solution does not converge, the generator cost curves and real power generation limits should be checked. Solution tolerance and iteration limits can then be relaxed if necessary to obtain solution convergence. However, if the load flow solution is not accomplished in 3 to 5 iterations there is

usually an error in data entry or the initial estimate of system parameters. These should be rechecked before reruns with expanded iteration limits are made.

Conclusions

The computer code developed is an effective engineering tool for the analysis of power system performance. Its direct on-line calculations and interactive capability provide the flexibility to significantly reduce the engineering manhours involved in problem set-up and system analysis. In addition, its ability to store network parameters for use in subsequent studies further enhances its utility for quick response problems such as serious outage conditions. The code has demonstrated sufficient accuracy to reliably determine system transmission losses and operating cost data. Also, this code can be used on nuclear or fossile fuel powered generating plants but would not be applicable to hydroelectric plants unless a fuel equivalent ratio were developed for the water used in electric power generation. The timesharing feature of the DEC-10 provides a significant cost advantage in that a high cost computer need not be dedicated to the sole support of the engineering effort but can serve all management functions simultaneously.

Current nationwide energy conservation efforts dictate that electrical power companies continue their efforts to improve efficiency. The latest industry survey by Friedlander (1977:51) indicates that 50 per cent of the power companies have now developed some type of system performance analysis capability. The computer code developed in this thesis continues this effort to optimize the analysis process for continued improvement in energy conservation efforts.

Recommendations

Recent advances in computer technology have expanded the capability of digital computers to process and store the large quantity of data necessary to analyze electrical power system performance. Therefore, the power system engineer should continue to develop new and better ways to use this increasing computer capacity for the improvement of all phases of electrical power production and distribution. Research should continue in the area of interactive computer programming of electrical power system performance and control. Extensive use of this interactive code indicates the following areas where further development could enhance its utility and capability.

1. Replace the matrix inversion routines used to obtain Z bus matrix and the inverse jacobian matrix in Equations (4.16) and (4.17) with a direct

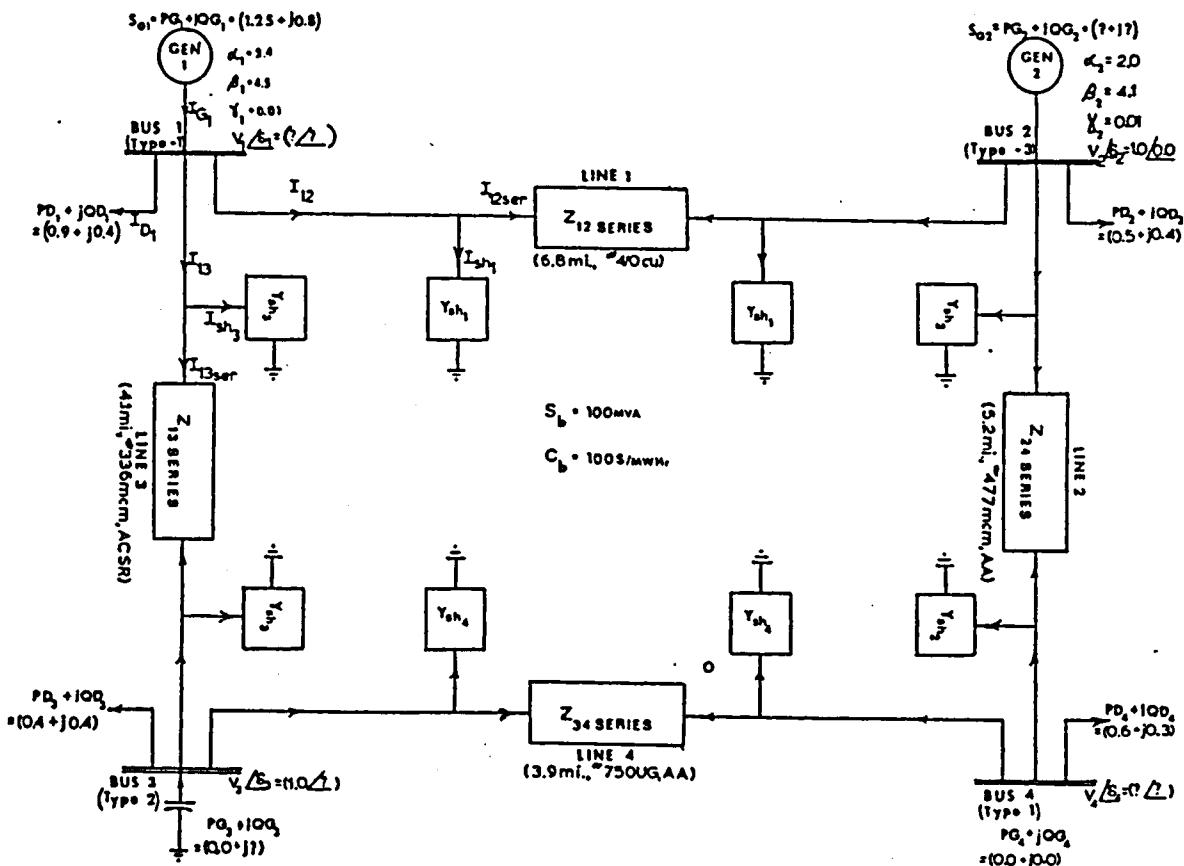
solution method using optimally ordered triangular factorization (see, e.g., Tinney and Walker, 1967:1801-1809; Tinney and Meyer, 1973). This would reduce the computer time required to obtain these inverse matrices by one-third. It would also improve solution accuracy by reducing roundoff errors inherent in matrix inversion routines. In addition, it would preserve the sparsity that is characteristic of the Y admittance matrix. This would permit further reduction in central (core) memory storage requirements (see, e.g., Ogbuobiri, 1970:150-155; Tinney and Sato, 1963).

2. Features could be added to accommodate tap changing under load and phase shifting transformers (see, e.g., Elgerd, 1971:263-270; Peterson and Meyer, 1971:103-108). This would improve flexibility in voltage control and line power flow and further enhance the solution convergence reliability.
3. The incorporation of penalty factors instead of hard limits for reactive power generation and steepest descent or gradient method for finding the optimum power point should be investigated as ways to further improve speed and reliability of convergence (see, e.g., Elgerd, 1971:304-312; Dommel and Tinney, 1968; Peschon et al., 1968:40-48).

APPENDIX A

SAMPLE PROBLEMS

Problem 1: 4-Bus Power System



.RUN EDPF15C3733,547J

ECONOMIC DISPATCH EXECUTIVE PROGRAM

```

>>ENTER TYPE PROBLEM
      0=LOAD FLOW PROBLEM
      1=ECONOMIC DISPATCH PROBLEM
0

>>ENTER LOAD FLOW SOLUTION METHOD
      0=NEWTON-RAPHSON
      1=ACCELERATED GAUSS-SEIDEL
      2=PATTERN SEARCH
0

>>ENTER TOTAL NUMBER OF (LINES, & BUSES).
4,4

>>WANT TO TYPE IN NEW(LINE DATA, BUS DATA, OR GENERATOR DATA)?
YNY

**SYSTEM LINE DATA**
>>ENTER (LINE #,SB #,EB #, LINE LENGTH, YSHUNT G,YSHUNT B,ZSERIES R,ZSERIES X)
1,1,2,35.904,0.0,0.0,0.271267E-2,0.60586E-2
2,2,4,27.456,0.0,0.0,0.19329E-2,0.56475E-2
3,1,3,21.648,0.0,0.0,0.27410E-2,0.56522E-2
4,3,4,20.592,0.0,0.9,2531E-4,0.15123E-2,0.17958E-2

**SYSTEM BUS DATA**
>>ENTER(BUS#, BUS TYPE,PG,OG,PD,OD,VSPEC)
1,-1,1.25,0.8,0.9,0.4,1.0,0.0\0.0,\
2,-3,1.2,1.1,0.5,0.4,1.0
3,2,0.0,0.4,0.4,0.4,1.0
4,1,0.0,0.0,0.6,0.3,1.0

**GENERATOR CONSTRAINT DATA**
>>ENTER FOR TYPE -1 & -3 BUS (BUS #,PGMAX,PGMIN)
      FOR TYPE -2 BUS      (BUS #,PGMAX,PGMIN,OGMAX,OGMIN)
      FOR TYPE +2 BUS      (BUS #,OGMAX,OGMIN)
1,3,0,0.5
2,3,0,0.5,2.0,-2.0
3,2,0,-2.0

>>WANT A COPY OF (LDATA,RDATA,GDATA,OR SYSTEM CONVERGENCE CRITERIA)?
YYYY

**SYSTEM LINE DATA**
LINE # SB EB      LENGTH          Y SHUNT          Z SERIES
1      1  2  0.35904E+02  0.00000E+00  0.00000E+00  0.27127E-02  0.60586E-02
2      2  4  0.27456E+02  0.00000E+00  0.00000E+00  0.19329E-02  0.56475E-02
3      3  1  0.21648E+02  0.00000E+00  0.00000E+00  0.27410E-02  0.56522E-02
4      3  4  0.20592E+02  0.00000E+00  0.92531E-03  0.15123E-02  0.17958E-02

**SYSTEM BUS DATA**
BUS   TYPE   PG      OG      PD      OD      VSPEC
1     -1    1.25000  0.80000  0.90000  0.40000  1.00000
2     -3    1.20000  1.10000  0.50000  0.40000  1.00000
3      2    0.00000  0.40000  0.40000  0.40000  1.00000
4      1    0.00000  0.00000  0.60000  0.30000  1.00000

```

```

**GENERATOR CONSTRAINTS**
BUS #   PGMAX   PGMIN   QGMAX   QGMIN
  1     3.0000   0.5000
  2     3.0000   0.5000
  3
                    2.0000   -2.0000

```

```

**SYSTEM CONVERGENCE CRITERIA**
LOAD FLOW ITERATIONS= 5
LOAD FLOW TOLERANCE= 0.10000E-03
ECON DISP ITERATIONS= 50
ESP1= 0.10000E-02
ESP2= 0.10000E-02

```

```

>>WANT TO CHANGE (LIDATA, BDATA, GDATA, OR CONVERGENCE CRITERIA)?
YYYY

```

```

** LINE DATA CHANGES**
>>ENTER (VARIABLE #, LINE #, NEW VALUE THEN *CR*)
  1=STARTING BUS #
  2=ENDING BUS #
  3=LINE LENGTH
  4=Y SHUNT G
  5=Y SHUNT B
  6=Z SERIES R
  7=Z SERIES X
  8=RETYPE COPY OF ALL LINE DATA
  9=CHANGE TOTAL NUMBER OF LINES
>>ENTER 0 THEN *CR* WHEN CHANGES COMPLETED

```

0

```

**BUS DATA CHANGES**
>>ENTER (VARIABLE #, BUS #, NEW VALUE THEN *CR*)
  1=BUS TYPE
  2=PG
  3=QG
  4=PD
  5=QD
  6=VSPEC
  7=RETYPE COPY OF ALL BUS DATA
  8=CHANGE TOTAL NUMBER OF BUSES
>>ENTER 0 THEN *CR* WHEN CHANGES COMPLETED.

```

0

```

**GENERATOR DATA CHANGES**
>>ENTER (VARIABLE #, BUS #, NEW VALUE THEN *CR*)
  1=ALPHA
  2=BETA
  3=GAMMA
  4=PGMAX
  5=PGMIN
  6=QGMAX
  7=QGMIN
  8=RETYPE ALL GENERATOR DATA
>>ENTER 0 THEN *CR* WHEN CHANGES COMPLETED.

```

0

****CONVERGENCE CRITERIA CHANGES****
 >>ENTER(VARIABLE #,NEW VALUE THEN 'CR')
 1=LOAD FLOW ITERATIONS
 2=LOAD FLOW TOLERANCE
 3=ECON DISP ITERATIONS
 4=ESP1
 5=ESP2
 >>ENTER 0 THEN 'CR' WHEN CHANGES COMPLETED.

0

****GENERATING YBUS MATRIX****

>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?
 YN

****CALCULATED SYSTEM LINE DATA****

LINE #	Y SHUNT		Y SERIES	
1	0.000000E+00	0.000000E+00	0.171459E+01	-0.382941E+01
2	0.000000E+00	0.000000E+00	0.197584E+01	-0.577296E+01
3	0.000000E+00	0.000000E+00	0.320870E+01	-0.661664E+01
4	0.000000E+00	0.952699E-02	0.133240E+02	-0.158217E+02

****YBUS MATRIX****

ROW 1
 0.11548E+02-0.11304E+01 0.41957E+01 0.19918E+01 0.73536E+01 0.20223E+01
 0.00000E+00 0.00000E+00
 ROW 2
 0.41957E+01 0.19918E+01 0.10287E+02-0.12039E+01 0.00000E+00 0.00000E+00
 0.61017E+01 0.19006E+01
 ROW 3
 0.73536E+01 0.20223E+01 0.00000E+00 0.00000E+00 0.27864E+02-0.93559E+00
 0.20685E+02 0.22707E+01
 ROW 4
 0.00000E+00 0.00000E+00 0.61017E+01 0.19006E+01 0.20685E+02 0.22707E+01
 0.26458E+02-0.95418E+00

****SOLVING LOAD FLOW EQUATIONS BY NR****

*****NR CONVERGENCE IN 3 ITERATIONS**

>>TYPE CODE # FOR DESIRED ACTION

1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

2

*****SYSTEM BUS AND GENERATOR SOLUTIONS*****

SYSTEM LOSSES(PU)= 0.0431, SYSTEM LOAD(PU)= 2.4000

BUS #	BTYPE	PG	QG	PD	QD	VMAG	VANG
1	-1	1.2500	0.8000	0.9000	0.4000	1.0419	-0.0521
2	-3	1.1931	0.0965	0.5000	0.4000	1.0000	0.0000
3	2	0.0000	0.6846	0.4000	0.4000	1.0000	-0.1008
4	1	0.0000	0.0000	0.6000	0.3000	0.9832	-0.0906

LINE POWER FLOW

LINE#	SB	EB	REAL POWER	REACTIVE POWER
1	1	2	-0.1303	0.2657
1	2	1	0.1381	-0.2481
2	2	4	0.5550	-0.0554
2	4	2	-0.5385	0.1036
3	1	3	0.4803	0.1343
3	3	1	-0.4667	-0.1063
4	3	4	0.0667	0.3909
4	4	3	-0.0615	-0.4036

>>TYPE CODE # FOR DESIRED ACTION

1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

5

****ECONOMIC DISPATCH EXECUTIVE PROGRAM****

>>ENTER TYPE PROBLEM

0=LOAD FLOW PROBLEM
 1=ECONOMIC DISPATCH PROBLEM

1

>>IS SYSTEM LOSSLESS?

NO

>>ENTER LOAD FLOW SOLUTION METHOD

0=NEWTON-RAPHSON
 1=ACCELERATED GAUSS-SEIDEL
 2=PATTERN SEARCH

0

>>ENTER TOTAL NUMBER OF (LINES, & BUSES).

4,4

>>WANT TO TYPE IN NEW(LINE DATA, BUS DATA, OR GENERATOR DATA)?

NNN

>>WANT A COPY OF (LDATA,BDATA,GDATA,OR SYSTEM CONVERGENCE CRITERIA)?

NNYN

SYSTEM GENERATOR DATA

NUMBER OF GENERATORS = 2

BUS#	ALPHA	BETA	GAMMA
1	2.40000	4.50000	0.01000
2	2.00000	4.10000	0.01000

GENERATOR CONSTRAINTS

BUS #	PGMAX	PGMIN	QGMAX	QGMIN
1	3.0000	0.5000		
2	3.0000	0.5000		
3			2.0000	-2.0000

>>WANT TO CHANGE (LDATA,BDATA,GDATA, OR CONVERGENCE CRITERIA)?

NNNN

GENERATING YBUS MATRIX

CALCULATING ZBUS MATRIX

>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?
NY

ZBUS MATRIX

ROW 1
0.52388E+02-0.15700E+01 0.52446E+02-0.15705E+01 0.52478E+02-0.15707E+01
0.52487E+02-0.15709E+01
ROW 2
0.52446E+02-0.15705E+01 0.52375E+02-0.15700E+01 0.52486E+02-0.15709E+01
0.52479E+02-0.15707E+01
ROW 3
0.52478E+02-0.15707E+01 0.52486E+02-0.15709E+01 0.52474E+02-0.15707E+01
0.52491E+02-0.15709E+01
ROW 4
0.52487E+02-0.15709E+01 0.52479E+02-0.15707E+01 0.52491E+02-0.15709E+01
0.52474E+02-0.15707E+01

SOLVING LOAD FLOW EQUATIONS BY NR

****NR CONVERGENCE IN 3 ITERATIONS

OPTIMIZING COST FUNCTIONS

LAMBDA DETERMINED IN 15 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR

****NR CONVERGENCE IN 2 ITERATIONS

OPTIMIZING COST FUNCTIONS

LAMBDA DETERMINED IN 4 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR

****NR CONVERGENCE IN 1 ITERATIONS

OPTIMIZING COST FUNCTIONS

LAMBDA DETERMINED IN 0 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR

****NR CONVERGENCE IN 1 ITERATIONS

OPTIMIZING COST FUNCTIONS

LAMBDA DETERMINED IN 0 ITERATIONS

>>TYPE CODE # FOR DESIRED ACTION

- 1=PRINT BUS & GEN SOLUTIONS ONLY.
- 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
AND SYSTEM OPERATING COST.
- 3=CREATE SOS FILE OF SOLUTIONS
- 4=CHANGE DATA OR TOLERANCES AND RERUN
- 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
RERUN WITH EXISTING DATA
- 6=NEW PROBLEM
- 7=TERMINATE

2

****SYSTEM BUS AND GENERATOR SOLUTIONS****

ECON. DISPATCH CONVERGENCE IN 4 ITERATIONS

ESP1= 0.0010, ESP2= 0.0010, LAMBDA= .7.9094

SYSTEM LOSSES(PU)= 0.0464, SYSTEM LOAD(PU)= 2.4000

BUS#	BTYPE	IC	ITL	PG	QG	PD	QD	VMAG	VANG
1	-1	7.5834	0.0412	1.1488	0.8000	0.9000	0.4000	1.0384	-0.0658
2	-3	7.3368	0.0724	1.2976	0.0760	0.5000	0.4000	1.0000	0.0000
3	2	0.0000	0.0000	0.0000	0.7144	0.4000	0.4000	1.0000	-0.1105
4	1	0.0000	0.0000	0.0000	0.0000	0.6000	0.3000	0.9836	-0.0981

****SYSTEM OPERATING COST****

GEN.# 1= 5.73P.U.
 GEN.# 2= 6.05P.U.
 TOTAL SYSTEM OPERATING COST = 11.79P.U.

****LINE POWER FLOW****

LINE#	SB	EB	REAL POWER	REACTIVE POWER
1	1	2	-0.1893	0.2783
1	2	1	0.1995	-0.2554
2	2	4	0.5981	-0.0686
2	4	2	-0.5788	0.1248
3	1	3	0.4381	0.1217
3	3	1	-0.4267	-0.0982
4	3	4	0.0267	0.4127
4	4	3	-0.0212	-0.4248

>>TYPE CODE # FOR DESIRED ACTION

- 1=PRINT BUS & GEN SOLUTIONS ONLY.
- 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
AND SYSTEM OPERATING COST.
- 3=CREATE SOS FILE OF SOLUTIONS
- 4=CHANGE DATA OR TOLERANCES AND RERUN
- 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
RERUN WITH EXISTING DATA
- 6=NEW PROBLEM
- 7=TERMINATE

4

>>WANT TO CHANGE (LDATA,BRATA,GDATA, OR CONVERGENCE CRITERIA)?
 NNYN

GENERATOR DATA CHANGES

>>ENTER (VARIABLE #, BUS #, NEW VALUE THEN 'CR')

- 1=ALPHA
- 2=BETA
- 3=GAMMA
- 4=PGMAX
- 5=PGMIN
- 6=QGMAX
- 7=QGMIN
- 8=RETYPE ALL GENERATOR DATA
- 9=UPDATE SOS FILE WITH CHANGES
- >>ENTER 0 THEN 'CR' WHEN CHANGES COMPLETED.

4,1,1.25

PGMAX(BUS # 1)= 0.12500E+01

5,1,1.25

PGMIN(BUS # 1)= 0.12500E+01

>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?
 NN

SOLVING LOAD FLOW EQUATIONS BY NR

****NR CONVERGENCE IN 0 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 13 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR

****NR CONVERGENCE IN 2 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 5 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR
 ***NR CONVERGENCE IN 1 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 0 ITERATIONS

>>TYPE CODE # FOR DESIRED ACTION
 1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
 AND SYSTEMOPERATING COST.
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

2

****SYSTEM BUS AND GENERATOR SOLUTIONS****
 ECON. DISPATCH CONVERGENCE IN 3 ITERATIONS
 ESP1= 0.0010, ESP2= 0.0010, LAMBDA= 7.4000
 SYSTEM LOSSES(PU)= 0.0431, SYSTEM LOAD(PU)= 2.4000

BUS#	RTYPE	IC	ITL	FG	GG	PD	QD	VMAG	VANG
1	-1	7.0549	0.0466	1.2500	0.8000	0.9000	0.4000	1.0419	-0.0521
2	-3	6.9078	0.0665	1.1931	0.0965	0.5000	0.4000	1.0000	0.0000
3	2	0.0000	0.0000	0.0000	0.6846	0.4000	0.4000	1.0000	-0.1008
4	1	0.0000	0.0000	0.0000	0.0000	0.6000	0.3000	0.9832	-0.0906

****SYSTEM OPERATING COST****
 GEN.# 1= 6.52P.U.
 GEN.# 2= 5.31P.U.
 TOTAL SYSTEM OPERATING COST = 11.83P.U.

****LINE POWER FLOW****

LINE#	SB	EB	REAL POWER	REACTIVE POWER
1	1	2	-0.1303	0.2657
1	2	1	0.1381	-0.2481
2	2	4	0.5550	-0.0554
2	4	2	-0.5385	0.1036
3	1	3	0.4803	0.1343
3	3	1	-0.4667	-0.1063
4	3	4	0.0667	0.3909
4	4	3	-0.0615	-0.4036

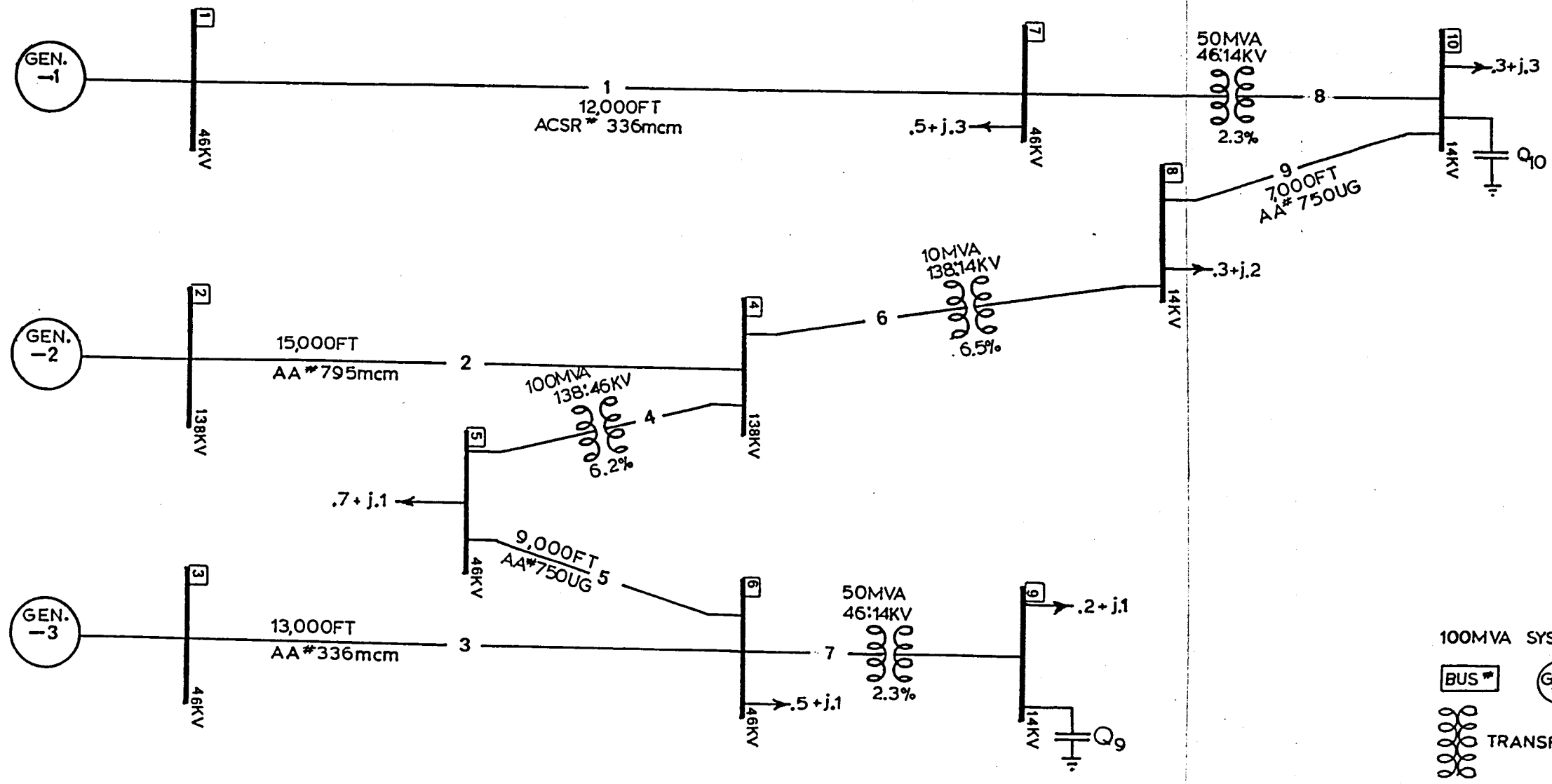
>>TYPE CODE # FOR DESIRED ACTION
 1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
 AND SYSTEMOPERATING COST.
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

7

STOP

END OF EXECUTION
 CPU TIME: 1.54 ELAPSED TIME: 5:46.85
 EXIT

Problem 2: 10-Bus Power System



RUN EDSF25[3733,547]

ECONOMIC DISPATCH EXECUTIVE PROGRAM

>>ENTER TYPE PROBLEM

0=LOAD FLOW PROBLEM
1=ECONOMIC DISPATCH PROBLEM

0

>>ENTER TOTAL NUMBER OF (LINES, & BUSES).

9,10

>>WANT TO TYPE IN NEW(LINE DATA, BUS DATA, OR GENERATOR DATA,
OR CALCULATE Y/ZBUS MATRIX)?

NNNY

>>WANT A COPY OF (LDATA,BDATA,GDATA,OR SYSTEM CONVERGENCE CRITERIA)?
YYYY

SYSTEM LINE DATA /

LINE #	SB	EB	LENGTH	Y SHUNT		Z SERIES	
1	1	7	0.22000E+02	0.00000E+00	0.00000E+00	0.27410E-02	0.56522E-02
2	2	4	0.25000E+02	0.00000E+00	0.00000E+00	0.11720E-02	0.00000E+00
3	3	6	0.23000E+02	0.00000E+00	0.00000E+00	0.27505E-02	0.58270E-02
4	4	5	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.62000E-01
5	5	6	0.90000E+01	0.00000E+00	0.92535E-03	0.15123E-02	0.17958E-02
6	4	8	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.62000E-01
7	6	9	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.46000E-01
8	7	10	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.46000E-01
9	8	10	0.70000E+01	0.00000E+00	0.92535E-03	0.15123E-02	0.17958E-02

SYSTEM BUS DATA

BUS	TYPE	PG	OG	PD	GD	VMAG	VANG
1	-1	0.80000	0.50000	0.00000	0.00000	1.00000	0.00000
2	-3	1.50000	0.30000	0.00000	0.00000	1.00000	0.00000
3	-2	0.70000	0.20000	0.00000	0.00000	1.00000	0.00000
4	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
5	1	0.00000	0.00000	0.70000	0.10000	1.00000	0.00000
6	1	0.00000	0.00000	0.50000	0.10000	1.00000	0.00000
7	1	0.00000	0.00000	0.50000	0.30000	1.00000	0.00000
8	1	0.00000	0.00000	0.30000	0.20000	1.00000	0.00000
9	2	0.00000	0.00000	0.20000	0.10000	1.00000	0.00000
10	2	0.00000	0.00000	0.30000	0.30000	1.00000	0.00000

GENERATOR CONSTRAINTS

BUS #	PGMAX	PGMIN	QGMAX	QGMIN
1	0.7500	0.0000		
2	3.0000	0.0000		
3	1.0000	0.0000	2.0000	0.0000
9			2.0000	0.0000
10			2.0000	0.0000

SYSTEM CONVERGENCE CRITERIA

LOAD FLOW ITERATIONS= 5
LOAD FLOW TOLERANCE= 0.10000E-03
ECON DISP ITERATIONS= 50
ESP1= 0.10000E-02
ESP2= 0.10000E-02

>>WANT TO CHANGE (LDATA,BDATA,GDATA, OR CONVERGENCE CRITERIA)?
NYYN

```

**BUS DATA CHANGES**
>>ENTER(VARIABLE #, BUS #, NEW VALUE THEN 'CR'
    1=BUS TYPE
    2=PG
    3=QG
    4=PD
    5=QD
    6=VMAG
    7=VANG
    8=RETYPE COPY OF ALL BUS DATA
    9=CHANGE TOTAL NUMBER OF BUSES
    10=REENTER ORIGINAL BUS DATA FROM SOS FILE
    11=UPDATE SOS FILE WITH CHANGES
    >>ENTER 0 THEN 'CR' WHEN CHANGES COMPLETED.

```

```

1,1,-2
BUS TYPE(BUS # 1)= -2
11
0

```

```

**GENERATOR DATA CHANGES**
>>ENTER (VARIABLE #, BUS #, NEW VALUE THEN 'CR')
    1=ALPHA
    2=BETA
    3=GAMMA
    4=PGMAX
    5=PGMIN
    6=QGMAX
    7=QGMIN
    8=RETYPE ALL GENERATOR DATA
    9=UPDATE SOS FILE WITH CHANGES
    >>ENTER 0 THEN 'CR' WHEN CHANGES COMPLETED.

```

```

6,1,2.0
QGMAX(BUS # 1)= 0.20000E+01
7,1,0.0
QGMIN(BUS # 1)= 0.00000E+00
9
0

```

```

**GENERATING YBUS MATRIX**

```

```

>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?
NN

```

```

**SOLVING LOAD FLOW EQUATIONS BY NR**
BUS # 1 EXCEEDS QGMIN,BUS CHANGED TO TYPE 1
BUS # 3 EXCEEDS QGMIN,BUS CHANGED TO TYPE 1
***NR CONVERGENCE IN 3 ITERATIONS

```

```

>>TYPE CODE # FOR DESIRED ACTION
    1=PRINT BUS & GEN SOLUTIONS ONLY.
    2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
      AND SYSTEMOPERATING COST.
    3=CREATE SOS FILE OF SOLUTIONS
    4=CHANGE DATA OR TOLERANCES AND RERUN
    5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
      RERUN WITH EXISTING DATA
    6=NEW PROBLEM
    7=TERMINATE

```

```

2

```

****SYSTEM BUS AND GENERATOR SOLUTIONS****

SYSTEM LOSSES(PU)= 0.1158, SYSTEM LOAD(FU)= 2.5000

BUS #	BTYPE	PG	QG	PD	QD	UMAG	VANG
1	-1	0.8000	0.0000	0.0000	0.0000	1.0246	0.0667
2	-3	1.1158	-0.5159	0.0000	0.0000	1.0000	0.0000
3	-1	0.7000	0.0000	0.0000	0.0000	1.0195	0.0262
4	1	0.0000	0.0000	0.0000	0.0000	0.9674	-0.0156
5	1	0.0000	0.0000	0.7000	0.1000	0.9765	-0.0636
6	1	0.0000	0.0000	0.5000	0.1000	0.9804	-0.0678
7	1	0.0000	0.0000	0.5000	0.3000	0.9823	-0.0323
8	1	0.0000	0.0000	0.3000	0.2000	0.9927	-0.0376
9	2	0.0000	0.5276	0.2000	0.1000	1.0000	-0.0772
10	2	0.0000	1.2932	0.3000	0.3000	1.0000	-0.0446

****LINE POWER FLOW****

LINE#	SB	EB	REAL POWER	REACTIVE POWER
1	1	7	0.8000	0.0000
1	7	1	-0.7632	0.0758
2	2	4	1.1158	-0.5159
2	4	2	-1.0715	0.5159
3	3	6	0.7000	0.0000
3	6	3	-0.6702	0.0632
4	4	5	0.7308	-0.1246
4	5	4	-0.7308	0.1610
5	5	6	0.0308	-0.2610
5	6	5	-0.0298	0.2542
6	4	8	0.3407	-0.3912
6	8	4	-0.3407	0.4090
7	6	9	0.2000	-0.4174
7	9	6	-0.2000	0.4276
8	7	10	0.2632	-0.3758
8	10	7	-0.2632	0.3858
9	8	10	0.0407	-0.6090
9	10	8	-0.0368	0.6073

>>TYPE CODE # FOR DESIRED ACTION

- 1=PRINT BUS & GEN SOLUTIONS ONLY.
- 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
AND SYSTEM OPERATING COST.
- 3=CREATE SOS FILE OF SOLUTIONS
- 4=CHANGE DATA OR TOLERANCES AND RERUN
- 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
RERUN WITH EXISTING DATA
- 6=NEW PROBLEM
- 7=TERMINATE

4

>>WANT TO CHANGE (LDATA,BDATA,GDATA, OR CONVERGENCE CRITERIA)?
NYNN

BUS DATA CHANGES

>>ENTER(VARIABLE #, BUS #, NEW VALUE THEN *CR*

- 1=BUS TYPE
 - 2=PG
 - 3=QG
 - 4=PD
 - 5=QD
 - 6=UMAG
 - 7=VANG
 - 8=RETYPE COPY OF ALL BUS DATA
 - 9=CHANGE TOTAL NUMBER OF BUSES
 - 10=REENTER ORIGINAL BUS DATA FROM SOS FILE
 - 11=UPDATE SOS FILE WITH CHANGES
- >>ENTER 0 THEN *CR* WHEN CHANGES COMPLETED.

```

10
6,1,1.05
VMAG(BUS # 1)= 0.10500E+01
6,2,1.05
VMAG(BUS # 2)= 0.10500E+01
6,3,1.05
VMAG(BUS # 3)= 0.10500E+01
8

```

***SYSTEM BUS DATA**

BUS	TYPE	PG	QG	PD	QD	VMAG	VANG
1	-2	0.80000	0.50000	0.00000	0.00000	1.05000	0.00000
2	-3	1.50000	0.30000	0.00000	0.00000	1.05000	0.00000
3	-2	0.70000	0.20000	0.00000	0.00000	1.05000	0.00000
4	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
5	1	0.00000	0.00000	0.70000	0.10000	1.00000	0.00000
6	1	0.00000	0.00000	0.50000	0.10000	1.00000	0.00000
7	1	0.00000	0.00000	0.50000	0.30000	1.00000	0.00000
8	1	0.00000	0.00000	0.30000	0.20000	1.00000	0.00000
9	2	0.00000	0.00000	0.20000	0.10000	1.00000	0.00000
10	2	0.00000	0.00000	0.30000	0.30000	1.00000	0.00000

```

11
0
>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?
NN

```

```

**SOLVING LOAD FLOW EQUATIONS BY NR**
****NR CONVERGENCE IN 2 ITERATIONS

```

```

>>TYPE CODE # FOR DESIRED ACTION
1=PRINT BUS # GEN SOLUTIONS ONLY.
2=PRINT LINE POWERS, BUS # GEN SOLUTIONS,
  AND SYSTEMOPERATING COST.
3=CREATE SOS FILE OF SOLUTIONS
4=CHANGE DATA OR TOLERANCES AND RERUN
5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
  RERUN WITH EXISTING DATA
6=NEW PROBLEM
7=TERMINATE

```

2

SYSTEM BUS AND GENERATOR SOLUTIONS

SYSTEM LOSSES(PU)= 0.1055, SYSTEM LOAD(PU)= 2.5000

BUS #	BTYPE	PG	QG	PD	QD	VMAG	VANG
1	-2	0.8000	0.1534	0.0000	0.0000	1.0500	0.0944
2	-3	1.1055	0.5551	0.0000	0.0000	1.0500	0.0000
3	-2	0.7000	0.0736	0.0000	0.0000	1.0500	0.0572
4	1	0.0000	0.0000	0.0000	0.0000	1.0193	0.0152
5	1	0.0000	0.0000	0.7000	0.1000	1.0045	-0.0289
6	1	0.0000	0.0000	0.5000	0.1000	1.0020	-0.0277
7	1	0.0000	0.0000	0.5000	0.3000	0.9896	0.0075
8	1	0.0000	0.0000	0.3000	0.2000	1.0015	-0.0052
9	2	0.0000	0.0567	0.2000	0.1000	1.0000	-0.0368
10	2	0.0000	0.4367	0.3000	0.3000	1.0000	-0.0048

LINE POWER FLOW

LINE#	SB	EB	REAL POWER	REACTIVE POWER
1	1	7	0.8000	0.1534
1	7	1	-0.7637	-0.0785
2	2	4	1.1055	0.5551
2	4	2	-1.0648	-0.5551

3	3	6	0.7000	0.0736
3	6	3	-0.6716	-0.0134
4	4	5	0.7286	0.2593
4	5	4	-0.7286	-0.2236
5	5	6	0.0286	0.1237
5	6	5	-0.0283	-0.1318
6	4	8	0.3363	0.2959
6	8	4	-0.3363	-0.2839
7	6	9	0.2000	0.0452
7	9	6	-0.2000	-0.0433
8	7	10	0.2637	-0.2214
8	10	7	-0.2637	0.2270
9	8	10	0.0364	0.0839
9	10	8	-0.0363	-0.0903

>>TYPE CODE # FOR DESIRED ACTION
 1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
 AND SYSTEM OPERATING COST.
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

5

>>ENTER TYPE PROBLEM
 0=LOAD FLOW PROBLEM
 1=ECONOMIC DISPATCH PROBLEM

1

>>IS SYSTEM LOSSLESS?
 NO

>>ENTER TOTAL NUMBER OF (LINES, & BUSES).
 9,10

>>WANT TO TYPE IN NEW(LINE DATA, BUS DATA, OR GENERATOR DATA,
 OR CALCULATE Y/ZBUS MATRIX)?
 NNNY

GENERATOR DATA

>>ENTER(BUS#,ALPHA,BETA,GAMMA).

1,2.5,5.2,0.02

2,2.0,4.3,0.01

3,2.3,4.8,0.02

GENERATOR CONSTRAINT DATA

>>ENTER FOR TYPE -1 & -3 BUS (BUS #,PGMAX,PGMIN)

FOR TYPE -2 BUS (BUS #,PGMAX,PGMIN,OGMAX,OGMIN)

FOR TYPE +2 BUS (BUS #,OGMAX,OGMIN)

1,0.75,0.0,2.0,0.0

2,2.0,4.3,0.01,10.0,3.4,0.2,3.0,0.0

3,1.0,0.0,2.0,-2.0

9,2.0,-2.0,0.2,0.0

10,2.0,0.0

>>WANT A COPY OF (LDATA,BDATA,GDATA,OR SYSTEM CONVERGENCE CRITERIA)?
 YYYYY

SYSTEM LINE DATA

LINE #	SB	EB	LENGTH	Y SHUNT		Z SERIES	
1	1	7	0.22000E+02	0.00000E+00	0.00000E+00	0.27410E-02	0.58522E-02
2	2	4	0.25000E+02	0.00000E+00	0.00000E+00	0.11720E-02	0.00000E+00
3	3	6	0.23000E+02	0.00000E+00	0.00000E+00	0.27505E-02	0.58270E-02
4	4	5	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.62000E-01
5	5	6	0.90000E+01	0.00000E+00	0.92535E-03	0.15123E-02	0.17958E-02
6	4	8	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.62000E-01
7	6	9	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.46000E-01
8	7	10	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.46000E-01
9	8	10	0.70000E+01	0.00000E+00	0.92535E-03	0.15123E-02	0.17958E-02

SYSTEM BUS DATA

BUS	TYPE	PG	DG	PD	QD	VMAG	VANG
1	-2	0.80000	0.50000	0.00000	0.00000	1.05000	0.00000
2	-3	1.50000	0.30000	0.00000	0.00000	1.05000	0.00000
3	-2	0.70000	0.20000	0.00000	0.00000	1.05000	0.00000
4	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
5	1	0.00000	0.00000	0.70000	0.10000	1.00000	0.00000
6	1	0.00000	0.00000	0.50000	0.10000	1.00000	0.00500
7	1	0.00000	0.00000	0.50000	0.30000	1.00000	0.00000
8	1	0.00000	0.00000	0.30000	0.20000	1.00000	0.00000
9	2	0.00000	0.00000	0.20000	0.10000	1.00000	0.00000
10	2	0.00000	0.00000	0.30000	0.30000	1.00000	0.00000

SYSTEM GENERATOR DATA

NUMBER OF GENERATORS = 3

BUS#	ALPHA	BETA	GAMMA
1	2.50000	5.20000	0.02000
2	2.00000	4.30000	0.01000
3	2.30000	4.80000	0.02000

GENERATOR CONSTRAINTS

BUS #	PGMAX	PGMIN	DGMAX	DGMIN
1	0.7500	0.0000	2.0000	0.0000
2	3.0000	0.0000		
3	1.0000	0.0000	2.0000	-2.0000
9			2.0000	0.0000
10			2.0000	0.0000

SYSTEM CONVERGENCE CRITERIA

LOAD FLOW ITERATIONS= 5
 LOAD FLOW TOLERANCE= 0.10000E-03
 ECON DISP ITERATIONS= 50
 ESP1= 0.10000E-02
 ESP2= 0.10000E-02

>>WANT TO CHANGE (LDATA,BDATA,GDATA, OR CONVERGENCE CRITERIA)?
 NNNN

GENERATING YBUS MATRIX

CALCULATING ZBUS MATRIX

>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?
 NN

SOLVING LOAD FLOW EQUATIONS BY NR

***NR CONVERGENCE IN 2 ITERATIONS

***OPTIMIZING COST FUNCTIONS**

LAMBDA DETERMINED IN 15 ITERATIONS

***SOLVING LOAD FLOW EQUATIONS BY NR**
 ****NR CONVERGENCE IN 2 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 5 ITERATIONS

***SOLVING LOAD FLOW EQUATIONS BY NR**
 ****NR CONVERGENCE IN 1 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 1 ITERATIONS

***SOLVING LOAD FLOW EQUATIONS BY NR**
 ****NR CONVERGENCE IN 1 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 0 ITERATIONS

>>TYPE CODE # FOR DESIRED ACTION
 1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
 AND SYSTEM OPERATING COST.
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

2

****SYSTEM BUS AND GENERATOR SOLUTIONS****
 ECON. DISPATCH CONVERGENCE IN 4 ITERATIONS
 ESP1= 0.0010, ESP2= 0.0010, LAMBDA= 6.9125
 SYSTEM LOSSES(PU)= 0.1101, SYSTEM LOAD(PU)= 2.5000

BUS#	BTYPE	IC	ITL	PG	QG	PD	QD	VMAG	VANG
1	-2	6.3424	0.0825	0.7362	0.1681	0.0000	0.0000	1.0500	0.0804
2	-3	6.5350	0.0546	1.0523	0.6111	0.0000	0.0000	1.0500	0.0000
3	-2	6.2532	0.0954	0.8216	0.0340	0.0000	0.0000	1.0500	0.0859
4	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0208	0.0167
5	1	0.0000	0.0000	0.0000	0.0000	0.7000	0.1000	1.0032	-0.0207
6	1	0.0000	0.0000	0.0000	0.0000	0.5000	0.1000	1.0015	-0.0170
7	1	0.0000	0.0000	0.0000	0.0000	0.5000	0.3000	0.9908	0.0021
8	1	0.0000	0.0000	0.0000	0.0000	0.3000	0.2000	1.0022	-0.0072
9	2	0.0000	0.0000	0.0000	0.0693	0.2000	0.1000	1.0000	-0.0262
10	2	0.0000	0.0000	0.0000	0.3987	0.3000	0.3000	1.0000	-0.0074

****SYSTEM OPERATING COST****
 GEN.# 1= 3.25P.U.
 GEN.# 2= 4.49P.U.
 GEN.# 3= 3.51P.U.
 TOTAL SYSTEM OPERATING COST = .11.25P.U.

****LINE POWER FLOW****

LINE#	SB	EB	REAL POWER	REACTIVE POWER
1	1	7	0.7362	0.1681
1	7	1	-0.7050	-0.1038
2	2	4	1.0523	0.6111
2	4	2	-1.0130	-0.6111
3	3	6	0.8216	0.0340
3	6	3	-0.7828	0.0482
4	4	5	0.6178	0.3012
4	5	4	-0.6178	-0.2731
5	5	6	-0.0822	0.1731
5	6	5	0.0828	-0.1808
6	4	8	0.3952	0.3100
6	8	4	-0.3952	-0.2950

7	6	9	0.2000	0.0326
7	9	6	-0.2000	-0.0307
8	7	10	0.2050	-0.1962
8	10	7	-0.2050	0.2000
9	8	10	0.0952	0.0950
9	10	8	-0.0950	-0.1012

>>TYPE CODE # FOR DESIRED ACTION

1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
 AND SYSTEM OPERATING COST.
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

4

>>WANT TO CHANGE (LDATA,BDATA,GDATA, OR CONVERGENCE CRITERIA)?
 NNYN

GENERATOR DATA CHANGES

>>ENTER (VARIABLE #, BUS #, NEW VALUE THEN 'CR')

1=ALPHA
 2=BETA
 3=GAMMA
 4=PGMAX
 5=PGMIN
 6=OGMAX
 7=OGMIN
 8=RETYPE ALL GENERATOR DATA
 9=UPDATE SOS FILE WITH CHANGES
 >>ENTER 0 THEN 'CR' WHEN CHANGES COMPLETED.

4,1,.8

PGMAX(BUS # 1)= 0.80000E+00

5,1,.8

PGMIN(BUS # 1)= 0.80000E+00

4,3,.7

PGMAX(BUS # 3)= 0.70000E+00

5,3,.7

PGMIN(BUS # 3)= 0.70000E+00

0

>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?
 NN

SOLVING LOAD FLOW EQUATIONS BY NR

***NR CONVERGENCE IN 0 ITERATIONS

OPTIMIZING COST FUNCTIONS

LAMBDA DETERMINED IN 12 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR

***NR CONVERGENCE IN 2 ITERATIONS

OPTIMIZING COST FUNCTIONS

LAMBDA DETERMINED IN 2 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR

***NR CONVERGENCE IN 1 ITERATIONS

OPTIMIZING COST FUNCTIONS

LAMBDA DETERMINED IN 0 ITERATIONS

>>TYPE CODE # FOR DESIRED ACTION
 1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
 AND SYSTEM OPERATING COST.
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

2

****SYSTEM BUS AND GENERATOR SOLUTIONS****
 ECON. DISPATCH CONVERGENCE IN 3 ITERATIONS
 ESP1= 0.0010, ESP2= 0.0010, LAMBDA= 7.1875

SYSTEM LOSSES(PU)= 0.1057, SYSTEM LOAD(PU)= 2.5000

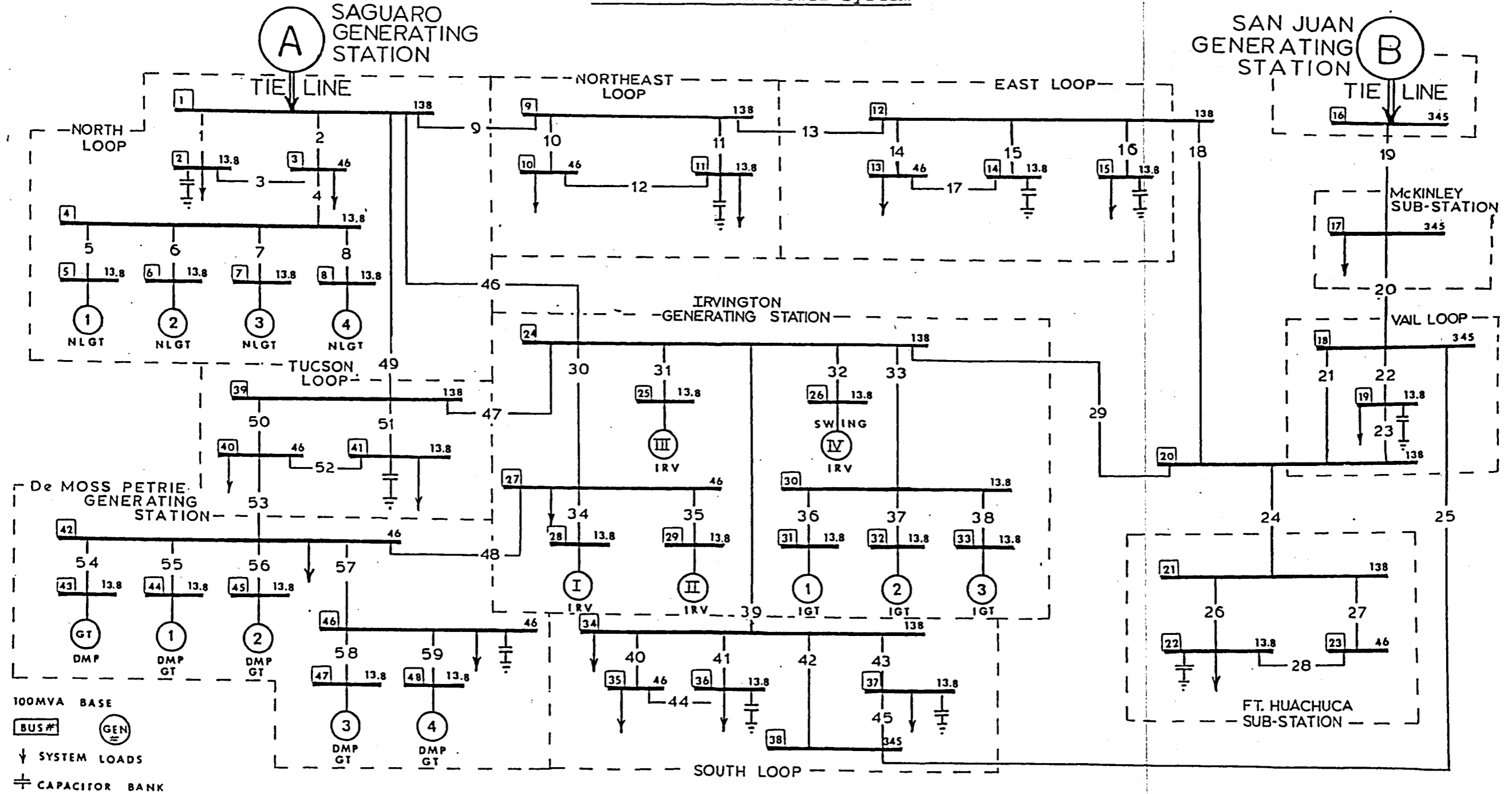
BUS#	BTYPE	IC	ITL	PG	QG	PD	QD	VMAG	VANG
1	-2	6.5313	0.0913	0.8000	0.1534	0.0000	0.0000	1.0500	0.0944
2	-3	6.7706	0.0580	1.1057	0.5551	0.0000	0.0000	1.0500	0.0000
3	-2	5.6698	0.0789	0.7000	0.0737	0.0000	0.0000	1.0500	0.0572
4	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0193	0.0152
5	1	0.0000	0.0000	0.0000	0.0000	0.7000	0.1000	1.0045	-0.0289
6	1	0.0000	0.0000	0.0000	0.0000	0.5000	0.1000	1.0020	-0.0277
7	1	0.0000	0.0000	0.0000	0.0000	0.5000	0.3000	0.9896	0.0075
8	1	0.0000	0.0000	0.0000	0.0000	0.3000	0.2000	1.0015	-0.0052
9	2	0.0000	0.0000	0.0000	0.0568	0.2000	0.1000	1.0000	-0.0369
10	2	0.0000	0.0000	0.0000	0.4368	0.3000	0.3000	1.0000	-0.0048

****SYSTEM OPERATING COST****
 GEN.# 1= 3.67P.U.
 GEN.# 2= 4.84P.U.
 GEN.# 3= 2.79P.U.
 TOTAL SYSTEM OPERATING COST = 11.30P.U.

****LINE POWER FLOW****

LINE#	SB	EB	REAL POWER	REACTIVE POWER
1	1	7	0.8000	0.1534
1	7	1	-0.7637	-0.0785
2	2	4	1.1057	0.5551
2	4	2	-1.0650	-0.5551
3	3	6	0.7000	0.0737
3	6	3	-0.6716	-0.0134
4	4	5	0.7287	0.2593
4	5	4	-0.7287	-0.2236
5	5	6	0.0287	0.1236
5	6	5	-0.0284	-0.1317
6	4	8	0.3364	0.2958
6	8	4	-0.3364	-0.2838
7	6	9	0.2000	0.0451
7	9	6	-0.2000	-0.0432
8	7	10	0.2637	-0.2215
8	10	7	-0.2637	0.2270
9	8	10	0.0364	0.0838
9	10	8	-0.0363	-0.0902

Problem 3: TGE Power System



.RUN EDSP50C3733,547J WITH MODERATE SYSTEM LOAD OF 6.85 pu

****ECONOMIC DISPATCH EXECUTIVE PROGRAM****

>>ENTER TYPE PROBLEM
 0=LOAD FLOW PROBLEM
 1=ECONOMIC DISPATCH PROBLEM

0

>>ENTER TOTAL NUMBER OF (LINES, & BUSES).
 59,48

>>WANT TO TYPE IN NEW(LINE DATA, BUS DATA, OR GENERATOR DATA,
 OR CALCULATE Y/ZBUS MATRIX)?
 NNNN

>>WANT A COPY OF (LDATA,BDATA,GDATA,OR SYSTEM CONVERGENCE CRITERIA)?
 YYYY

```

**SYSTEM LINE DATA**
LINE # SB EB LENGTH Y SHUNT Z SERIES
 1 1 2 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.19100E+00
 2 1 3 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.10600E+00
 3 2 3 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.62000E-01
 4 3 4 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.95500E+00
 5 4 5 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.67190E+00
 6 4 6 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.67190E+00
 7 4 7 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.67190E+00
 8 4 8 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.67190E+00
 9 1 9 0.10000E+01 0.00000E+00 0.82000E-02 0.10700E-01 0.62300E-01
10 9 10 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.70400E+00
11 9 11 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.13040E+00
12 10 11 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.45000E-01
13 9 12 0.10000E+01 0.00000E+00 0.50000E-02 0.47000E-02 0.62300E-01
14 12 13 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.10760E+00
15 12 14 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.19210E+00
16 12 15 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.87500E-01
17 13 14 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.61700E-01
18 12 20 0.10000E+01 0.00000E+00 0.80000E-02 0.13500E-01 0.78300E-01
19 16 17 0.10000E+01 0.00000E+00 0.39400E+00 0.40000E-02 0.43400E-01
20 17 18 0.10000E+01 0.00000E+00 0.14172E+01 0.14100E-01 0.15260E+00
21 18 20 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.16500E-01
22 18 19 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.14940E+00
23 19 20 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.10710E+00
24 20 21 0.10000E+01 0.00000E+00 0.20000E+00 0.55400E-01 0.21170E+00
25 18 38 0.10000E+01 0.00000E+00 0.58300E-01 0.60000E-03 0.65000E-02
26 21 22 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.52440E+00
27 21 23 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.27400E+00
28 22 23 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.20500E+00
29 20 24 0.10000E+01 0.00000E+00 0.92000E-02 0.35800E-02 0.20970E-01
30 24 27 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.12500E+00
31 24 25 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.19320E+00
32 24 26 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.11750E+00
33 24 30 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.24580E+00
34 27 28 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.18650E+00
35 27 29 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.17720E+00
36 30 31 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.43030E+00
37 30 32 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.43030E+00
38 30 33 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.43030E+00
39 24 34 0.10000E+01 0.00000E+00 0.15700E-01 0.60000E-02 0.31300E-01
40 34 35 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.93800E-01
41 34 36 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.16810E+00
42 34 38 0.10000E+01 0.00000E+00 0.00000E+00 0.00000E+00 0.16500E-01

```

43	34	37	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.14940E+00
44	35	36	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.58100E-01
45	37	38	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.10710E+00
46	1	24	0.10000E+01	0.00000E+00	0.12500E-01	0.17700E-01	0.10580E+00
47	24	39	0.10000E+01	0.00000E+00	0.52000E-02	0.73000E-02	0.42700E-01
48	27	42	0.10000E+01	0.00000E+00	0.00000E+00	0.44000E-01	0.26220E+00
49	1	39	0.10000E+01	0.00000E+00	0.75000E-02	0.10400E-01	0.60700E-01
50	39	40	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.21620E+00
51	39	41	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.12770E+00
52	40	41	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.68100E-01
53	40	42	0.10000E+01	0.00000E+00	0.00000E+00	0.73000E-02	0.54400E-01
54	42	43	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.33320E+00
55	42	44	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.86280E+00
56	42	45	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.31110E+00
57	42	46	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.16700E+00
58	46	47	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.54310E+00
59	46	48	0.10000E+01	0.00000E+00	0.00000E+00	0.00000E+00	0.84610E+00

SYSTEM BUS DATA

BUS	TYPE	FG	GG	PD	GD	UMAG	VANG
1	-2	1.10000	0.20000	0.00000	0.00000	1.05000	0.00000
2	2	0.00000	0.00000	0.06000	0.02000	1.00000	0.00000
3	1	0.00000	0.00000	0.35000	0.13000	1.00000	0.00000
4	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
5	-2	0.15000	0.20000	0.00000	0.00000	1.00000	0.00000
6	-2	0.15000	0.20000	0.00000	0.00000	1.00000	0.00000
7	-2	0.25000	0.20000	0.00000	0.00000	1.00000	0.00000
8	-2	0.25000	0.20000	0.00000	0.00000	1.00000	0.00000
9	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
10	1	0.00000	0.00000	0.92000	0.21000	1.00000	0.00000
11	2	0.00000	0.00000	0.07000	0.01500	1.00000	0.00000
12	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
13	1	0.00000	0.00000	0.72000	0.24000	1.00000	0.00000
14	2	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
15	2	0.00000	0.00000	0.37000	0.13000	1.00000	0.00000
16	-2	1.65000	0.00000	0.00000	0.00000	1.01450	0.00000
17	1	0.00000	0.00000	0.26000	0.04000	1.00000	0.00000
18	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
19	2	0.00000	0.00000	0.02000	0.01800	1.00000	0.00000
20	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
21	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
22	2	0.00000	0.10000	0.25000	0.05000	1.00000	0.00000
23	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
24	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
25	-2	0.50000	0.20000	0.00000	0.00000	1.00000	0.00000
26	-3	1.20000	0.20000	0.00000	0.00000	1.00000	0.00000
27	1	0.00000	0.00000	1.12000	0.60000	1.00000	0.00000
28	-2	0.26000	0.20000	0.00000	0.00000	1.00000	0.00000
29	-2	0.25000	0.20000	0.00000	0.00000	1.00000	0.00000
30	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
31	-1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
32	-1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
33	-1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
34	1	0.00000	0.00000	0.20000	0.35000	1.00000	0.00000
35	1	0.00000	0.00000	0.31000	0.34000	1.00000	0.00000
36	2	0.00000	0.00000	0.25000	0.01000	1.00000	0.00000
37	2	0.00000	0.00000	0.34000	0.25000	1.00000	0.00000
38	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
39	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
40	1	0.00000	0.00000	0.42000	0.15000	1.00000	0.00000
41	2	0.00000	0.20000	0.36000	0.12000	1.00000	0.00000
42	1	0.00000	0.00000	0.61000	0.21000	1.00000	0.00000
43	-2	0.48100	0.20000	0.00000	0.00000	1.00000	0.00000
44	-2	0.14000	0.00000	0.00000	0.00000	1.00000	0.00000

45	-2	0.13000	0.00000	0.00000	0.00000	1.00000	0.00000
46	2	0.00000	0.00000	0.22000	0.07000	1.00000	0.00000
47	-2	0.24500	0.10000	0.00000	0.00000	1.00000	0.00000
48	-2	0.46000	0.15000	0.00000	0.00000	1.00000	0.00000

GENERATOR CONSTRAINTS

BUS #	PGMAX	PGMIN	QGMAX	QGMIN
1	1.1000	0.0000	0.2000	-2.0000
2			2.0000	-2.0000
5	0.2510	0.0000	2.0000	-2.0000
6	0.2510	0.0000	2.0000	-2.0000
7	0.2510	0.0000	2.0000	-2.0000
8	0.2510	0.0000	2.0000	-2.0000
11			0.8000	-2.0000
14			0.4000	-2.0000
15			0.4000	-2.0000
16	1.6500	0.0000	2.0000	-2.0000
19			0.4500	-2.0000
22			0.2400	-2.0000
25	1.0900	0.0000	2.0000	-2.0000
26	1.5900	0.0000		
28	0.7700	0.0000	2.0000	-2.0000
29	0.7900	0.0000	2.0000	-2.0000
31	0.2490	0.0000		
32	0.2490	0.0000		
33	0.2490	0.0000		
36			0.4000	-2.0000
37			0.4300	-2.0000
41			0.4000	-2.0000
43	0.4810	0.0000	0.4500	-2.0000
44	0.1480	0.0000	0.1500	-2.0000
45	0.1320	0.0000	0.1400	-2.0000
46			0.3600	-2.0000
47	0.2450	0.0000	0.2500	-2.0000
48	0.4680	0.0000	0.4500	-2.0000

SYSTEM CONVERGENCE CRITERIA

LOAD FLOW ITERATIONS= 5
LOAD FLOW TOLERANCE= 0.10000E-03
ECON DISP ITERATIONS= 50
ESP1= 0.10000E-02
ESP2= 0.10000E-02

>>WANT TO CHANGE (LDATA,BDATA,GDATA, OR CONVERGENCE CRITERIA)?
NNNN\NNNN\YYYY

** LINE DATA CHANGES**

>>ENTER (VARIABLE #, LINE #, NEW VALUE THEN 'CR')
1=STARTING BUS #
2=ENDING BUS #
3=LINE LENGTH
4=Y SHUNT G
5=Y SHUNT B
6=Z SERIES R
7=Z SERIES X
8=RETYPE COPY OF ALL LINE DATA
9=CHANGE TOTAL NUMBER OF LINES
10=UPDATE SOS FILE WITH CHANGES
>>ENTER 0 THEN 'CR' WHEN CHANGES COMPLETED

0

```

**BUS DATA CHANGES**
>>ENTER(VARIABLE #, BUS #, NEW VALUE THEN 'CR'
    1=BUS TYPE
    2=PG
    3=QG
    4=PD
    5=QD
    6=VMAG
    7=VANG
    8=RETYPE COPY OF ALL BUS DATA
    9=CHANGE TOTAL NUMBER OF BUSES
    10=REENTER ORIGINAL BUS DATA FROM SOS FILE
    11=UPDATE SOS FILE WITH CHANGES
>>ENTER 0 THEN 'CR' WHEN CHANGES COMPLETED.

```

0

```

**GENERATOR DATA CHANGES**
>>ENTER (VARIABLE #, BUS #, NEW VALUE THEN 'CR')
    1=ALPHA
    2=BETA
    3=GAMMA
    4=PGMAX
    5=PGMIN
    6=QGMAX
    7=QGMIN
    8=RETYPE ALL GENERATOR DATA
    9=UPDATE SOS FILE WITH CHANGES
>>ENTER 0 THEN 'CR' WHEN CHANGES COMPLETED.

```

0

```

**CONVERGENCE CRITERIA CHANGES**
>>ENTER(VARIABLE #,NEW VALUE THEN 'CR')
    1=LOAD FLOW ITERATIONS
    2=LOAD FLOW TOLERANCE
    3=ECON DISP ITERATIONS
    4=ESP1
    5=ESP2
>>ENTER 0 THEN 'CR' WHEN CHANGES COMPLETED.

```

0

****GENERATING YBUS MATRIX****

```

>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?
NN

```

```

**SOLVING LOAD FLOW EQUATIONS BY NR**
BUS # 1 EXCEEDS QGMAX,BUS CHANGED TO TYPE 1
****NR CONVERGENCE IN 4 ITERATIONS

```

```

>>TYPE CODE # FOR DESIRED ACTION
    1=PRINT BUS & GEN SOLUTIONS ONLY.
    2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
      AND SYSTEM OPERATING COST.
    3=CREATE SOS FILE OF SOLUTIONS
    4=CHANGE DATA OR TOLERANCES AND RERUN
    5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
      RERUN WITH EXISTING DATA
    6=NEW PROBLEM
    7=TERMINATE

```

2

****SYSTEM BUS AND GENERATOR SOLUTIONS****

SYSTEM LOSSES(PU)= 0.0746, SYSTEM LOAD(PU)= 6.8500

BUS #	BTYPE	PG	QG	PD	QD	VMAG	VANG
1	-1	1.1000	0.2000	0.0000	0.0000	0.9981	-0.0997
2	2	0.0000	0.4621	0.0600	0.0200	1.0000	-0.0794
3	1	0.0000	0.0000	0.3500	0.1300	0.9733	-0.0688
4	1	0.0000	0.0000	0.0000	0.0000	0.9156	0.9612
5	-2	0.1500	0.1339	0.0000	0.0000	1.0000	1.0715
6	-2	0.1500	0.1339	0.0000	0.0000	1.0000	1.0715
7	-2	0.2500	0.1488	0.0000	0.0000	1.0000	1.1457
8	-2	0.2500	0.1488	0.0000	0.0000	1.0000	1.1457
9	1	0.0000	0.0000	0.0000	0.0000	0.9883	-0.1762
10	1	0.0000	0.0000	0.9200	0.2100	0.9892	-0.3148
11	2	0.0000	0.3979	0.0700	0.0150	1.0000	-0.2817
12	1	0.0000	0.0000	0.0000	0.0000	0.9909	-0.1893
13	1	0.0000	0.0000	0.7200	0.2400	0.9865	-0.2448
14	2	0.0000	0.2717	0.0000	0.0000	1.0000	-0.2313
15	2	0.0000	0.2401	0.3700	0.1300	1.0000	-0.2220
16	-2	1.6500	-0.7939	0.0000	0.0000	1.0145	0.1620
17	1	0.0000	0.0000	0.2600	0.0400	1.0359	0.0915
18	1	0.0000	0.0000	0.0000	0.0000	1.0061	-0.1087
19	2	0.0000	-0.0486	0.0200	0.0180	1.0000	-0.1159
20	1	0.0000	0.0000	0.0000	0.0000	1.0028	-0.1189
21	1	0.0000	0.0000	0.0000	0.0000	1.0038	-0.1758
22	2	0.0000	0.0427	0.2500	0.0500	1.0000	-0.2381
23	1	0.0000	0.0000	0.0000	0.0000	1.0011	-0.2114
24	1	0.0000	0.0000	0.0000	0.0000	0.9980	-0.1072
25	-2	0.5000	0.0346	0.0000	0.0000	1.0000	-0.0102
26	-3	0.9086	0.0657	0.0000	0.0000	1.0000	0.0000
27	1	0.0000	0.0000	1.1200	0.6000	0.9666	-0.1617
28	-2	0.2600	0.1859	0.0000	0.0000	1.0000	-0.1115
29	-2	0.2500	0.1945	0.0000	0.0000	1.0000	-0.1159
30	1	0.0000	0.0000	0.0000	0.0000	0.9980	-0.1072
31	-1	0.0000	0.0000	0.0000	0.0000	0.9980	-0.1072
32	-1	0.0000	0.0000	0.0000	0.0000	0.9980	-0.1072
33	-1	0.0000	0.0000	0.0000	0.0000	0.9980	-0.1072
34	1	0.0000	0.0000	0.2000	0.3500	0.9959	-0.1204
35	1	0.0000	0.0000	0.3100	0.3400	0.9858	-0.1537
36	2	0.0000	0.2821	0.2500	0.0100	1.0000	-0.1560
37	2	0.0000	0.2542	0.3400	0.2500	1.0000	-0.1372
38	1	0.0000	0.0000	0.0000	0.0000	1.0029	-0.1129
39	1	0.0000	0.0000	0.0000	0.0000	0.9961	-0.1128
40	1	0.0000	0.0000	0.4200	0.1500	0.9855	-0.1357
41	2	0.0000	0.3674	0.3600	0.1200	1.0000	-0.1439
42	1	0.0000	0.0000	0.6100	0.2100	0.9832	-0.1106
43	-2	0.4810	0.0899	0.0000	0.0000	1.0000	0.0532
44	-2	0.1400	0.0281	0.0000	0.0000	1.0000	0.0126
45	-2	0.1300	0.0567	0.0000	0.0000	1.0000	-0.0694
46	2	0.0000	0.3003	0.2200	0.0700	1.0000	-0.0281
47	-2	0.2450	0.0164	0.0000	0.0000	1.0000	0.1053
48	-2	0.4600	0.0932	0.0000	0.0000	1.0000	0.3717

****LINE POWER FLOW****

LINE#	SB	EB	REAL POWER	REACTIVE POWER
1	1	2	-0.1064	-0.0086
1	2	1	0.1064	0.0108
2	1	3	-0.2836	0.2381
2	3	1	0.2836	-0.2236
3	2	3	-0.1664	0.4312
3	3	2	0.1664	-0.4180
4	3	4	-0.8000	0.5116
4	4	3	0.8000	0.3974

5	4	5	-0.1500	-0.1068
5	5	4	0.1500	0.1339
6	4	6	-0.1500	-0.1068
6	6	4	0.1500	0.1339
7	4	7	-0.2500	-0.0919
7	7	4	0.2500	0.1488
8	4	8	-0.2500	-0.0919
8	8	4	0.2500	0.1488
9	1	9	1.2084	-0.0082
9	9	1	-1.1927	0.0914
10	9	10	0.1919	0.0120
10	10	9	-0.1919	0.0146
11	9	11	0.7981	-0.0463
11	11	9	-0.7981	0.1316
12	10	11	-0.7281	-0.2246
12	11	10	0.7281	0.2513
13	9	12	0.2027	-0.0571
13	12	9	-0.2025	0.0550
14	12	13	0.5037	0.0542
14	13	12	-0.5037	-0.0261
15	12	14	0.2163	-0.0424
15	14	12	-0.2163	0.0519
16	12	15	0.3700	-0.0971
16	15	12	-0.3700	0.1101
17	13	14	-0.2163	-0.2139
17	14	13	0.2163	0.2198
18	12	20	-0.8875	0.0303
18	20	12	0.8984	0.0247
19	16	17	1.6500	-0.7939
19	17	16	-1.6381	0.5093
20	17	18	1.3781	-0.5493
20	18	17	-1.3525	-0.6519
21	18	20	0.6206	0.2064
21	20	18	-0.6206	-0.1994
22	18	19	0.0481	0.0413
22	19	18	-0.0481	-0.0407
23	19	20	0.0281	-0.0259
23	20	19	-0.0281	0.0260
24	20	21	0.2538	-0.1640
24	21	20	-0.2500	-0.0229
25	18	38	0.6838	0.4042
25	38	18	-0.6835	-0.4588
26	21	22	0.1193	0.0109
26	22	21	-0.1193	-0.0035
27	21	23	0.1307	0.0120
27	23	21	-0.1307	-0.0073
28	22	23	-0.1307	-0.0038
28	23	22	0.1307	0.0073
29	20	24	-0.5035	0.3127
29	24	20	0.5047	-0.3145
30	24	27	0.4206	0.2626
30	27	24	-0.4206	-0.2317
31	24	25	-0.5000	0.0139
31	25	24	0.5000	0.0346
32	24	26	-0.9086	0.0318
32	26	24	0.9086	0.0657
33	24	30	-0.0000	0.0000
33	30	24	0.0000	0.0000
34	27	28	-0.2600	-0.1668
34	28	27	0.2600	0.1859
35	27	29	-0.2500	-0.1767
35	29	27	0.2500	0.1945
36	30	31	-0.0000	0.0000
36	31	30	0.0000	0.0000

37	30	32	-0.0000	0.0000
37	32	30	0.0000	0.0000
38	30	33	-0.0000	0.0000
38	33	30	0.0000	0.0000
39	24	34	0.4176	-0.0173
39	34	24	-0.4165	0.0072
40	34	35	0.3489	0.1124
40	35	34	-0.3489	-0.0997
41	34	36	0.2111	-0.0207
41	36	34	-0.2111	0.0283
42	34	38	-0.4555	-0.4224
42	38	34	0.4555	0.4289
43	34	37	0.1121	-0.0265
43	37	34	-0.1121	0.0285
44	35	36	0.0389	-0.2403
44	36	35	-0.0389	0.2438
45	37	38	-0.2279	-0.0244
45	38	37	0.2279	0.0300
46	1	24	0.0684	-0.0161
46	24	1	-0.0683	0.0042
47	24	39	0.1340	0.0194
47	39	24	-0.1338	-0.0238
48	27	42	-0.1894	-0.0248
48	42	27	0.1911	0.0350
49	1	39	0.2132	-0.0053
49	39	1	-0.2128	0.0006
50	39	40	0.1042	0.0499
50	40	39	-0.1042	-0.0470
51	39	41	0.2424	-0.0267
51	41	39	-0.2424	0.0343
52	40	41	0.1176	-0.2091
52	41	40	-0.1176	0.2131
53	40	42	-0.4334	0.1061
53	42	40	0.4349	-0.0949
54	42	43	-0.4810	-0.0101
54	43	42	0.4810	0.0899
55	42	44	-0.1400	-0.0105
55	44	42	0.1400	0.0281
56	42	45	-0.1300	-0.0505
56	45	42	0.1300	0.0567
57	42	46	-0.4850	-0.0790
57	46	42	0.4850	0.1207
58	46	47	-0.2450	0.0164
58	47	46	0.2450	0.0164
59	46	48	-0.4600	0.0932
59	48	46	0.4600	0.0932

>>TYPE CODE # FOR DESIRED ACTION

1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
 AND SYSTEM OPERATING COST.
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

5

ECONOMIC DISPATCH EXECUTIVE PROGRAM

>>ENTER TYPE PROBLEM

0=LOAD FLOW PROBLEM
 1=ECONOMIC DISPATCH PROBLEM

1

>>IS SYSTEM LOSSLESS?
NO

>>ENTER TOTAL NUMBER OF (LINES, & BUSES).
59,48

>>WANT TO TYPE IN NEW(LINE DATA, BUS DATA, OR GENERATOR DATA,
OR CALCULATE Y/ZBUS MATRIX)?
NNNY

>>WANT A COPY OF (LDATA,BDATA,GDATA,OR SYSTEM CONVERGENCE CRITERIA)?
NNYN

SYSTEM GENERATOR DATA
NUMBER OF GENERATORS = 18

BUS#	ALPHA	BETA	GAMMA
1	0.00000	0.00000	0.00000
5	9.56170	5.52200	-2.12000
6	9.56170	5.52200	-2.12000
7	9.56170	5.52200	-2.12000
8	9.56170	5.52200	-2.12000
16	0.00000	0.00000	0.00000
25	8.70820	1.24000	0.08900
26	8.39970	0.42050	0.13000
28	8.80940	1.00100	0.44100
29	7.98410	2.78000	0.17000
31	9.56170	5.52200	-2.12000
32	9.56170	5.52200	-2.12000
33	9.56170	5.52200	-2.12000
43	9.46170	4.52200	-2.12000
44	9.20980	13.87000	19.33000
45	9.20980	12.87000	18.33000
47	9.56170	5.52200	-2.12000
48	9.51170	5.22200	-2.12000

GENERATOR CONSTRAINTS

BUS #	PGMAX	PGMIN	QGMAX	QGMIN
1	1.1000	0.0000	0.2000	-2.0000
2			2.0000	-2.0000
5	0.2510	0.0000	2.0000	-2.0000
6	0.2510	0.0000	2.0000	-2.0000
7	0.2510	0.0000	2.0000	-2.0000
8	0.2510	0.0000	2.0000	-2.0000
11			0.8000	-2.0000
14			0.4000	-2.0000
15			0.4000	-2.0000
16	1.6500	0.0000	2.0000	-2.0000
19			0.4500	-2.0000
22			0.2400	-2.0000
25	1.0900	0.0000	2.0000	-2.0000
26	1.5900	0.0000		
28	0.7700	0.0000	2.0000	-2.0000
29	0.7900	0.0000	2.0000	-2.0000
31	0.2490	0.0000		
32	0.2490	0.0000		
33	0.2490	0.0000		
36			0.4000	-2.0000
37			0.4300	-2.0000
41			0.4000	-2.0000
43	0.4810	0.0000	0.4500	-2.0000
44	0.1480	0.0000	0.1500	-2.0000
45	0.1320	0.0000	0.1400	-2.0000
46			0.3600	-2.0000

47	0.2450	0.0000	0.2500	-2.0000
48	0.4680	0.0000	0.4500	-2.0000

>>WANT TO CHANGE (LDATA,BDATA,GDATA, OR CONVERGENCE CRITERIA)?
NNNN

GENERATING YBUS MATRIX
 CALCULATING ZBUS MATRIX
 [Exceeding quota on STDN]
 [Exceeding quota on STDN]

>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?
NN

SOLVING LOAD FLOW EQUATIONS BY NR
 BUS # 1 EXCEEDS QGMAX,BUS CHANGED TO TYPE 1
 ****NR CONVERGENCE IN 3 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 20 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR
 BUS # 41 EXCEEDS QGMAX,BUS CHANGED TO TYPE 1
 BUS # 1 EXCEEDS QGMAX,BUS CHANGED TO TYPE 1
 ****NR CONVERGENCE IN 4 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 16 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR
 BUS # 1 EXCEEDS QGMAX,BUS CHANGED TO TYPE 1
 BUS # 41 EXCEEDS QGMAX,BUS CHANGED TO TYPE 1
 ****NR CONVERGENCE IN 3 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 22 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR
 BUS # 1 EXCEEDS QGMAX,BUS CHANGED TO TYPE 1
 BUS # 41 EXCEEDS QGMAX,BUS CHANGED TO TYPE 1
 ****NR CONVERGENCE IN 2 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 21 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR
 BUS # 1 EXCEEDS QGMAX,BUS CHANGED TO TYPE 1
 BUS # 41 EXCEEDS QGMAX,BUS CHANGED TO TYPE 1
 ****NR CONVERGENCE IN 2 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 20 ITERATIONS

>>TYPE CODE # FOR DESIRED ACTION
 1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
 AND SYSTEM OPERATING COST.
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

****SYSTEM BUS AND GENERATOR SOLUTIONS****

ECON. DISPATCH CONVERGENCE IN 5 ITERATIONS

ESP1= 0.0010, ESP2= 0.0010, LAMBDA= 10.3902

SYSTEM LOSSES(PU)= 0.0889, SYSTEM LOAD(PU)= 6.8500

BUS#	BTYPE	IC	ITL	PG	QG	PD	QD	VMAG	VANG
1	-1	0.0000	0.0701	1.1000	0.2000	0.0000	0.0000	0.9990	-0.2242
2	2	0.0000	0.0000	0.0000	0.1162	0.0600	0.0200	1.0000	-0.2445
3	1	0.0000	0.0000	0.0000	0.0000	0.3500	0.1300	0.9944	-0.2474
4	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.9986	-0.1639
5	-2	9.6795	0.0684	0.0217	0.0023	0.0000	0.0000	1.0000	-0.1493
6	-2	9.6795	0.0684	0.0217	0.0023	0.0000	0.0000	1.0000	-0.1493
7	-2	9.6795	0.0684	0.0217	0.0023	0.0000	0.0000	1.0000	-0.1493
8	-2	9.6795	0.0684	0.0217	0.0023	0.0000	0.0000	1.0000	-0.1493
9	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.9893	-0.2882
10	1	0.0000	0.0000	0.0000	0.0000	0.9200	0.2100	0.9893	-0.4267
11	2	0.0000	0.0000	0.0000	0.3889	0.0700	0.0150	1.0000	-0.3936
12	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.9905	-0.2893
13	1	0.0000	0.0000	0.0000	0.0000	0.7200	0.2400	0.9864	-0.3448
14	2	0.0000	0.0000	0.0000	0.2762	0.0000	0.0000	1.0000	-0.3312
15	2	0.0000	0.0000	0.0000	0.2447	0.3700	0.1300	1.0000	-0.3220
16	-2	0.0000	-0.0204	1.6500	-0.7924	0.0000	0.0000	1.0145	0.0783
17	1	0.0000	0.0000	0.0000	0.0000	0.2600	0.0400	1.0358	0.0078
18	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0058	-0.1925
19	2	0.0000	0.0000	0.0000	-0.0436	0.0200	0.0180	1.0000	-0.2000
20	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0024	-0.2033
21	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0036	-0.2603
22	2	0.0000	0.0000	0.0000	0.0435	0.2500	0.0500	1.0000	-0.3227
23	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0011	-0.2959
24	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.9978	-0.1885
25	-2	9.8304	0.0539	0.8523	0.0824	0.0000	0.0000	1.0000	-0.0227
26	-3	9.3969	0.0533	1.5909	0.1694	0.0000	0.0000	1.0000	0.0000
27	1	0.0000	0.0000	0.0000	0.0000	1.1200	0.6000	0.9665	-0.2153
28	-2	9.7449	0.0621	0.7111	0.2285	0.0000	0.0000	1.0000	-0.0777
29	-2	9.7380	0.0628	0.6081	0.2229	0.0000	0.0000	1.0000	-0.1036
30	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.9966	-0.1560
31	-1	9.7998	0.0568	0.0437	0.0000	0.0000	0.0000	0.9964	-0.1371
32	-1	9.7998	0.0568	0.0437	0.0000	0.0000	0.0000	0.9964	-0.1371
33	-1	9.7998	0.0568	0.0437	0.0000	0.0000	0.0000	0.9964	-0.1371
34	1	0.0000	0.0000	0.0000	0.0000	0.2000	0.3500	0.9956	-0.2031
35	1	0.0000	0.0000	0.0000	0.0000	0.3100	0.3400	0.9857	-0.2365
36	2	0.0000	0.0000	0.0000	0.2857	0.2500	0.0100	1.0000	-0.2388
37	2	0.0000	0.0000	0.0000	0.2584	0.3400	0.2500	1.0000	-0.2204
38	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0027	-0.1963
39	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.9928	-0.2285
40	1	0.0000	0.0000	0.0000	0.0000	0.4200	0.1500	0.9843	-0.3203
41	1	0.0000	0.0000	0.0000	0.4000	0.3600	0.1200	0.9986	-0.3045
42	1	0.0000	0.0000	0.0000	0.0000	0.6100	0.2100	0.9787	-0.3324
43	-2	9.7315	0.0634	0.0614	0.0647	0.0000	0.0000	1.0000	-0.3115
44	-2	9.7331	0.0632	0.0359	0.0253	0.0000	0.0000	1.0000	-0.3007
45	-2	9.7303	0.0635	0.0383	0.0688	0.0000	0.0000	1.0000	-0.3202
46	2	0.0000	0.0000	0.0000	0.2006	0.2200	0.0700	1.0000	-0.3575
47	-2	9.7275	0.0638	0.0303	0.0003	0.0000	0.0000	1.0000	-0.3410
48	-2	9.7301	0.0635	0.0425	0.0008	0.0000	0.0000	1.0000	-0.3215

****SYSTEM OPERATING COST****

GEN.# 1= 0.00P.U.
 GEN.# 5= 0.21P.U.
 GEN.# 6= 0.21P.U.
 GEN.# 7= 0.21P.U.
 GEN.# 8= 0.21P.U.
 GEN.# 16= 0.00P.U.
 GEN.# 25= 7.89P.U.
 GEN.# 26= 14.07P.U.

GEN.# 28= 6.571P.U.
 GEN.# 29= 5.38P.U.
 GEN.# 31= 0.42P.U.
 GEN.# 32= 0.42P.U.
 GEN.# 33= 0.42P.U.
 GEN.# 43= 0.59P.U.
 GEN.# 44= 0.34P.U.
 GEN.# 45= 0.36P.U.
 GEN.# 47= 0.29P.U.
 GEN.# 48= 0.41P.U.
 TOTAL SYSTEM OPERATING COST = 38.01P.U.

****LINE POWER FLOW****

LINE#	SB	EB	REAL POWER	REACTIVE POWER
1	1	2	0.1061	-0.0042
1	2	1	-0.1061	0.0064
2	1	3	-0.2171	0.0454
2	3	1	0.2171	-0.0402
3	2	3	0.0461	0.0898
3	3	2	-0.0461	-0.0892
4	3	4	-0.0868	-0.0007
4	4	3	0.0868	0.0079
5	4	5	-0.0217	-0.0020
5	5	4	0.0217	0.0023
6	4	6	-0.0217	-0.0020
6	6	4	0.0217	0.0023
7	4	7	-0.0217	-0.0020
7	7	4	0.0217	0.0023
8	4	8	-0.0217	-0.0020
8	8	4	0.0217	0.0023
9	1	9	1.0164	0.0087
9	9	1	-1.0053	0.0477
10	9	10	0.1919	0.0134
10	10	9	-0.1919	0.0133
11	9	11	0.7981	-0.0389
11	11	9	-0.7981	0.1240
12	10	11	-0.7281	-0.2233
12	11	10	0.7281	0.2499
13	9	12	0.0154	-0.0221
13	12	9	-0.0153	0.0173
14	12	13	0.5037	0.0518
14	13	12	-0.5037	-0.0237
15	12	14	0.2163	-0.0445
15	14	12	-0.2163	0.0540
16	12	15	0.3700	-0.1016
16	15	12	-0.3700	0.1147
17	13	14	-0.2163	-0.2163
17	14	13	0.2163	0.2222
18	12	20	-1.0747	0.0769
18	20	12	1.0906	0.0078
19	16	17	1.6500	-0.7924
19	17	16	-1.6381	0.5077
20	17	18	1.3781	-0.5477
20	18	17	-1.3525	-0.6529
21	18	20	0.6631	0.2099
21	20	18	-0.6631	-0.2020
22	18	19	0.0509	0.0395
22	19	18	-0.0509	-0.0388
23	19	20	0.0309	-0.0228
23	20	19	-0.0309	0.0230
24	20	21	0.2538	-0.1646
24	21	20	-0.2500	-0.0222
25	18	38	0.6386	0.4035
25	38	18	-0.6382	-0.4585

26	21	22	0.1193	0.0106
26	22	21	-0.1193	-0.0031
27	21	23	0.1307	0.0116
27	23	21	-0.1307	-0.0069
28	22	23	-0.1307	-0.0034
28	23	22	0.1307	0.0069
29	20	24	-0.6505	0.3358
29	24	20	0.6524	-0.3338
30	24	27	0.2074	0.2521
30	27	24	-0.2074	-0.2387
31	24	25	-0.8523	0.0593
31	25	24	0.8523	0.0824
32	24	26	-1.5909	0.1313
32	26	24	1.5909	0.1694
33	24	30	-0.1312	0.0068
33	30	24	0.1312	-0.0025
34	27	28	-0.7111	-0.1245
34	28	27	0.7111	0.2285
35	27	29	-0.6081	-0.1486
35	29	27	0.6081	0.2229
36	30	31	-0.0437	0.0008
36	31	30	0.0437	0.0000
37	30	32	-0.0437	0.0008
37	32	30	0.0437	0.0000
38	30	33	-0.0437	0.0008
38	33	30	0.0437	0.0000
39	24	34	0.4631	-0.0241
39	34	24	-0.4618	0.0152
40	34	35	0.3489	0.1105
40	35	34	-0.3489	-0.0979
41	34	36	0.2111	-0.0223
41	36	34	-0.2111	0.0300
42	34	38	-0.4130	-0.4250
42	38	34	0.4130	0.4309
43	34	37	0.1148	-0.0284
43	37	34	-0.1148	0.0305
44	35	36	0.0389	-0.2421
44	36	35	-0.0389	0.2457
45	37	38	-0.2252	-0.0221
45	38	37	0.2252	0.0276
46	1	24	-0.3248	0.0657
46	24	1	0.3268	-0.0664
47	24	39	0.9249	-0.0251
47	39	24	-0.9186	0.0567
48	27	42	0.4065	-0.0883
48	42	27	-0.3983	0.1368
49	1	39	0.0851	0.0844
49	39	1	-0.0850	-0.0909
50	39	40	0.4145	0.0577
50	40	39	-0.4145	-0.0192
51	39	41	0.5891	-0.0234
51	41	39	-0.5891	0.0685
52	40	41	-0.2291	-0.2049
52	41	40	0.2291	0.2116
53	40	42	0.2235	0.0742
53	42	40	-0.2231	-0.0710
54	42	43	-0.0614	-0.0620
54	43	42	0.0614	0.0647
55	42	44	-0.0359	-0.0236
55	44	42	0.0359	0.0253
56	42	45	-0.0383	-0.0669
56	45	42	0.0383	0.0688
57	42	46	0.1471	-0.1232
57	46	42	-0.1471	0.1296

58	46	47	-0.0303	0.0003
58	47	46	0.0303	0.0003
59	46	48	-0.0425	0.0008
59	48	46	0.0425	0.0008

>>TYPE CODE # FOR DESIRED ACTION
 1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
 AND SYSTEM OPERATING COST.
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

7
 STOP

.RUN EDSP50 WITH LIGHT SYSTEM LOAD OF 3.26 pu

ECONOMIC DISPATCH EXECUTIVE PROGRAM

>>ENTER TYPE PROBLEM
 0=LOAD FLOW PROBLEM
 1=ECONOMIC DISPATCH PROBLEM

0

>>ENTER TOTAL NUMBER OF (LINES, & BUSES).
 59,48

>>WANT TO TYPE IN NEW(LINE DATA, BUS DATA, OR GENERATOR DATA,
 OR CALCULATE Y/ZBUS MATRIX)?

NNNNN

>>WANT A COPY OF (LDATA,BDATA,GDATA,OR SYSTEM CONVERGENCE CRITERIA)?
 NYYN

SYSTEM BUS DATA

BUS	TYPE	PG	QG	PD	QD	VHAG	VANG
1	-2	1.10000	0.20000	0.00000	0.00000	1.05000	0.00000
2	2	0.00000	0.00000	0.01000	0.00500	1.00000	0.00000
3	1	0.00000	0.00000	0.35000	0.13000	1.00000	0.00000
4	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
5	-1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
6	-1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
7	-1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
8	-1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
9	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
10	1	0.00000	0.00000	0.35000	0.21000	1.00000	0.00000
11	2	0.00000	0.00000	0.07000	0.01500	1.00000	0.00000
12	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
13	1	0.00000	0.00000	0.40000	0.24000	1.00000	0.00000
14	2	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
15	2	0.00000	0.00000	0.37000	0.13000	1.00000	0.00000
16	-2	1.65000	0.00000	0.00000	0.00000	1.01450	0.00000
17	1	0.00000	0.00000	0.26000	0.04000	1.00000	0.00000
18	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
19	2	0.00000	0.00000	0.02000	0.01800	1.00000	0.00000
20	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
21	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
22	2	0.00000	0.10000	0.10000	0.02000	1.00000	0.00000
23	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000

24	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
25	-2	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
26	-3	0.70000	0.60000	0.00000	0.00000	1.00000	0.00000
27	1	0.00000	0.00000	0.60000	0.30000	1.00000	0.00000
28	-2	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
29	-2	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
30	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
31	-1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
32	-1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
33	-1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
34	1	0.00000	0.00000	0.20000	0.03000	1.00000	0.00000
35	1	0.00000	0.00000	0.05000	0.02000	1.00000	0.00000
36	2	0.00000	0.00000	0.05000	0.01000	1.00000	0.00000
37	2	0.00000	0.00000	0.22000	0.12000	1.00000	0.00000
38	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
39	1	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
40	1	0.00000	0.00000	0.22000	0.01000	1.00000	0.00000
41	2	0.00000	0.20000	0.15000	0.05000	1.00000	0.00000
42	1	0.00000	0.00000	0.02000	0.01000	1.00000	0.00000
43	-2	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
44	-2	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
45	-2	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
46	2	0.00000	0.00000	0.02000	0.01000	1.00000	0.00000
47	-2	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000
48	-2	0.00000	0.00000	0.00000	0.00000	1.00000	0.00000

GENERATOR CONSTRAINTS

BUS #	PGMAX	PGMIN	QGMAX	QGMIN
1	1.1000	0.0000	0.2000	-2.0000
2			2.0000	-2.0000
5	0.2510	0.0000		
6	0.2510	0.0000		
7	0.2510	0.0000		
8	0.2510	0.0000		
11			0.8000	-2.0000
14			0.4000	-2.0000
15			0.4000	-2.0000
16	1.6500	0.0000	2.0000	-2.0000
19			0.4500	-2.0000
22			0.2400	-2.0000
25	1.0900	0.0000	2.0000	-2.0000
26	1.5900	0.0000		
28	0.7700	0.0000	2.0000	-2.0000
29	0.7900	0.0000	2.0000	-2.0000
31	0.2490	0.0000		
32	0.2490	0.0000		
33	0.2490	0.0000		
36			0.4000	-2.0000
37			0.4300	-2.0000
41			0.4000	-2.0000
43	0.4810	0.0000	0.4500	-2.0000
44	0.1480	0.0000	0.1500	-2.0000
45	0.1320	0.0000	0.1400	-2.0000
46			0.3600	-2.0000
47	0.2450	0.0000	0.2500	-2.0000
48	0.4680	0.0000	0.4500	-2.0000

>>WANT TO CHANGE (LDATA,BDATA,GDATA, OR CONVERGENCE CRITERIA)?
NNNN

>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?
NN

SOLVING LOAD FLOW EQUATIONS BY NR
 ****NR CONVERGENCE IN 3 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 20 ITERATIONS

SOLVING LOAD FLOW EQUATIONS BY NR
 ****NR CONVERGENCE IN 2 ITERATIONS
 OPTIMIZING COST FUNCTIONS
 LAMBDA DETERMINED IN 18 ITERATIONS

>>TYPE CODE # FOR DESIRED ACTION
 1=PRINT BUS & GEN SOLUTIONS ONLY.
 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
 AND SYSTEM OPERATING COST.
 3=CREATE SOS FILE OF SOLUTIONS
 4=CHANGE DATA OR TOLERANCES AND RERUN
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 RERUN WITH EXISTING DATA
 6=NEW PROBLEM
 7=TERMINATE

2

SYSTEM BUS AND GENERATOR SOLUTIONS
 ECON. DISPATCH CONVERGENCE IN 2 ITERATIONS
 ESP1= 0.0010, ESP2= 0.0010, LAMBDA= 8.6383
 SYSTEM LOSSES(PU)= 0.0456, SYSTEM LOAD(PU)= 3.2600

BUS#	BTYPE	IC	ITL	PG	QG	PD	QD	VMAG	VANG
1	-2	0.0000	0.0220	1.1000	-0.0703	0.0000	0.0000	1.0000	-0.0379
2	2	0.0000	0.0000	0.0000	0.0912	0.0100	0.0050	1.0000	-0.0586
3	1	0.0000	0.0000	0.0000	0.0000	0.3500	0.1300	0.9947	-0.0647
4	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.9947	-0.0647
5	-1	8.4448	0.0224	0.0000	0.0000	0.0000	0.0000	0.9947	-0.0647
6	-1	8.4448	0.0224	0.0000	0.0000	0.0000	0.0000	0.9947	-0.0647
7	-1	8.4448	0.0224	0.0000	0.0000	0.0000	0.0000	0.9947	-0.0647
8	-1	8.4448	0.0224	0.0000	0.0000	0.0000	0.0000	0.9947	-0.0647
9	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.9966	-0.0702
10	1	0.0000	0.0000	0.0000	0.0000	0.3500	0.2100	0.9907	-0.1271
11	2	0.0000	0.0000	0.0000	0.2577	0.0700	0.0150	1.0000	-0.1148
12	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.9979	-0.0760
13	1	0.0000	0.0000	0.0000	0.0000	0.2000	0.2000	0.9913	-0.0913
14	2	0.0000	0.0000	0.0000	0.1524	0.0000	0.0000	1.0000	-0.0875
15	2	0.0000	0.0000	0.0000	0.1597	0.3700	0.1300	1.0000	-0.1085
16	-2	0.0000	0.0100	1.6500	-0.8335	0.0000	0.0000	1.0145	0.2412
17	1	0.0000	0.0000	0.0000	0.0000	0.2600	0.0400	1.0376	0.1707
18	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0134	-0.0283
19	2	0.0000	0.0000	0.0000	-0.1606	0.0200	0.0180	1.0000	-0.0360
20	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0095	-0.0394
21	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0135	-0.0627
22	2	0.0000	0.0000	0.0000	0.0472	0.1000	0.1000	1.0000	-0.0874
23	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0057	-0.0767
24	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0043	-0.0416
25	-2	8.5614	0.0089	0.0000	0.0776	0.0000	0.1000	1.0000	-0.0416
26	-3	8.5656	0.0084	0.3551	0.0705	0.0000	0.1000	1.0000	0.0000
27	1	0.0000	0.0000	0.0000	0.0000	0.6000	0.3000	0.9871	-0.0910
28	-2	8.5433	0.0110	0.0000	0.0690	0.0000	0.0000	1.0000	-0.0910
29	-2	8.5471	0.0106	0.2005	0.0762	0.0000	0.0000	1.0000	-0.0550
30	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0043	-0.0416
31	-1	8.5617	0.0089	0.0000	0.0000	0.0000	0.0000	1.0043	-0.0416
32	-1	8.5617	0.0089	0.0000	0.0000	0.0000	0.0000	1.0043	-0.0416
33	-1	8.5617	0.0089	0.0000	0.0000	0.0000	0.0000	1.0043	-0.0416
34	1	0.0000	0.0000	0.0000	0.0000	0.2000	0.0300	1.0071	-0.0393
35	1	0.0000	0.0000	0.0000	0.0000	0.0500	0.0200	1.0020	-0.0450

36	2	0.0000	0.0000	0.0000	0.0339	0.0500	0.1100	1.0000	-0.0457
37	2	0.0000	0.0000	0.0000	0.0714	0.2200	0.2200	1.0000	-0.0486
38	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0110	-0.0320
39	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.0004	-0.0504
40	1	0.0000	0.0000	0.0000	0.0000	0.2200	0.0100	0.9986	-0.0881
41	2	0.0000	0.0000	0.0000	0.0711	0.1500	0.0500	1.0000	-0.0816
42	1	0.0000	0.0000	0.0000	0.0000	0.0200	0.0100	0.9975	-0.0906
43	-2	8.5268	0.0129	0.0000	0.0076	0.0000	0.0000	1.0000	-0.0906
44	-2	8.5268	0.0129	0.0000	0.0029	0.0000	0.0000	1.0000	-0.0906
45	-2	8.5268	0.0129	0.0000	0.0081	0.0000	0.0000	1.0000	-0.0906
46	2	0.0000	0.0000	0.0000	0.0251	0.0200	0.0100	1.0000	-0.0939
47	-2	8.5265	0.0129	0.0000	0.0000	0.0000	0.0000	1.0000	-0.0939
48	-2	8.5265	0.0129	0.0000	0.0000	0.0000	0.0000	1.0000	-0.0939

SYSTEM OPERATING COST

GEN.# 1=	0.00P.U.
GEN.# 5=	0.00P.U.
GEN.# 6=	0.00P.U.
GEN.# 7=	0.00P.U.
GEN.# 8=	0.00P.U.
GEN.# 16=	0.00P.U.
GEN.# 25=	0.00P.U.
GEN.# 26=	3.01P.U.
GEN.# 28=	0.00P.U.
GEN.# 29=	1.66P.U.
GEN.# 31=	-0.00P.U.
GEN.# 32=	0.00P.U.
GEN.# 33=	0.00P.U.
GEN.# 43=	0.00P.U.
GEN.# 44=	0.00P.U.
GEN.# 45=	0.00P.U.
GEN.# 47=	0.00P.U.
GEN.# 48=	0.00P.U.

TOTAL SYSTEM OPERATING COST = 4.67P.U.

LINE POWER FLOW

LINE#	SB	EB	REAL POWER	REACTIVE POWER
1	1	2	0.1083	0.0011
1	2	1	-0.1083	0.0011
2	1	3	0.2517	0.0530
2	3	1	-0.2517	-0.0460
3	2	3	0.0983	0.0851
3	3	2	-0.0983	-0.0840
4	3	4	-0.0000	-0.0000
4	4	3	0.0000	0.0000
5	4	5	-0.0000	0.0000
5	5	4	0.0000	0.0000
6	4	6	-0.0000	0.0000
6	6	4	0.0000	0.0000
7	4	7	-0.0000	0.0000
7	7	4	0.0000	0.0000
8	4	8	-0.0000	0.0000
8	8	4	0.0000	0.0000
9	1	9	0.5129	-0.0295
9	9	1	-0.5100	0.0377
10	9	10	0.0797	0.0107
10	10	9	-0.0797	-0.0061
11	9	11	0.3403	-0.0183
11	11	9	-0.3403	0.0336
12	10	11	-0.2703	-0.2039
12	11	10	0.2703	0.2091
13	9	12	0.0900	-0.0301
13	12	9	-0.0900	0.0257

14	12	13	0.1402	0.0627
14	13	12	-0.1402	-0.0601
15	12	14	0.0598	-0.0104
15	14	12	-0.0598	0.0111
16	12	15	0.3700	-0.0176
16	15	12	-0.3700	0.0297
17	13	14	-0.0598	-0.1399
17	14	13	0.0598	0.1413
18	12	20	-0.4800	-0.0603
18	20	12	0.4832	0.0707
19	16	17	1.6500	-0.8335
19	17	16	-1.6379	0.5502
20	17	18	1.3779	-0.5902
20	18	17	-1.3526	-0.6270
21	18	20	0.6920	0.2441
21	20	18	-0.6920	-0.2354
22	18	19	0.0524	0.0913
22	19	18	-0.0524	-0.0897
23	19	20	0.0324	-0.0888
23	20	19	-0.0324	0.0898
24	20	21	0.1007	-0.1461
24	21	20	-0.1000	-0.0560
25	18	38	0.6082	0.2916
25	38	18	-0.6079	-0.3484
26	21	22	0.0477	0.0268
26	22	21	-0.0477	-0.0252
27	21	23	0.0523	0.0293
27	23	21	-0.0523	-0.0283
28	22	23	-0.0523	-0.0276
28	23	22	0.0523	0.0283
29	20	24	0.1406	0.2211
29	24	20	-0.1404	-0.2289
30	24	27	0.3917	0.1479
30	27	24	-0.3917	-0.1262
31	24	25	-0.0000	0.0225
31	25	24	0.0000	-0.0224
32	24	26	-0.3551	0.0444
32	26	24	0.3551	-0.0295
33	24	30	-0.0000	0.0000
33	30	24	0.0000	0.0000
34	27	28	-0.0000	-0.0681
34	28	27	0.0000	0.0690
35	27	29	-0.2005	-0.0681
35	29	27	0.2005	0.0762
36	30	31	-0.0000	0.0000
36	31	30	0.0000	0.0000
37	30	32	-0.0000	0.0000
37	32	30	0.0000	0.0000
38	30	33	-0.0000	0.0000
38	33	30	0.0000	0.0000
39	24	34	-0.0878	-0.0789
39	34	24	0.0879	0.0635
40	34	35	0.0616	0.0549
40	35	34	-0.0616	-0.0542
41	34	36	0.0384	0.0425
41	36	34	-0.0384	-0.0420
42	34	38	-0.4508	-0.2388
42	38	34	0.4508	0.2431
43	34	37	0.0629	0.0480
43	37	34	-0.0629	-0.0471
44	35	36	0.0116	0.0342
44	36	35	-0.0116	-0.0341
45	37	38	-0.1571	-0.1016
45	38	37	0.1571	0.1053

46	1	24	0.0271	-0.0517
46	24	1	-0.0271	0.0394
47	24	39	0.2187	0.0536
47	39	24	-0.2184	-0.0566
48	27	42	-0.0078	-0.0377
48	42	27	0.0079	0.0380
49	1	39	0.2000	-0.0433
49	39	1	-0.1996	0.0383
50	39	40	0.1737	0.0114
50	40	39	-0.1737	-0.0049
51	39	41	0.2442	0.0069
51	41	39	-0.2442	0.0007
52	40	41	-0.0942	-0.0198
52	41	40	0.0942	0.0204
53	40	42	0.0479	0.0147
53	42	40	-0.0479	-0.0145
54	42	43	-0.0000	-0.0075
54	43	42	0.0000	0.0076
55	42	44	-0.0000	-0.0029
55	44	42	0.0000	0.0029
56	42	45	-0.0000	-0.0081
56	45	42	0.0000	0.0081
57	42	46	0.0200	-0.0150
57	46	42	-0.0200	0.0151
58	46	47	-0.0000	0.0000
58	47	46	0.0000	0.0000
59	46	48	-0.0000	0.0000
59	48	46	0.0000	0.0000

>>TYPE CODE # FOR DESIRED ACTION

- 1=PRINT BUS & GEN SOLUTIONS ONLY.
- 2=PRINT LINE POWERS, BUS & GEN SOLUTIONS,
AND SYSTEM OPERATING COST.
- 3=CREATE SOS FILE OF SOLUTIONS
- 4=CHANGE DATA OR TOLERANCES AND RERUN
- 5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,
RERUN WITH EXISTING DATA
- 6=NEW PROBLEM
- 7=TERMINATE

7
STOP

END OF EXECUTION
CPU TIME: 3:54.54
EXIT

ELAPSED TIME: 17:48.93

APPENDIX B

COMPUTER CODE LISTINGS

Computer Code EDSP50

```

C ECONOMIC DISPATCH EXECUTIVE PROGRAM
C THIS PROGRAM PROVIDES LOAD FLOW SOLUTIONS AND ECONOMIC
C DISPATCH FOR POWER SYSTEMS WITH A MAXIMUM OF 50
C BUSES AND 100 TRANSMISSION LINES. IT SOLVES FOR SYSTEM
C LOAD, LOSSES, GENERATOR INCREMENTAL COSTS, REAL POWER
C GENERATION, TRANSMISSION LINE REAL & REACTIVE POWER FLOWS.

REAL LNGTH, LAMBDA, IC
INTEGER ABORT, AMS, BDAT, BTYPE, BUSH, CE, CC, CG, CBC, CHB, CHG, CHL,
ICL, CHY, CHZ, EB, GDAT, QDAT, MBUS, BGSOL, LPSOL, SB, ILDAT, TBDAT,
ITGDAT, TBUSH
DOUBLE PRECISION AJ1, AJ2, AJ3, AJ4, BJ1, BJ2, BJ3, BJ4,
ICALP, CALQ, DQ, DVANG, EVHAG, G, H, ITL, P, C, VANG, VHAG,
ZXI, YANG, YHAG, YY, YYSHT, ZANG, ZHAG, YSER
CCOMMON/ / AJ1(50,50), AJ2(50,50), AJ3(50,50),
1AJ4(50,50), ALPHA(50), BDAT, BETA(50),
1BGSOL, BJ1(50,50), BJ2(50,50), BJ3(50,50),
1BJ4(50,50), BTYPE(50), BUSH, CALP(50),
ICALQ(50), CB, CC, CG, CHB,
1CHG, CHL, CL, CHY,
1CHZ, DQ(50), DVANG(50), DVHAG(50),
1EB(100), ESP1, ESP2, G(50),
1GANNA(50), GDAT, H(50), IC(50),
1II, ITER, ITL(50), KINV,
1LAMBDA, LDAT, LITER,
1LNGTH(100), LMO, LOSS, LPSOL,
1LSET, MBUS, M5, MSWGB,
1P(50), PD(50), PG(50), PGHAX(50),
1PGHIN(50), Q(50), QD(50), QDAT, QG(50),
1QGHAX(50), QGHIN(50), SB(100), YYSHT(100,2),
1TOL, TLDAT, TPD, TBDAT, TPL, TGDAT, VANG(50),
1VHAG(50), IX(50,50), YANG(50,50),
1YHAG(50,50), YYSHT(100,2), YY(50,50), ZANG(50,50),
1ZHAG(50,50), ZSER(100,2), YSER(100,2), ABORT, IBT(50)
DATA
1ABORT/0/, BDAT/0/, BUSH/0/, CB/'N'/.
1CG/'N'/, CHB/'N'/, CHC/'N'/.
1CHG/'N'/, CHL/'N'/, CL/'N'/.
1CHY/'N'/, CHZ/'N'/, ESP1/0.001/.
1ESP2/0.001/, GDAT/0/, ITER/50/, KINV/0/.
1LDAT/0/, LITER/5/, LOSS/'N'/.
1TOL/0.0001/, QDAT/0/

CALL ERRSET(0)
10 TYPE 1000
1000 FORMAT(15X'*****ECONOMIC DISPATCH EXECUTIVE PROGRAM*****')

C SYSTEM INITIALIZATION
20 TYPE 1010
1010 FORMAT(/IX,'>>ENTER TYPE PROBLEM'/8X,'0=LOAD FLOW PROBLEM'/
18X,'1=ECONOMIC DISPATCH PROBLEM')
22 ACCEPT 2000, KINV
2000 FORMAT(I1)
IF((KINV.EQ.0).OR.(KINV.EQ.1)) GO TO 24
TYPE 1012
1012 FORMAT(1X,'WRONG ENTRY, MUST BE 0 OR 1, TRY AGAIN')
GO TO 22
24 IF(KINV)30,30,26
26 TYPE 1014
1014 FORMAT(/IX,'>>IS SYSTEM LOSSLESS?')
28 ACCEPT 2001, LOSS

```

```

2001  FORMAT(1A1)
      IF((LOSS.EQ.'N').OR.(LOSS.EQ.'Y')) GO TO 30
      TYPE 1013
1013  FORMAT(1X,'WRONG ENTRY, MUST BE "Y" OR "N", TRY AGAIN.')
      GO TO 28
30     IF((LDAT.EQ.1).AND.(BDAT.EQ.1).AND.(GDAT.EQ.1))
      1GO TO 70
      TYPE 1020
1020  FORMAT(/1X,'>>>ENTER TOTAL NUMBER OF (LINES, & BUSES).')
36     ACCEPT 2004,LNO,MBUS
2004  FORMAT(2I)
      IF(((LNO.GE.1).AND.(LNO.LE.100)).AND.((MBUS.GE.1)
      1.AND.(MBUS.LE.50))) GO TO 40
      TYPE1016
1016  FORMAT(1X,'WRONG ENTRY,TOTAL LINES=1 TO 100 &TOTAL BUSES=1 TO 50,
      1TRY AGAIN.')
      GO TO 36

```

C CHECK METHOD OF DATA INPUT (SOS FILE/CRT/TTY)

```

40     TYPE 1030
1030  FORMAT(/1X,'>>>WANT TO TYPE IN MEN(LINE DATA, BUS DATA, OR
      1 GENERATOR DATA, '/5X,'OR CALCULATE Y/ZBUS MATRIX)?')
50     ACCEPT 2008,ILDAT,TBDAT,TGDAT,TBUSH
      IF(((ILDAT.EQ.'N').OR.(ILDAT.EQ.'Y')).AND.((TBDAT.EQ.'N')
      1.OR.(TBDAT.EQ.'Y')).AND.((TGDAT.EQ.'N').OR.(TGDAT.EQ.'Y')
      1.AND.(TBUSH.EQ.'N').OR.(TBUSH.EQ.'Y'))) GO TO 60
      TYPE 1015
1015  FORMAT(1X,'WRONG ENTRY, MUST BE "N" OR "Y" FOR
      1EACH DATA GROUP, '/1X,'i.e. "NYN" means type in bus
      1data only, please use CAP N & Y, '/1X,'try again.')
2008  FORMAT(4A1)
      GO TO 50

```

C READ SYSTEM DATA FROM SOS FILE, TTY, OR CRT

```

60     IF(LDAT.EQ.0) CALL LDATA
      IF(ABORT.EQ.1) GO TO 320
      IF(TBUSH.EQ.'Y') GO TO 80
      OPEN(UNIT=24,DEVICE='DSK',ACCESS='SEQIN',DISPOSE='SAVE',
      1FILE='FOR24.DAT')
      DO 52 I=1,LNO
52     READ(24,4000) (YYSHT(I,1),YYSHT(I,2),YSER(I,1),YSER(I,2))
4000  FORMAT(4D)
      DO 54 I=1,MBUS
54     READ(24,4005) (YHAG(I,J),YANG(I,J),J=1,MBUS)
4005  FORMAT(2D)
      BUSH=1
      IF(KINV.EQ.0) GO TO 80
      DO 55 I=1,MBUS
55     READ(24,4005) (ZHAG(I,J),ZANG(I,J),J=1,MBUS)
      BUSH=2
80     IF(BDAT.EQ.0) CALL BDATA
      IF(ABORT.EQ.1) GO TO 320
90     IF(GDAT.EQ.0) CALL GDATA
      IF(ABORT.EQ.1) GO TO 320

```

C CHECK FOR PRINTOUT OF SYSTEM DATA

```

70     TYPE 1050
1050  FORMAT(/1X,'>>>WANT A COPY OF (LDATA,BDATA,GDATA,
      1OR SYSTEM CONVERGENCE CRITERIA)?')

```

```

100 READ(5,2020)CL,CB,CG,CC
2020 FORMAT(4A1)
IF(((CL.EQ.'N').OR.(CL.EQ.'Y')).AND.
1((CB.EQ.'N').OR.(CB.EQ.'Y')).AND.
2((CG.EQ.'N').OR.(CG.EQ.'Y')).AND.
3((CC.EQ.'N').OR.(CC.EQ.'Y'))).GO TO 110
TYPE 1019
1019 FORMAT(1X,'WRONG ENTRY, MUST BE "N" OR "Y" FOR
1EACH DATA GROUP. '/1X,'I.E. "N" MEANS TYPE OUT
2BUS DATA AND CONVERGENCE CRITERIA ONLY. '/1X, 'TRY AGAIN. ')
GO TO 100
110 IF(CL.EQ.'Y')CALL LDATA
120 IF(CB.EQ.'Y')CALL BDATA
130 IF(CG.EQ.'Y')CALL GDATA

C PRINT SYSTEM CONVERGENCE CRITERIA
140 IF(CC.EQ.'N')GO TO 145
142 WRITE(5,1065)LITER,TOL,ITER,ESP1,ESP2
1065 FORMAT(/1X,'**SYSTEM CONVERGENCE CRITERIA**'/10X,
1'LOAD FLOW ITERATIONS=',I3/
110X,'LOAD FLOW TOLERANCE=',E13.5/
210X,'ECON DISP ITERATIONS=',I3/10X,'ESP1=',E13.5/10X,'ESP2=',
3E13.5)

C CHECK FOR CHANGES TO CONVERGENCE CRITERIA OR SYSTEM DATA
145 TYPE 1070
1070 FORMAT(/1X,'>>WANT TO CHANGE
1(LDATA,BDATA,GDATA, OR CONVERGENCE CRITERIA)?')
150 ACCEPT 2040,CHL,CHB,CHG,CHC
2040 FORMAT(4A1)
IF(((CHC.EQ.'N').OR.(CHC.EQ.'Y')).AND.
1((CHL.EQ.'N').OR.(CHL.EQ.'Y')).AND.
1((CHB.EQ.'N').OR.(CHB.EQ.'Y')).AND.
1((CHG.EQ.'N').OR.(CHG.EQ.'Y'))).GO TO 160
TYPE 1021
1021 FORMAT(1X,'WRONG ENTRY, MUST BE "N" OR "Y" FOR EACH DATA
1GROUP, TRY AGAIN. ')
GO TO 150
160 IF(CHL.EQ.'Y')CALL LDATA
IF(CHB.EQ.'Y')CALL BDATA
IF(CHG.EQ.'Y')CALL GDATA
IF(CHC.EQ.'N')GO TO 190
TYPE 1090
1090 FORMAT(/1X,'**CONVERGENCE CRITERIA CHANGES**'/
11X,'>>ENTER (VARIABLE #,NEW VALUE THEN "CR") '/
110X,'1=LOAD FLOW ITERATIONS'/10X,'2=LOAD FLOW TOLERANCE'/
210X,'3=ECON DISP ITERATIONS'/10X,'4=ESP1'/10X,'5=ESP2'/
310X,'>>ENTER 0 THEN "CR" WHEN CHANGES CCHPLETED. ')
170 READ(5,2050)NAME,X
2050 FORMAT(I,Y)
IF((NAME.GE.0).AND.(NAME.LE.5)).GO TO 180
TYPE 1100
1100 FORMAT(1X,'WRONG ENTRY,VARIABLE MUST BE 1-5, TRY AGAIN. ')
GO TO 170
180 IF(NAME.EQ.0)GO TO 190
GO TO(181,182,183,184,185)NAME
181 LITER=IFIX(X)
TYPE 1110,LITER
1110 FORMAT(8X,'LOAD FLOW ITERATIONS=',I3)
GO TO 170
182 TOL=X

```

```

1120   TYPE 1120,TOL
      FORNAT(8X,'LOAD FLOW TOLERANCE=',E13.5)
      GO TO 170
183   ITER=IFIX(X)
      TYPE 1130,ITER
1130   FORNAT(8X,'OPT DISP ITERATIONS=',I3)
      GO TO 170
184   ESP1=X
      TYPE 1140,ESP1
1140   FORNAT(8X,'ESP1=',E13.5)
      GO TO 170
185   ESP2=X
      TYPE 1150,ESP2
1150   FORNAT(8X,'ESP2=',E13.5)
      GO TO 170

C CHECK FOR COPY OF Y/ZBUS MATRIX
C CHECK FOR COPY OF Y/ZBUS MATRIX
190   IF((BUSH.EQ.0).OR.((BUSH.NE.2).AND.(KINV.EQ.1)))CALL YBUSH
222   TYPE 1152
1152   FORNAT(/IX,'>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?')
223   ACCEPT 2060,CHY,CHZ
      IF(KINV.EQ.0)CHZ='N'
2060   FORNAT(2A1)
      IF(((CHY.EQ.'N').OR.(CHY.EQ.'Y')).AND.((CHZ.EQ.'N').OR.
1(CHZ.EQ.'Y'))GO TO 224
      TYPE 1021
      GO TO 223
224   IF ((CHY.EQ.'Y').OR.(CHZ.EQ.'Y'))CALL YBUSH
225   CONTINUE

C SYSTEM INITIALIZED STARTING LOAD FLOW CALCULATIONS
LSET=0

C CALCULATING LOAD FLOW BY NEWTON-RAPHSON
CALL WRLF
IF(ABORT.EQ.1)GO TO 320
IF(KINV.EQ.0)GO TO 320

C CALCULATING OPT DISP POWER BALANCE EQUATIONS
CALL OPT
GO TO 330

320   ABORT=D
330   TYPE1210
1210   FORNAT(/IX,'>>TYPE CODE # FOR DESIRED ACTION'/
18X,'1=PRINT BUS & GEN SOLUTIONS ONLY.'/8X,'2=PRINT LINE
2POWERS, BUS & GEN SOLUTIONS,'/13X,'AND SYSTEM
2 OPERATING COST.'/8X,'3=CREATE SOS FILE OF
2 SOLUTIONS'/8X,'4=CHANGE DATA OR TOLERANCES AND RERUN'/
18X,'5=CHANGE TYPE PROBLEM OR SOLUTION METHOD,'/13X,'RERUN WITH
1EXISTING DATA'/8X,'6=NEW PROBLEM'/8X,'7=TERMINATE')

340   ACCEPT 2000,ANS
      IF((ANS.GE.1).AND.(ANS.LE.7))GO TO 350
      TYPE 1220
1220   FORNAT(1X,'WRONG ENTRY, MUST BE 1 TO 7, TRY AGAIN.')
      GO TO 340
350   GO TO(361,362,380,363,365,367,500)ANS

```



```

361  N5=5
      BGSOL=1
      LPSOL=0
      CALL SOL
      GO TO 330
362  N5=5
      BGSOL=1
      LPSOL=1
      CALL SOL
      GO TO 330
363  LSET=0
      TBDAT='M'
      DO 65 I=1,NBUS
      IF (IBT(I).NE.2) GO TO 65
      BTYPE(I)=ISIGN(2,BTYPE(I))
      VHAG(I)=1.0
      IBT(I)=0
65   CONTINUE
      GO TO 145
      LSET=0
365  TBDAT='M'
      DO 66 I=1,NBUS
      IF (IBT(I).NE.2) GO TO 66
      BTYPE(I)=ISIGN(2,BTYPE(I))
      VHAG(I)=1.0
      IBT(I)=0
66   CONTINUE
      GO TO 10
367  LDAT=0
      BDAT=0
      GDAT=0
      QDAT=0
      LSET=0
      GO TO 10

```

C CREATING SOS FILE OF BUS & GENERATOR SOLUTIONS, AND
C LINE POWER FLOW.

```

380  OPEN(UNIT=1,DEVICE='DSK',ACCESS='SEQOUT',
      1DISPOSE='SAVE',FILE='SOL.DAT')
      N5=1
      BGSOL=1
      LPSOL=1
      CALL SOL
      CLOSE(UNIT=1)
      N5=5
      GO TO 330
500  CONTINUE
      STOP
      END

```

SUBROUTINE LDATA
C SUBROUTINE TO READ, WRITE, AND CHANGE LINE DATA

```

REAL LENGH
INTEGER ABORT,BUSH,CL,CHL,EB,SB,ILDAT
DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,EJ3,EJ4,
1CALP,CALQ,DQ,DVANG,DVHAG,G,H,ITL,P,Q,VANG,VHAG,

```

```

2IX,YANG,YHAG,YY,YYSH,ZANG,ZHAG,YSER
COMMON/ / AJ1(50,50), AJ2(50,50), AJ3(50,50),
1AJ4(50,50), ALPHA(50), EDAT, BETA(50),
1BGSOL, BJ1(50,50), BJ2(50,50), BJ3(50,50),
1BJ4(50,50), BTYPE(50), BUSH, CALP(50),
1CALQ(50), CB,CC, CG, CNB,
1CHG, CHL, CL, CHY,
1CIZ, DQ(50), DVANG(50), EVEAG(50),
1EB(100), ZSP1, ZSP2, G(50),
1GANHA(50), GDAT, H(50), IC(50),
1II, ITER, ITL(50), KINV,
1LANBDA, LDAT, LITER,
1LNGTH(100), LNO, LOSS, LPSOL,
1LSET, MBUS, M5, MSHGB,
1P(50), PD(50), PG(50), PGHAY(50),
1PGHIN(50), Q(50), QD(50), QDAT, QG(50),
1QGMAX(50), QGHIN(50), SB(100), YSHT(100,2),
1TOL, TLDAT, TPD, TBDAT, TPL, TGDAT, VANG(50),
1VHAG(50), YX(50,50), YANG(50,50),
1VHAG(50,50), YSHT(100,2), YY(50,50), ZANG(50,50),
1ZHAG(50,50), ZSER(100,2), YSER(100,2), ABORT

```

```

ILD=0
IF(LDAT.EQ.1)GO TO 50
IF(TLDAT.EQ.'Y')GO TO 20

```

```

C READ LINE DATA FOR SOS FILE POR20.DAT
OPEN(UNIT=20,DEVICE='DSK',ACCESS='SEQIN',DISPOSE='SAVE',
1FILE='POR20.DAT')
10 DO 5 I=1,LNO
5 READ(20,*)K,SB(I),EB(I),LNGTH(I),YSHT(I,1),YSHT(I,2),
1ZSER(I,1),ZSER(I,2)
CLOSE(UNIT=20)
2000 FORMAT(3I,5F)
IF(K.EQ.LNO)GO TO 40
TYPE 8
8 FORMAT(1X,'TOTAL NUMBER OF LINES ENTERED DOES NOT EQUAL
1NUMBER OF DATA LINES IN POR20.DAT')
ABORT=1
LDAT=0
RETOBH

C READ LINE DATA FROM CRT/TTY
20 OPEN(UNIT=20,DEVICE='DSK',ACCESS='SEQOUT',DISPOSE='SAVE',
1FILE='POR20.DAT')
IF(ILD.EQ.1)GO TO 21
TYPE 1000
1000 FORMAT(/1X,'**SYSTEM LINE DATA**'/1X,'>>ENTER (LINE #,
1SB #,EB #, LINE LENGTH, YSHUNT G,YSBUNT B,
2ZSERIES R,ZSERIES X)')
DO 30 I=1,LNO
IF(ILD.EQ.1)GO TO 25
22 ACCEPT 2002,K,SB(I),EB(I),LNGTH(I),YSHT(I,1),YSHT(I,2),
1ZSER(I,1),ZSER(I,2)
2002 FORMAT(3I,5F)
IF(K.EQ.I)GO TO 25
TYPE 1002,I
1002 FORMAT(1X,'WRONG ENTRY, LINE # SHOULD=',I3,', TRY AGAIN')
GO TO 22
25 WRITE(20,1004)I,SB(I),EB(I),LNGTH(I),YSHT(I,1),YSHT(I,2),
1ZSER(I,1),ZSER(I,2)

```

```

1004   FORMAT(3I3,5E12.5)
30     CONTINUE
      CLOSE(UNIT=20)
      IF(ILD.EQ.1)GO TO 80
40     BUSH=0
      LDAT=1

C CHECK FOR LINE DATA PRINT OUT
50     IF(CL.EQ.'N')GO TO 70
      TYPE 1010
1010   FORMAT(/1X,'**SYSTEM LINE DATA**'/1X,'LINE #',1X,
      1'SB',1X,'EB',4X,'LENGTH',12X,'Y SHUNT',19X,'Z SERIES')
      DO 60 I=1,LNO
60     TYPE 1020,I,SB(I),EB(I),LNTH(I),YSHT(I,1),YSHT(I,2),
      1ZSER(I,1),ZSER(I,2)
1020   FORMAT(1X,I3,2X,2I3,1X,E12.5,2(1X,2F12.5))
      CL='N'

      IF(ILD.EQ.1)GO TO 80
C CHECK FOR LINE DATA CHANGES
70     IF(CHL.EQ.'N')GO TO 180
      TYPE 1030
1030   FORMAT(/1X,'** LINE DATA CHANGES**'/
      11X,'>>ENTER (VARIABLE #, LINE #, NEW VALUE THEN "CR")'/
      110X,'1=STARTING BUS #'/10X,'2=ENDING BUS #'/10X,'3=LINE
      1LENGTH'/10X,'4=Y SHUNT G'/10X,'5=Y SHUNT B'/10X,'6=Z SERIES R'/
      210X,'7=Z SERIES X'/10X,'8=RETYPE COPY OF ALL LINE DATA'/10X,'
      19=CHANGE TOTAL NUMBER OF LINES'/10X,'10=UPDATE SOS
      1FILE WITH CHANGES'/10X,'>>ENTER 0 THEN
      1"CR" WHEN CHANGES COMPLETED')
80     READ(5,2010) NAME,I,X
2010   FORMAT(2I,F)
      IF(NAME.EQ.0)GO TO 179
      IF(NAME.EQ.8)GO TO 172
      IF(NAME.EQ.9)GO TO 173
      IF(NAME.EQ.10)GO TO 175
      IF(((NAME.GE.1).AND.(NAME.LE.7)).AND.((I.GE.0).AND.(I.LE.LNO)))
      1GO TO 100
      TYPE 1040,LNO
1040   FORMAT(1X,'WRONG ENTRY, VARIABLE # MUST BE 1-7, '/
      11X,'LINE # MUST BE 1 TO',I3,', TRY AGAIN')
      GO TO 80
100     BUSH=0
      GO TO(110,120,130,140,150,160,170) NAME
110     SB(I)=IFIX(X)
      TYPE 1060, I,SB(I)
1060   FORMAT(1X,'SB(LINE #',I3,')=',I3)
      GO TO 80
120     EB(I)=IFIX(X)
      TYPE 1070,I,EB(I)
1070   FORMAT(1X,'EB(LINE #',I3,')=',I3)
      GO TO 80
130     LNTH(I)=I
      TYPE 1080,I,LNTH(I)
1080   FORMAT(1X,'LENGTH(LINE #',I3,')=',E12.5)
      GO TO 80
140     YSHT(I,1)=I
      TYPE 1090,I,YSHT(I,1)
1090   FORMAT(1X,'YSHT G (LINE #',I3,')=',E12.5)
      GO TO 80
150     YSHT(I,2)=I

```

```

1100 TYPE 1100,I,YSHT(I,2)
      FORMAT(1X,'YSHT B (LINE #',I3,')=',E12.5)
      GO TO 80
160   ZSER(I,1)=X
      TYPE 1110,I,ZSER(I,1)
1110  FORMAT(1X,'ZSER R (LINE #',I3,')=',E12.5)
      GO TO 80
170   ZSER(I,2)=X
      TYPE 1120,I,ZSER(I,2)
1120  FORMAT(1X,'ZSER X (LINE #',I3,')=',E12.5)
      GO TO 80
172   ILD=1
      CL='Y'
      GO TO 50
173   LNO=I
      BUSH=0
      TYPE 1130,I
1130  FORMAT(1X,'TOTAL NUMBER OF LINES =',I3)
      GO TO 80
175   ILD=1
      GO TO 20
179   ILD=0
      CHL='M'
180   RETURN
      END

```

```

SUBROUTINE BDATA
C SUBROUTINE TO READ,WRITE,AND CHANGE BUS DATA
INTEGER ABORT,BDAT,BTYPE,CB,CHB,MBUS,TBDAT
DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,EJ3,EJ4,
1CALP,CALQ,DQ,DVANG,DVHAG,C,H,ITL,P,Q,VANG,VHAG,
2XX,YANG,YHAG,YY,YSHT,ZANG,ZHAG,YSER
COMMON /
1AJ4(50,50), ALPHA(50), BDAT, AJ3(50,50),
1BGSOL, BJ1(50,50), BJ2(50,50), BJJ(50,50),
1BJ4(50,50), BTYPE(50), BUSH, CALP(50),
1CALQ(50), CB,CC, CG, CHB,
1CHG, CHL, CL, CHY,
1CHZ, DQ(50), DVANG(50), DVHAG(50),
1EB(100), ESP1, ESP2, G(50),
1GAMMA(50), GDAT, H(50), IC(50),
1II, ITER, ITL(50), KINV,
1LAMBDA, LDAT, LITER,
1LNGTH(100), LNO, LOSS, LPSOL,
1LSET, MBUS, M5, MSWGB,
1P(50), PD(50), PG(50), PGHAX(50),
1PGHIN(50), Q(50), QD(50),QDAT, QG(50),
1QGMAX(50), QGHIN(50), SB(100), YSHT(100,2),
1TOL,TLDAT, TPD,TBDAT, TPL,TGDAT, VANG(50),
1VHAG(50), XX(50,50), YANG(50,50),
1YHAG(50,50), YSHT(100,2), YY(50,50), ZANG(50,50),
1ZHAG(50,50), ZSER(100,2), YSER(100,2), ABORT

IBD=0
IF(BDAT.EQ.1)GO TO 50
IF(TBDAT.EQ.'Y')GO TO 20

```

```

C READ BUS DATA FROM SOS FILE FOR21.DAT

```

```

5      OPEN(UNIT=21,DEVICE='DSK',ACCESS='SEQIN',DISPOSE='SAVE',
        1FILE='FOR21.DAT')
10     DO 15 I=1,HBUS
15     READ(21,*)K,BTYPE(I),PG(I),QG(I),PD(I),QD(I),
        1VHAG(I),VANG(I)
2000   FORMAT(2I,6F)
        CLOSE(UNIT=21)
        IF(K.EQ.HBUS)GO TO 45
        TYPE 500
500    FORMAT(1X,'TOTAL NUMBER OF BUSES ENTERED DOES NOT
        1EQUAL NUMBER OF DATA LINES IN FOR21.DAT')
        BDAT=0
        ABORT=1
        RETURN

C READ BUS DATA FROM CRT/TTY
19     OPEN(UNIT=21,DEVICE='DSK',ACCESS='SEQOUT',DISPOSE='SAVE',
        1FILE='FOR21.DAT')
        IF(IBM.EQ.1)GO TO 21
20     TYPE1000
1000   FORMAT(/1X,'**SYSTEM BUS DATA**'/1X,'>>>ENTER(BUS#,
        1 BUS TYPE,PG,QG,PD,QD,VHAG,VANG)')
21     DO 30 I=1,HBUS
        IF(IBM.EQ.1)GO TO 25
22     ACCEPT 2000,K,BTYPE(I),PG(I),QG(I),PD(I),QD(I),
        1VHAG(I),VANG(I)
        IF(K.EQ.I)GO TO 25
        TYPE 1005,I
1005   FORMAT(1X,'WRONG ENTRY, BUS # SHOULD=',I3,', TRY AGAIN.')
        GO TO 22
25     WRITE(21,1010)I,BTYPE(I),PG(I),QG(I),PD(I),QD(I),
        1VHAG(I),VANG(I)
1010   FORMAT(2I3,6F10.5)
30     CONTINUE
        CLOSE(UNIT=21)
45     BDAT=1
        IF(IBM.EQ.1)GO TO 80

C CHECK FOR PRINTOUT OF BUS DATA
50     IF(CB.EQ.'N')GO TO 70
        TYPE 1020
1020   FORMAT(/1X,'**SYSTEM BUS DATA**'/2X,'BUS',I3,'TYPE',
        15X,'PG',8X,'QG',8X,'PD',8X,'QD',7X,'VHAG',6X,'VANG')
        DO 60 I=1,HBUS
        TYPE 1030,I,BTYPE(I),PG(I),QG(I),PD(I),QD(I),
        1VHAG(I),VANG(I)
1030   FORMAT(1X,I3,4X,I3,6F10.5)
60     CONTINUE
        CB='N'
        IF(IBM.EQ.1)GO TO 80

C CHECK FOR BUS DATA CHANGES
70     IF(CHB.EQ.'N')GO TO 170
        TYPE 1040
1040   FORMAT(/1X,'**BUS DATA CHANGES**'/
        11X,'>>>ENTER(VARIABLE #, BUS #, NEW VALUE THEN "CR"/
        110X,'1=BUS TYPE'/10X,'2=PG'/10X,'3=QG'/10X,'4=PD'
        1/10X,'5=QD'/10X,'6=VHAG'/10X,'7=VANG'

```

```

1/10X,'8=RETYPE COPY OF ALL BUS DATA'
1/10X,'9=CHANGE TOTAL NUMBER OF BUSES'/10X,
1'10=REENTER ORIGINAL BUS DATA FROM SOS FILE'/10X,
2'11=UPDATE SOS FILE WITH CHANGES'/10X,
1'>>ENTER 0 THEN "CP" WHEN CHANGES COMPLETED.')
80 READ(5,2010) NAME,I,X
2010 FORMAT(2I,F)
IF(NAME.EQ.0)GO TO 170
IF(NAME.EQ.9)GO TO 164
IF(NAME.EQ.10)GO TO 165
IF(NAME.EQ.11)GO TO 166
IF(((NAME.GE.1).AND.(NAME.LE.8)).AND.
1((I.GE.0).AND.(I.LE.MBUS)))GO TO 100
TYPE 1050,MBUS
1050 FORMAT(1X,'WRONG ENTRY, VARIABLE NAME MUST BE 1-8,/'
11X,'BUS # MUST BE 1 TO',I3,', TRY AGAIN.')
GO TO 80
100 GO TO(110,120,130,140,150,160,162,163)NAME
110 BTYPE(I)=IPIX(X)
TYPE 1060,I,BTYPE(I)
1060 FORMAT(1X,'BUS TYPE(BUS #',I3,')=',I3)
GO TO 80
120 PG(I)=X
TYPE 1070,I,PG(I)
1070 FORMAT(1X,'PG(BUS #',I3,')=',Z12.5)
GO TO 80
130 QG(I)=X
TYPE 1080,I,QG(I)
1080 FORMAT(1X,'QG(BUS #',I3,')=',Z12.5)
GO TO 80
140 PD(I)=X
TYPE 1090,I,PD(I)
1090 FORMAT(1X,'PD(BUS #',I3,')=',Z12.5)
GO TO 80
150 QD(I)=X
TYPE 1100,I,QD(I)
1100 FORMAT(1X,'QD(BUS #',I3,')=',Z12.5)
GO TO 80
160 VHAG(I)=X
TYPE 1110,I,VHAG(I)
1110 FORMAT(1X,'VHAG(BUS #',I3,')=',Z12.5)
GO TO 80
162 VANG(I)=X
TYPE 1111,I,VANG(I)
1111 FORMAT(1X,'VANG(BUS#',I3,')=',Z12.5)
GO TO 80
163 CB='Y'
IBD=1
GO TO 50
164 MBUS=I
TYPE 1120,I
1120 FORMAT(1X,'TOTAL NUMBER OF BUSES =',I3)
GO TO 80
165 IBD=1
LSET=0
GO TO 5
166 IBD=1
GO TO 19
170 IBD=0
CHB='N'

```

```

RETURN
END

```

```

SUBROUTINE GDATA
C SUBROUTINE TO READ,WRITE,AND CHANGE GENERATOR DATA

```

```

INTEGER BTYPE,CG,CHG,GDAT,GNO,MBUS,IGDAT,QDAT
DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,BJ3,BJ4,
1CALP,CALQ,DQ,DVANG,EVHAG,G,H,ITL,P,C,VANG,VHAG,
2XI,YANG,YHAG,YY,YSHT,ZANG,ZHAG,YSER
COMMON / AJ1(50,50), AJ2(50,50), AJ3(50,50),
1AJ4(50,50), ALPHA(50), BDAT, BETA(50),
1BGSOL, BJ1(50,50), BJ2(50,50), BJ3(50,50),
1BJ4(50,50), BTYPE(50), BSSH, CALP(50),
1CALQ(50), CB,CC, CG, CHB,
1CHG, CHL, CL, CHY,
1CHZ, DQ(50), DVANG(50), DVHAG(50),
1EB(100), ESP1, ESP2, G(50),
1GAMMA(50), GDAT, H(50), IC(50),
1II, ITER, ITL(50), KINV,
1LAMBDA, LDAT, LITER,
1LNGTH(100), LWO, LOSS, IPSOL,
1LSET, MBUS, NS, NSHGB,
1P(50), PD(50), PG(50), PGMAY(50),
1PGHIN(50), Q(50), QD(50), QDAT, QG(50),
1QGMAY(50), QGHIN(50), SB(100), YSHT(100,2),
1TOL, TLDAT, TPD, TBDAT, TPL, TGDAT, VANG(50),
1VHAG(50), XI(50,50), YANG(50,50),
1YHAG(50,50), YSHT(100,2), YY(50,50), ZANG(50,50),
1ZHAG(50,50), ZSER(100,2), YSER(100,2), ABOOT

```

```

IGB=0
IF(GDAT.EQ.1)GO TO 56
IF(KINV.EQ.0)GO TO 25
IF(TGDAT.EQ.'Y')GO TO 20

```

```

C READ GENERATOR DATA FROM SOS FILE FOR22.DAT
OPEN(UNIT=22,DEVICE='DSK',ACCESS='SEQIN',DISPOSE='SAVE',
1FILE='FOR22.DAT')
GNO=0
10 DO 15 I=1,MBUS
IF((BTYPE(I)).GE.0)GO TO 15
READ(22,*)K,ALPHA(I),BETA(I),GAMMA(I)
2000 FORMAT(I,3F)
GNO=GNO+1
15 CONTINUE
CLOSE(UNIT=22)
GO TO 40

C READ GENERATOR DATA FROM CRT/TTY
20 OPEN(UNIT=22,DEVICE='DSK',ACCESS='SEQOUT',DISPOSE='SAVE',
1FILE='FOR22.DAT')
IF(IGB.EQ.1)GO TO 29
TYPE 1000
1000 FORMAT(/IX,'**GENERATOR DATA**'/IX,'>>ENTER(BUS#,ALPHA,
1BETA,GAMMA)')
29 DO 30 I=1,MBUS
IF(BTYPE(I).GE.0)GO TO 30
IF(IGB.EQ.1)GO TO 33

```

```

32      ACCEPT 2002,K,ALPHA(I),BETA(I),GAMMA(I)
2002    FORMAT(I,3F)
        IF(K.EQ.I)GO TO 31
        TYPE 1010,I
1010    FORMAT(1X,'WRONG ENTRY, BUS # SHOULD=',I3,', TRY AGAIN.')
        GO TO 32
31      GNO=GNO+1
33      WRITE(22,2003)I,ALPHA(I),BETA(I),GAMMA(I)
2003    FORMAT(I3,3F)
30      CONTINUE
        CLOSE(UNIT=22)
40      GDAT=1
        IF(IGB.EQ.1)GO TO 48

C INITIALIZING GENERATOR AND Q CONSTRAINTS
25      IF(QDAT.EQ.1)GO TO 56
        IF(TGDAT.2Q.'N')GO TO 50

C READ CONSTRAINT DATA FROM TTY/CRT.
        TYPE 1006
1006    FORMAT(/1X,'**GENERATOR CONSTRAINT DATA**'/1X,'>>ENTER FOR
        TYPE -1 & -3 BUS (BUS #,PGHAX,PGHIN)'/9X,'FOR TYPE -2 BUS
        1 (BUS #,PGHAX,PGHIN,QGHAX,QGHIN)'/9X,'FOR TYPE +2 BUS
        1 (BUS #,QGHAX,QGHIN)')
        DO 36 I=1,HBUS
35      IF(BTYPE(I).GE.0)GO TO 38
        IF(BTYPE(I).EQ.-2)GO TO 37
        ACCEPT 2005,K,PGHAX(I),PGHIN(I)
2005    FORMAT(I,2F)
        GO TO 39
37      ACCEPT 2020,K,PGHAX(I),PGHIN(I),QGHAX(I),QGHIN(I)
2020    FORMAT(I,4F)
        GO TO 39
38      IF(BTYPE(I).NE.2)GO TO 36
        ACCEPT 2005,K,QGHAX(I),QGHIN(I)
39      IF(K.EQ.I)GO TO 36
        TYPE 1015,I
1015    FORMAT(1X,'WRONG ENTRY,BUS # SHOULD BE=',I3,',TRY AGAIN.')
        GO TO 35
36      CONTINUE

C ENTER CONSTRAINT DATA INTO SOS FILE FOR23.DAT
48      OPEN(UNIT=23,DEVICE='DSK',ACCESS='SEQOUT',DISPOSE='SAVE',
        1FILE='FOR23.DAT')

        DO 52 I=1,HBUS
        IF(BTYPE(I).GE.0)GO TO 53
        IF (BTYPE(I).EQ.-2)GO TO 51
        WRITE(23,2007)I,PGHAX(I),PGHIN(I)
2007    FORMAT(1X,I3,2F11.4)
        GO TO 52
51      WRITE(23,2006)I,PGHAX(I),PGHIN(I),QGHAX(I),QGHIN(I)
2006    FORMAT(1X,I3,4F11.4)
        GO TO 52
53      IF (BTYPE(I).NE.2)GO TO 52
        WRITE(23,2009)I,QGHAX(I),QGHIN(I)
2009    FORMAT(1X,I3,22X,2F11.4)
52      CONTINUE
        CLOSE(UNIT=23)
        IF(IGB.EQ.1)GO TO 80

```



```

GO TO 54
C READ CONSTRAINT DATA FROM SOS FILE FOR23.DAT
50 OPEN(UNIT=23,DEVICE='DSK',ACCESS='SEQIN',DISPOSE='SAVE',
    1FILE='FOR23.DAT')
    DC 46 I=1,HBUS
    IF(BTYPE(I).GE.0)GO TO 42
    IF(BTYPE(I).EQ.-2)GO TO 41
    READ(23,*)K,PGHAX(I),PGHIN(I)
    GO TO 46
41 READ(23,2020)K,PGHAX(I),PGHIN(I),QGHAX(I),QGHIN(I)
    GO TO 46
42 IF(BTYPE(I).NE.2)GO TO 46
    READ(23,2005)K,QGHAX(I),QGHIN(I)
46 CONTINUE
    CLOSE(UNIT=23)
54 QDAT=1

C CHECK FOR PRINTOUT OF GENERATOR DATA
56 IF(CG.EQ.'N')GO TO 70
    IF(KINV.EQ.0)GO TO 61
    TYPE 1020,GNO
1020 FORMAT(/1X,'**SYSTEM GENERATOR DATA**'/1X,'NUMBER
    1OF GENERATORS =',I3/1X,'BUS#',4X,
    1'ALPHA',4X,'BETA',6X,'GAMMA')
    DO 60 I=1,HBUS
    IF((BTYPE(I).GE.0))GO TO 60
    TYPE 1030,I,ALPHA(I),BETA(I),GAMMA(I)
1030 FORMAT(1X,I3,3F10.5)
60 CONTINUE

C PRINT GENERATOR CONSTRAINTS
61 WRITE(5,1032)
1032 FORMAT(/1X,'**GENERATOR CONSTRAINTS**'/1X,'BUS #',
    13X,'PGHAX',5X,'PGHIN',7X,'QGHAX',6X,'QGHIN')
    DO 65 I=1,HBUS
    IF((BTYPE(I)).GE.0)GO TO 64
    IF(BTYPE(I).EQ.-2)GO TO 62
    WRITE(5,1034)I,PGHAX(I),PGHIN(I)
1034 FORMAT(1X,I3,2F11.4)
    GO TO 65
62 WRITE(5,1036)I,PGHAX(I),PGHIN(I),QGHAX(I),QGHIN(I)
1036 FORMAT(1X,I3,4F11.4)
    GO TO 65
64 IF(BTYPE(I).NE.2)GO TO 65
    WRITE(5,1038)I,QGHAX(I),QGHIN(I)
1038 FORMAT(1X,I3,22X,2F11.4)
65 CONTINUE
66 CG='N'
    IF(IGB.EQ.1)GO TO 80

C CHECK FOR GENERATOR DATA CHANGES
70 IF(CBG.EQ.'N')GO TO 180
    TYPE 1040
1040 FORMAT(/1I,'**GENERATOR DATA CHANGES**'/
    11X,'>>ENTER (VARIABLE #, BUS #, NEW VALUE THEN "CR")'/
    110X,'1=ALPHA'/10X,'2=BETA'/10X,'3=GAMMA'/10X,'4=PGHAX'/10X,'
    25=PGHIN'/10X,'6=QGHAX'/10X,'7=QGHIN'/10X,'8=RETYPE ALL
    1GENERATOR DATA'/10X,'9=UPDATE SOS FILE WITH CHANGES'
    1/10X,'>>ENTER 0 THEN "CR" WHEN CHANGES COMPLETED.')
80 READ(5,2010)NAME,I,X
2010 FORMAT(2I,F)

```

```

IF (NAME.EQ.0) GO TO 180
IF (NAME.EQ.8) GO TO 172
IF (NAME.EQ.9) GO TO 175
IF (((NAME.GE.1) .AND. (NAME.LE.7)) .AND. ((I.GE.0) .AND.
1(I.LE.MBUS))) GO TO 90
TYPE 1050, MBUS
1050  FORMAT(1X, 'WRONG ENTRY, VARIABLE MUST BE 1-8, /
11X, 'BUS # MUST BE 0 TO', I3, ', CHECK BUS TYPE IS' /
11X, 'NEGATIVE, AND TRY AGAIN.')
GO TO 80
90  CONTINUE
100  GO TO(110, 120, 130, 140, 150, 160, 170) NAME
110  ALPHA(I)=X
TYPE 1060, I, ALPHA(I)
1060  FORMAT(1X, 'ALPHA (BUS #', I3, ') =', Z12.5)
GO TO 80
120  BETA(I)=X
TYPE 1070, I, BETA(I)
1070  FORMAT(1X, 'BETA (BUS #', I3, ') =', Z12.5)
GO TO 80
130  GAMMA(I)=X
TYPE 1080, I, GAMMA(I)
1080  FORMAT(1X, 'GAMMA (BUS #', I3, ') =', Z12.5)
GO TO 80
140  PGHAX(I)=X
TYPE 1090, I, PGHAX(I)
1090  FORMAT(1X, 'PGHAX (BUS #', I3, ') =', Z12.5)
GO TO 80
150  PGHIN(I)=X
TYPE 1100, I, PGHIN(I)
1100  FORMAT(1X, 'PGHIN (BUS #', I3, ') =', Z12.5)
GO TO 80
160  QGHAX(I)=X
IF (QGHAX(I) .LT. QG(I)) QG(I) = QGHAX(I)
TYPE 1110, I, QGHAX(I)
1110  FORMAT(1X, 'QGHAX (BUS #', I3, ') =', Z12.5)
GO TO 80
170  QGHIN(I)=X
IF (QGHIN(I) .GT. QG(I)) QG(I) = QGHIN(I)
TYPE 1120, I, QGHIN(I)
1120  FORMAT(1X, 'QGHIN (BUS #', I3, ') =', Z12.5)
GO TO 80
172  CG='Y'
ICB=1
GO TO 56
175  ICB=1
IF (KINV.EQ.0) GO TO 48
GO TO 20
180  ICB=0
CHG='N'
RETURN
END

```

SUBROUTINE YBUSM
C SUBROUTINE TO CALCULATE YBUS AND ZBUS MATRIX

```

REAL LGTH
INTESER BUSH,CHI,CHZ,EB,MBUS,SB
DCUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,BJ3,BJ4,
1CALP,CALQ,DQ,DVANG,DVHAG,G,H,ITL,P,C,VANG,VHAG,
2XX,YANG,YHAG,YY,YYSH,ZANG,ZHAG,YSER,D

COMMON /      AJ1(50,50),  AJ2(50,50),  AJ3(50,50),
1AJ4(50,50),  ALPHA(50),  BDAT,      BETA(50),
1BGSOL,      BJ1(50,50),  BJ2(50,50),  BJ3(50,50),
1BJ4(50,50),  BTYPE(50),  BUSH,      CALP(50),
1CALQ(50),    CB,CC,      CG,          CHB,
1CHG,        CHL,        CL,          CHI,
1CHZ,        DQ(50),    DVANG(50),  DVHAG(50),
1EB(100),    ESP1,      ESP2,      G(50),
1GAMMA(50),  GDAT,      H(50),    IC(50),
1II,        ITER,     ITL(50),  KINV,
1LAMBDA,    LDAT,     LITER,
1LNGTH(100), LNO,      LOSS,
1LSET,      MBUS,     N5,      LPSOL,
1P(50),     PD(50),    PG(50),  HSHCB,
1PGMIN(50), Q(50),    QD(50),  PGMAX(50),
1QGMAY(50), QGMIN(50), SB(100),  QG(50),
1TCL,TLDAT, TPD,IBDAT, TPL,IGDAT,  YYSH(100,2),
1VHAG(50),  XX(50,50),  YANG(50,50),  VANG(50),
1YHAG(50,50), YSH(100,2), YY(50,50),  ZANG(50,50),
1ZHAG(50,50), ZSER(100,2), YSER(100,2),  ABORT

IF ((BUSH.EQ.2).OR.((KINV.EQ.0).AND.(BUSH.EQ.1))) GO TO 90
TYPE 1000
OPEN(UNIT=24,DEVICE='DSK',ACCESS='SEQOUT',DISPOSE='SAVE',
1FILE='POR24.DAT')

1000  FORMAT(/1X,'**GENERATING YBUS MATRIX**')

C CALCULATING LINE SHUNT AND SERIES ADMITTANCE
DO 15 I=1,LNO
  YYSHT(I,1)=(DBLE(YSH(I,1))*DBLE(LNGTH(I)))/2.0D0
  YYSHT(I,2)=(DBLE(YSH(I,2))*DBLE(LNGTH(I)))/2.0D0
  D=(DBLE(LNGTH(I))*((DBLE(ZSER(I,1))*DBLE(ZSER(I,1)))
  1+(DBLE(ZSER(I,2))*DBLE(ZSER(I,2))))
  IF(D.EQ.0.0D0)GO TO 20
  YSER(I,1)=DBLE(ZSER(I,1))/D
  YSER(I,2)=-DBLE(ZSER(I,2))/D
GO TO 15
20  YSER(I,1)=0.0D0
  YSER(I,2)=0.0D0
15  continue
DO 1 I=1,LNO
  WRITE(24,2000) YYSHT(I,1),YYSHT(I,2),YSER(I,1),YSER(I,2)
2000  FORMAT(4D)

C CALCULATING YBUS MATRIX
DO 30 I=1,MBUS
DO 30 J=1,MBUS
  YHAG(I,J)=0.0D0
  YANG(I,J)=0.0D0
  AJ1(I,J)=0.0D0
  AJ2(I,J)=0.0D0
  IF(J.EQ.I)GO TO 60

```

```

C OFF DIAGONAL ELEMENTS (I.NE.J)
DO 40 L=1,LNO
  IF ((SB(L).EQ.I).AND.(EB(L).EQ.J)).OR.((SB(L).EQ.J)
  1.AND.(EB(L).EQ.I)) GO TO 42
  GO TO 40
42  YMAG(I,J)=DSQRT((YSER(L,1)*YSER(L,1))+(YSER(L,2)*YSER(L,2)))
  IF(YSER(L,1).EQ.(0.0D0)) GO TO 22
  YANG(I,J)=DATAN2(-YSER(L,2),-YSER(L,1))
  GO TO 29
22  IF(YSER(L,2)) 24,26,28
24  YANG(I,J)=1.570796326794897
  GO TO 29
26  YANG(I,J)=0.0D0
  GO TO 29
28  YANG(I,J)=-1.570796326794897
29  IF(KINV.EQ.0) GO TO 40
  AJ1(I,J)=-YSER(L,1)
  AJ2(I,J)=-YSER(L,2)
40  CONTINUE
  GO TO 30

C ON DIAGONAL ELEMENTS (I.EQ.J)
60  DO 45 L=1,LNO
  IF ((SB(L).EQ.I).OR.(EB(L).EQ.I)) GO TO 46
  GO TO 45
46  AJ1(I,J)=AJ1(I,J)+YSHT(L,1)+YSER(L,1)
  AJ2(I,J)=AJ2(I,J)+YSHT(L,2)+YSER(L,2)
45  CONTINUE
  YMAG(I,J)=DSQRT(AJ1(I,J)*AJ1(I,J)+AJ2(I,J)*AJ2(I,J))
  IF(AJ1(I,J).EQ.(0.0D0)) GO TO 31
  YANG(I,J)=DATAN2(AJ2(I,J),AJ1(I,J))
  GO TO 30
31  IF(AJ2(I,J)) 32,33,34
32  YANG(I,J)=-1.570796326794897
  GO TO 30
33  YANG(I,J)=0.0D0
  GO TO 30
34  YANG(I,J)=+1.570796326794897
30  CONTINUE
  DO 2 I=1,HBUS
  2  WRITE(24,2010) (YMAG(I,J),YANG(I,J),J=1,HBUS)
2010  FORMAT(2D)
35  BUSH=1
  IF(KINV.EQ.0) GO TO 90

C CALCULATING ZBUS MATRIX
TYPE 1005
1005  FORMAT(15X,'**CALCULATING ZBUS MATRIX**')
  DO 50 I=1,HBUS
  DO 50 J=1,HBUS
  50  BJ1(I,J)=AJ1(I,J)
  BJ2(I,J)=AJ2(I,J)
  BJ3(I,J)=0.0D0
  BJ4(I,J)=0.0D0
  CALL CTRI(BJ1,BJ2,BJ3,BJ4,HBUS)
  CALL CTRIV(BJ3,BJ4,BJ1,BJ2,HBUS)
  DO 80 I=1,HBUS
  DO 80 J=1,HBUS
  ZMAG(I,J)=DSQRT(BJ1(I,J)*BJ1(I,J)+BJ2(I,J)*BJ2(I,J))
  IF(BJ1(I,J).EQ.0.0D0) GO TO 82
  80  ZMAG(I,J)=DATAN2(BJ2(I,J),BJ1(I,J))

```

```

      GO TO 81
82     IF (BJ2(I,J)) 83,84,85
83     ZANG(I,J)=-1.570796326794897
      GO TO 81
84     ZANG(I,J)=0.0D0
      GO TO 81
85     ZANG(I,J)=1.570796326794897
81     CONTINUE
      DO 4 I=1,MBUS
4       WRITE(24,2010) (ZHAG(I,J),ZANG(I,J),J=1,MBUS)
      BUSH=2

```

C PRINTOUT OF YBUS AND ZBUS MATRIX

```

90     CLOSE(UNIT=24)
      IF (CHY.EQ.'N') GO TO 105
      TYPE 4000
4000    FORMAT(/1X,'**CALCULATED SYSTEM LINE DATA**'/1X,
1'LINE #',15X,'Y SHUNT',23X,'Y SERIES')
      DO 95 I=1,LNO
4100    TYPE 4100,I,YYSH(I,1),YYSH(I,2),YSER(I,1),YSER(I,2)
95     FORMAT(I4,4X,2E14.6,2X,2E14.6)
      CONTINUE
      TYPE 1010
1010    FORMAT(/1X,'**YBUS MATRIX**')
      DO 100 I=1,MBUS
      TYPE 1020,I
1020    FORMAT(1X,'ROW',I3)
      TYPE 1030,(YHAG(I,J),YANG(I,J),J=1,MBUS)
1030    FORMAT(6E12.5)
100     CONTINUE
      CHY='N'
105     IF (KINV.EQ.0) GO TO 120
      IF (CNZ.EQ.'N') GO TO 120
      TYPE 1040
1040    FORMAT(/1X,'**ZBUS MATRIX**')
      DO 110 I=1,MBUS
      TYPE 1020,I
      TYPE 1030,(ZHAG(I,J),ZANG(I,J),J=1,MBUS)
110     CONTINUE
      CNZ='N'
120     RETURN
      END

```

C SUBROUTINE WRLF
CALCULATES P,Q,V,AND ANGLE AT EACH BUS
INTEGER ABORT,BTYPE, MBUS
DIMENSION DP(50)

DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,EJ3,BJ4,
1CALP,CALQ,DQ,DVANG,DVHAG,G,H,ITL,P,Q,YANG,VHAG,
2YX,YANG,YHAG,YY,YYSH,ZANG,ZHAG,YSER,GHAX,HHAX,DP

COMMON /	AJ1(50,50),	AJ2(50,50),	AJ3(50,50),
1AJ4(50,50),	ALPHA(50),	BDAT,	BETA(50),
1BGSOL,	BJ1(50,50),	BJ2(50,50),	BJ3(50,50),
1BJ4(50,50),	BTYPE(50),	BUSH,	CALP(50),
1CALQ(50),	CB,CC,	CG,	CHB,

```

1CHG,          CHL,          CL,          CMY,
1CHZ,          DQ(50),       DVANG(50),  DVHAG(50),
1EB(100),      ESP1,          ESP2,       G(50),
1GAMMA(50),   GDAT,          H(50),     IC(50),
1II,          ITER,       ITL(50),   KINV,
1LAMBDA,      LDAT,          LITER,
1LNTH(100),   LNO,          LOSS,
1LSET,        MBUS,         N5,        LPSOL,
1P(50),       PD(50),       PG(50),    MSUGB,
1PGMIN(50),   Q(50),        QD(50),QD,  PGMAX(50),
1QGHAX(50),   QGHIN(50),    SB(100),   QG(50),
1TOL, TLDAT,  TPD,TBDAT,   TPL,TGDAT,  YYSHT(100,2),
1VNAG(50),    XI(50,50),   YANG(50,50),  VANG(50),
1YHAG(50,50), YSHT(100,2),  YI(50,50),  ZANG(50,50),
1ZHAG(50,50), ZSER(100,2),  YSER(100,2),  ABORT,IBT(50)

LL=0
TYPE 100
100  FORMAT(/IX,'**SOLVING LOAD FLOW EQUATIONS BY NR**')
C    CALCULATING G AND H AT EACH BUS
    IF(LSET.EQ.1) GO TO 13
    DO 1 I=1,MBUS
      P(I)=DBLE(PG(I))-DBLE(PD(I))
      Q(I)=DBLE(QG(I))-DBLE(QD(I))
1    CONTINUE
13   CONTINUE
    DO 7 I=1,MBUS
      CALP(I)=0.000
      CALQ(I)=0.000

      DO 4 J=1,MBUS
        CALP(I)=CALP(I)+VHAG(I)*VHAG(J)*YHAG(I,J)
        1*DCOS(YANG(I,J)-VANG(I)+VANG(J))
        CALQ(I)=CALQ(I)-VHAG(I)*VHAG(J)*YHAG(I,J)
        1*DSIN(+YANG(I,J)-VANG(I)+VANG(J))
4    CONTINUE

      G(I)=P(I)-CALP(I)
      H(I)=Q(I)-CALQ(I)

7    CONTINUE
C    CHECK FOR CONVERGENCE(GMAX & HMAX.LT.TOL)

      GMAX=0.000
      HMAX=0.000

      DO 5 I=1,MBUS
        IF(GMAX.LT.DABS(G(I))) GMAX=DABS(G(I))
        IF(HMAX.LT.DABS(H(I))) HMAX=DABS(H(I))
5    CONTINUE
      IF((GMAX.LE.TOL).AND.(HMAX.LE.TOL)) GO TO 56
C*****GENERATING JACOBIAN AJ1
      DO 6 I=1,MBUS
        DO 8 J=1,MBUS
          IF(IABS(BTYPE(J)).EQ.3) GO TO 10
          IF(J.EQ.I) GO TO 9
          AJ1(I,J)=-VHAG(I)*VHAG(J)*YHAG(I,J)

```

```

1*DSIN(YANG(I,J)-VANG(I)+VANG(J))
GO TO 8
9   AJ1(I,J)=0.000

DO 12 K=1,MBUS
IF (K.EQ.I) GO TO 12
AJ1(I,J)=AJ1(I,J)+VHAG(I)*VHAG(K)+YHAG(I,K)
12  1*DSIN(YANG(I,K)-VANG(I)+VANG(K))
CONTINUE

GO TO 8
10  IF(J.EQ.I) GO TO 11
AJ1(I,J)=0.000
GO TO 8
11  AJ1(I,J)=-1.000

8   CONTINUE
6   CONTINUE

C*****GENERATING JACOBIAN AJ2
DO 14 I=1,MBUS

DO 17 J=1,MBUS
IF(IABS (BTYPE(J)).GT.1) GO TO 18
IF(J.EQ.I) GO TO 15
AJ2(I,J)=VHAG(I)*YHAG(I,J)
1*DCOS(YANG(I,J)-VANG(I)+VANG(J))
GO TO 17

15  AJ2(I,J)=0.000
DO 19 K=1,MBUS
IF (K.NE.I) GO TO 16
AJ2(I,J)=AJ2(I,J)+2*VHAG(I)*YHAG(I,I)
1*DCOS(+YANG(I,I))
GC TO 19
CCONTINUE
16  AJ2(I,J)=AJ2(I,J)+VHAG(K)*YHAG(I,K)
1*DCOS(YANG(I,K)-VANG(I)+VANG(K))
19  CONTINUE
GO TO 17

18  AJ2(I,J)=0.000

17  CONTINUE
14  CONTINUE

C*****GENERATING JACOBIAN AJ3
DO 20 I=1,MBUS

DO 24 J=1,MBUS
IF(IABS (BTYPE(J)).EQ.3) GO TO 22
IF(J.EQ.I) GO TO 23
AJ3(I,J)=-VHAG(I)*VHAG(J)+YHAG(I,J)
1*DCOS(YANG(I,J)-VANG(I)+VANG(J))

GO TO 24
23  AJ3(I,J)=0.000

DO 21 K=1,MBUS
IF(K.EQ.J) GO TO 21
AJ3(I,J)=AJ3(I,J)+VHAG(I)*VHAG(K)+YHAG(I,K)

```

```

21      1*DCOS(YANG(I,K)-VAKG(I)+VANG(K))
        CONTINUE
        GO TO 24

22      AJ3(I,J)=0.0D0

24      CCNTINJE
20      CONTINUE

C***** GENERATING JACOBIAN AJ4
        DO 29 I=1,NBUS

        DO 25 J=1,NBUS
        IF (IABS(BTYPE(J)).GT.1) GO TO 27
        IF (J.EQ.I) GO TO 28
        AJ4(I,J)=-VHAG(I)*YHAG(I,J)
        1*DSIN(YANG(I,J)-VANG(I)+VANG(J))
        GO TO 25

28      AJ4(I,J)=0.0D0

        DO 26 K=1,NBUS
        IF (K.NE.I) GO TO 30
        AJ4(I,J)=AJ4(I,J)-2*VHAG(I)*YHAG(I,I)
        1*DSIN(+YANG(I,I))
        GO TO 26

30      CONTINUE

        AJ4(I,J)=AJ4(I,J)-VHAG(K)*YHAG(I,K)
        1*DSIN(YANG(I,K)-VANG(I)+VANG(K))
26      CONTINUE
        GO TO 25

27      IF (J.EQ.I) GO TO 31
        AJ4(I,J)=0.0D0
        GO TO 25

31      AJ4(I,J)=-1.0D0
25      CONTINUE
29      CONTINUE

C      INVERTING JACOBIAN AJ4
        CALL MINV(AJ4,NBUS)

C*****GENERATING INVERSE SUBMATRIX EJ1, EJ2, EJ3, BJ4
C      BJ1=[ AJ1-AJ2(AJ4***-1) AJ3 ]***-1

        CALL ABULT(IX,AJ2,AJ4,NBUS)
        CALL ABULT(YI,XI,AJ3,NBUS)
        DO 37 I=1,NBUS

        DO 39 J=1,NBUS
        BJ1(I,J)=AJ1(I,J)-YI(I,J)
39      CONTINUE
37      CONTINUE

C      INVERTING JACOBIAN BJ1
        CALL MINV(BJ1,NBUS)

C*****GENERATING JACOBIAN BJ2

```



```

C      BJ2=-BJ1*AJ2*(AJ4**1)

      CALL ANULT (YY,BJ1,AJ2,MBUS)
      CALL ANULT (BJ2,YY,AJ4,MBUS)
      DO 44 I=1,MBUS
      DO 45 J=1,MBUS
      BJ2(I,J)=-1.000*(BJ2(I,J))
45     CONTINUE
44     CONTINUE

C*****GENERATING JACOBIAN BJ3
C      BJ3=- (AJ4**1)*AJ3*BJ1
      CALL ANULT (YY,AJ3,BJ1,MBUS)
      CALL ANULT (BJ3,AJ4,YY,MBUS)

      DO 47 I=1,MBUS

      DO 48 J=1,MBUS
      BJ3(I,J)=-1.000*BJ3(I,J)

48     CONTINUE
47     CONTINUE

C*****GENERATING JACOBIAN BJ4
C      BJ4=(AJ4**1)-(AJ4**1)*AJ3*BJ2
      CALL ANULT (YY,AJ4,AJ3,MBUS)
      CALL ANULT (XX,YY,BJ2,MBUS)
      DO 51 I=1,MBUS
      DO 50 J=1,MBUS
      BJ4(I,J)=AJ4(I,J)-XX(I,J)
50     CONTINUE
51     CONTINUE

C      CALCULATING DELTA P,Q,VHAG,ANGLE
      DO 52 I=1,MBUS
      DP(I)=0.000
      DQ(I)=0.000
      DVHAG(I)=0.000
      DVANG(I)=0.000
      IF (IABS(BTYPE(I))-EQ.3) GO TO 54
      IF (IABS(BTYPE(I))-EQ.2) GO TO 55
      DO 53 J=1,MBUS
      DVHAG(I)=DVHAG(I)+BJ3(I,J)*G(J)+BJ4(I,J)*H(J)
53     DVANG(I)=DVANG(I)+BJ1(I,J)*G(J)+BJ2(I,J)*H(J)
      GO TO 52
54     DO 64 J=1,MBUS
      DP(I)=DP(I)+BJ1(I,J)*G(J)+BJ2(I,J)*H(J)

54     DQ(I)=DQ(I)+BJ3(I,J)*G(J)+BJ4(I,J)*H(J)
      GO TO 52
55     DO 65 J=1,MBUS
      DQ(I)=DQ(I)+BJ3(I,J)*G(J)+BJ4(I,J)*H(J)
55     DVANG(I)=DVANG(I)+BJ1(I,J)*G(J)+BJ2(I,J)*H(J)
52     CONTINUE
C      CALCULATING NEW P,Q,V,ANGLE
      DO 62 I=1,MBUS
      P(I)=P(I)+DP(I)
      Q(I)=Q(I)+DQ(I)
      VHAG(I)=VHAG(I)+DVHAG(I)
      VANG(I)=VANG(I)+DVANG(I)

```

```

IF (IABS(BTYPE(I)).NE.2) GO TO 62
QHAX=QGHAX(I)-QD(I)
QHIX=QGHIX(I)-QD(I)
IF (Q(I).LT.DBLE(QHAX)) GO TO 58
Q(I)=DBLE(QHAX)
BTYPE(I)=ISIGN(1,BTYPE(I))
IBT(I)=2
TYPE 3000,I
3000  FORMAT(1X,'BUS #',I3,2X,'EXCEEDS QGHAX,
      1BUS CHANGED TO TYPE 1')
      GO TO 62
58    IF (Q(I).GT.DBLE(QHIX)) GO TO 62
      Q(I)=DBLE(QHIX)
      BTYPE(I)=ISIGN(1,BTYPE(I))
      IBT(I)=2
      TYPE 3001,I
3001  FORMAT(1X,'BUS #',I3,2X,'EXCEEDS QGHIX,
      1BUS CHANGED TO TYPE 1')
62    CONTINUE
      LL=LL+1
      IF (LL.LT.LITER) GO TO 13

      TYPE 2300,LL
2300  FORMAT(1X,'****WILL NOT CONVERGE IN',I3,2X,' ITERATIONS')
      ABORT=1
      GO TO 60

C      PRINT OUT SOLUTIONS
56     TYPE 2400,LL
2400  FORMAT(1X,'****NR CONVERGENCE IN',I3,' ITERATIONS')
      DO 70 I=1,NBUS
      PG(I)=P(I)+PD(I)
70     QG(I)=Q(I)+QD(I)
60     RETURN
      END

```

SUBROUTINE OPT
C SUBROUTINE TO CALCULATE ITL, IC, AND POWER FOR EACH GENERATOR
C CALCULATES OPTIMUM LAMBDA FOR SYSTEM

```

REAL IC,LAMBDA
INTEGER ABORT,BTYPE,NBUS
DIMENSION PGSIV(50)

DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,BJ3,BJ4,
1CALP,CALQ,DQ,DVANG,EVHAG,G,H,ITL,P,C,VANG,VHAG,
2XX,YANG,YHAG,YY,YSHT,ZANG,ZHAG,YSER,A,B
COMMON / / AJ1(50,50), AJ2(50,50), AJ3(50,50),
1AJ4(50,50), ALPHA(50), BDAT, BETA(50),
1BGSOL, BJ1(50,50), BJ2(50,50), BJ3(50,50),
1BJ4(50,50), BTYPE(50), EUSB, CALP(50),
1CALQ(50), CB,CC, CG, CHB,
1CHG, CHL, CL, CHY,
1CMZ, DQ(50), DVANG(50), DVHAG(50),
1EB(100), ESP1, ESP2, G(50),
1GAMMA(50), GDAT, H(50), IC(50),
1II, ITER, ITL(50), KINV,
1LAMBDA, LDAT, LITER,

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```

1LNTH(100), LNO, LOSS, LPSOL,
1LSET, MBUS, N5, NSUGB,
1P(50), PD(50), PG(50), PGMAX(50),
1PGMIN(50), Q(50), QD(50), QDAT, QG(50),
1QGMAX(50), QGMIF(50), SB(100), YYSHT(100,2),
1TOL, TLDAT, TPD, TDDAT, TPL, TGDAT, VANG(50),
1YHAG(50), XX(50,50), YANG(50,50),
1YHAG(50,50), YSHT(100,2), YY(50,50), ZANG(50,50),
1ZHAG(50,50), ZSER(100,2), YSER(100,2), ABOBT, IBT(50)

II=0
5 L=0
TPD=0.0
TPL=0.0
TPGCC=0.0

C COMPUTE TOTAL POWER DEMAND & LCSS AND TOTAL POWER
C GENERATED AT CONSTANT COST
DO 10 I=1,MBUS
TPD=TPD+PD(I)
TPL=TPL+P(I)
IF(BTYPE(I).GE.0)GO TO 10
IF((ALPHA(I).EQ.0.0).AND.(BETA(I).EQ.0.0).AND.
1(GAMMA(I).EQ.0.0).EQ.0.0)TPGCC=TPGCC+PGMAX(I)
10 CONTINUE

C CHECK FOR NEGATIVE TOTAL POWER LOSS
IF(TPL.GE.0.0)GO TO 20
TYPE 1000
1000' FORMAT(11X,'SYSTEM POWER LOSS IS NEGATIVE.'/11X,' CHECK
1TOTAL SYSTEM POWER GENERATION')
RETURN

20 IF(LOSS.EQ.'Y')TPL=0.0
IF(TPGCC.LT.(TPD+TPL))GO TO 30
TYPE 1010
1010' FORMAT(11X,'MAX CONSTANT COST POWER NOT USED.'/11X,
1'LOAD FLOW PROBLEM CNLY')
RETURN

C DETERMINE INITIAL LAMBDA
30 IF(LSET.EQ.1)GO TO 40
LAMBDA=5000.0
DO 50 I=1,MBUS
IF((BTYPE(I).GE.0).OR.(ALPHA(I).EQ.0))GO TO 50
IF(ALPHA(I).LT.LAMBDA)LAMBDA=ALPHA(I)
PGSAV(I)=PG(I)
50 CONTINUE
DLAM=0.8*LAMBDA
LSET=1
40 TYPE 1020
1020' FORMAT(5X,'***OPTIMIZING COST FUNCTIONS***')

C SKIP ITL CALCULATIONS IF LOSSLESS SYSTEM
IF(LOSS.EQ.'Y')GO TO 60

C CALCULATING ITL'S
DO 70 I=1,MBUS
IF(BTYPE(I).GE.0)GO TO 70
ITL(I)=0.0D0
DO 80 J=1,MBUS

```

```

      IF (BTYPE(J) .GE. 0) GO TO 80
      A = ((ZMAG(I, J) * DCOS(ZANG(I, J))) / (VMAG(I) * VMAG(J))) *
      1DCOS(VANG(I) - VANG(J))
      B = ((ZMAG(I, J) * DCOS(ZANG(I, J))) / (VMAG(I) * VMAG(J))) *
      1DSIN(VANG(I) - VANG(J))
      ITL(I) = ITL(I) + (P(J) * A - Q(J) * B)
80     CONTINUE
      ITL(I) = ITL(I) + ITL(I)
70     CONTINUE

C OPTIMIZING LAMBDA
60     DPSAV = 0.0
85     CONTINUE
      TPG = 0.0
      DO 90 I = 1, MBOS
      IF (BTYPE(I) .GE. 0) GO TO 90
      IF ((ALPHA(I) .EQ. 0.0) .AND. (BETA(I) .EQ. 0.0) .AND.
      1(GAMMA(I) .EQ. 0.0)) GO TO 100
      IF (LOSS .EQ. 'M') GO TO 110
      IC(I) = LAMBDA
      GO TO 120
110    IC(I) = LAMBDA * (1.0 - ITL(I))
      IF (IC(I) .GE. ALPHA(I)) GO TO 120
      PG(I) = 0.0
      GO TO 89

C COMPUTE PG'S FROM COST FUNCTIONS
120    IF (GAMMA(I) .NE. 0.0) GO TO 130
      PG(I) = (IC(I) - ALPHA(I)) / BETA(I)
      GO TO 89
130    C = BETA(I) * BETA(I) - 4.0 * (ALPHA(I) - IC(I)) * GAMMA(I)
      IF (C .GE. 0.0) GO TO 140
C     TYPE 1030, I
1030   FORMAT(1X, 'COST CURVE COEFFICIENTS GIVE NEGATIVE
      1DETERMINANT, GENERATOR', I3, 2X, 'SET TO ZERO')
135    PG(I) = 0.0
      GO TO 89
140    C = SQRT(C)
      PG(I) = (-BETA(I) + C) / (2.0 * GAMMA(I))
      IF (PG(I) .GE. PGMIN(I)) GO TO 89
      PG(I) = (-BETA(I) - C) / (2.0 * GAMMA(I))
      IF (PG(I) .GE. PGMIN(I)) GO TO 89
      PG(I) = PGMIN(I)
C     TYPE 1032, I
1032   FORMAT(1X, I3, 1X, 'PG NEG, GEN. SET TO 0.0')
      GO TO 89
100    PG(I) = PGMAX(I)
      IF ((ALPHA(I) .EQ. 0.0) .AND. (BETA(I) .EQ. 0.0) .AND.
      1(GAMMA(I) .EQ. 0.0)) GO TO 150
89     CONTINUE

C CHECK FOR PGMAX CONSTRAINTS
      IF (PG(I) .LE. PGMAX(I)) GO TO 105
      PG(I) = PGMAX(I)
C     TYPE 1036, I, PGMAX(I)
1036   FORMAT(1X, I3, 'PG EXCEEDS PGMAX, GEN RESET TO', F12.7)
      GO TO 165
105    IF (PG(I) .GE. PGMIN(I)) GO TO 150
      PG(I) = PGMIN(I)
C     TYPE 1038, I, PGMIN(I)
1038   FORMAT(1X, I3, 1X, 'PG EXCEEDS PGMIN, GEN RESET TO', F12.5)

```

```

165     IF (GAMMA(I) .NE. 0.0) GO TO 160
        IC(I) = ALPHA(I) + BETA(I) * PG(I)
        GO TO 150
160     IC(I) = ALPHA(I) + BETA(I) * PG(I) + GAMMA(I) * PG(I) * PG(I)
150     TPG = TPG + PG(I)
90      CONTINUE

C CHECK POWER BALANCE LESS THAN ESP1
DP = TPG - TPD - TPL
IF (ABS(DP) .LE. ESP1) GO TO 210
L = L + 1
IF (L .LE. ITER) GO TO 170
TYPE 1040, L
1040   FORMAT(11X, 'POWER BALANCE EQUATIONS NOT SATISFIED IN'
1, I3, 2X, 'ITERATIONS, ' / 11X, 'CHECK COST CURVES AND
2TOLERANCES')
RETURN

C ADJUST LAMBDA IN COMPARISON TO PREVIOUS ITERATION
170     IF ((DPSAV .GE. 0.0) .AND. (DP .GT. 0.0)) GO TO 180
        IF ((DPSAV .LE. 0.0) .AND. (DP .LT. 0.0)) GO TO 190
        IF ((DPSAV .GE. 0.0) .AND. (DP .LT. 0.0)) GO TO 200
        DLAM = 0.5 * DLAM
180     LAMBDA = LAMBDA - DLAM
        DPSAV = DP
        GO TO 85
200     DLAM = 0.5 * DLAM
190     LAMBDA = LAMBDA + DLAM
        DPSAV = DP
        GO TO 85
210     II = II + 1
        TYPE 1050, L
1050   FORMAT(11X, 'LAMBDA DETERMINED IN ', I3, 2X, 'ITERATIONS')

C CHECK PG(I) CONVERGENCE .LE. ESP2
DO 220 I = 1, MBUS
IF (BTYPE(I) .GE. 0) GO TO 220
IF (ABS(PG(I) - PGSV(I)) .GT. ESP2) GO TO 230
220   CONTINUE
RETURN

230   DO 240 I = 1, MBUS
        PGSV(I) = PG(I)
        P(I) = DBLE(PG(I)) - DBLE(PD(I))
        IF (IBT(I) .NE. 2) GO TO 240
        BTYPE(I) = ISIGN(2, BTYPE(I))
        VHAG(I) = 1.0
        IBT(I) = 0
240   CONTINUE
        DLAM = 0.5 * LAMBDA
250   CALL NRLF
        GO TO 5
END

```

```

SUBROUTINE CTRI(A, B, C, D, N)
DOUBLE PRECISION A(50,50), B(50,50), C(50,50), D(50,50), T(2), SUM(2)

```

```

C TRIANGULARIZE A INTO B (LOWER) AND

```

```

C      B UPPER TRIAG MATRIX
      DO 100 I=1,N
        C(I,1)=A(I,1)
100     D(I,1)=B(I,1)
        DO 105 J=2,N
          CALL CDIV(T(1),T(2),A(1,J),
            1B(1,J),A(1,1),B(1,1))
          C(1,J)=T(1)
105     D(1,J)=T(2)

        DO 275 IJ=2,N
          DO 250 J=IJ,N
            DO 250 I=IJ,N
              IF(I.LT.J) GO TO 205
              JH1=J-1
              SUM(2)=0.000
              SUM(1)=SUM(2)
              DO 200 K=1,JH1
                CALL CHUL(T(1),T(2),C(I,K),
1          D(I,K),C(K,J),D(K,J))
                SUM(1)=SUM(1)+T(1)
200     SUM(2)=SUM(2)+T(2)
                C(I,J)=A(I,J)-SUM(1)
                D(I,J)=B(I,J)-SUM(2)
              GO TO 250
205     CONTINUE
              CALL CDIV(T(1),T(2),C(J,I),
1          D(J,I),C(I,I),D(I,I))
              C(I,J)=T(1)
              D(I,J)=T(2)
250     CONTINUE
275     CONTINUE

        DO 280 I=1,N
          DO 280 J=1,N
            IF(I.GE.J) GO TO 280
            D(I,J)=0.000
            C(I,J)=D(I,J)
280     CONTINUE
          RETURN
        END

      SUBROUTINE CTRIV(A,B,C,D,N)
      DOUBLE PRECISION A(50,50),B(50,50),C(50,50),D(50,50),
        1SUM(2),T(2),AI

      I=N
10     CONTINUE
      K=I
20     CONTINUE
      SUM(2)=0.000
      SUM(1)=SUM(2)
      AI=SUM(1)
      IF(K-I) 25,22,25
22     AI=1.000
25     J=K+1
      IF(J.GT.N) GO TO 40

      DO 30 JJ=J,N
        CALL CHUL(T(1),T(2),A(JJ,K),

```

```

1 B(JJ,K),C(I,JJ),D(I,JJ)
SUM(1)=SUM(1)+T(1)
30 SUM(2)=SUM(2)+T(2)
40 T(1)=I-SUM(1)
T(2)=-SUM(2)
CALL CDIV(SUM(1),SUM(2),T(1),T(2))
1,A(K,K),B(K,K)
C(K,I)=SUM(1)
C(I,K)=C(K,I)
D(K,I)=SUM(2)
D(I,K)=D(K,I)

K=K-1
IF(K.EQ.0) GO TO 50
GO TO 20
50 I=I-1
IF(I.EQ.0) GO TO 60
GO TO 10
60 CONTINUE

RETURN

END

```

SUBROUTINE SOL

C SUBROUTINE TO CALCULATE AND PRINT BUS & GENERATOR SOLUTIONS
C AND LINE POWER FLOW

```

REAL LAMBDA,IC
INTEGER BTYPE,BGSOL,EB,SB
DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,BJ3,BJ4,
1CALP,CALQ,DQ,DVANG,DVHAG,C,H,ITL,P,Q,VANG,VHAG,
2IX,YANG,YMAG,YY,YSHT,ZANG,ZHAG,YSER,
3YA,YM,YSHTA,YSHTB,PLM,QLM

```

```

COMMON / / AJ1(50,50), AJ2(50,50), AJ3(50,50),
1AJ4(50,50), ALPHA(50), BDAT, BETA(50),
1BGSOL, BJ1(50,50), BJ2(50,50), BJ3(50,50),
1BJ4(50,50), BTYPE(50), BUSM, CALP(50),
1CALQ(50), CB,CC, CG, CHB,
1CHG, CHL, CL, CHY,
1CNZ, DQ(50), DVANG(50), DVHAG(50),
1EB(100), ESP1, ESP2, G(50),
1GAMMA(50), GDAT, H(50), IC(50),
1II, ITER, ITL(50), KINV,
1LAMBDA, LDAT, LITER, LOSS,
1LNCTH(100), LNO, LOSS, LPSOL,
1LSET, MBUS, NS, NSWGB,
1P(50), PD(50), PG(50), PGMAX(50),
1PGMIN(50), Q(50), QD(50),QDAT, QG(50),
1QGMAX(50), QGMIN(50), SB(100), YSHT(100,2),
1TOL,TLDAT, TPD,TBDAT, TPL,TGEAT, YANG(50),
1VMAG(50), XX(50,50), YANG(50,50),
1YMAG(50,50), YSHT(100,2), YY(50,50), ZANG(50,50),
1ZHAG(50,50), ZSER(100,2), YSER(100,2), ABORT

```

```

IF (BGSOL.EQ.0) GO TO 280
IF (KINV.EQ.1) GO TO 265
TPD=0.0
TPL=0.0
DO 275 I=1, NBUS
  TPD=TPD+PD(I)
  TPL=TPL+P(I)
275 CONTINUE
  WRITE (N5, 1157) TPL, TPD
1157 FORMAT (/1X, '****SYSTEM BUS AND GENERATOR SOLUTIONS****'/
  11X, 'SYSTEM LOSSES (PU)=' , F8.4, ', SYSTEM LOAD (PU)=' , F8.4, /
  21X, 'BUS #', 1X, 'BTYPE', 6X, 'PG', 6X, 'QG', 6X, 'PD', 6X,
  3'QD', 5X, 'VMAG', 4X, 'VANG')
  DO 277 I=1, NBUS
    PG(I)=P(I)+PD(I)
    QG(I)=Q(I)+QD(I)
277 WRITE (N5, 1158) I, BTYPE(I), PG(I), QG(I), PD(I), QD(I),
  1VMAG(I), VANG(I)
1158 FORMAT (1X, I3, 3X, I3, 4X, 6F8.4)
  BGSOL=0
  GO TO 280
265 WRITE (N5, 1155) II, ESP1, ESP2, LAMBDA, TPL, IPD
1155 FORMAT (/1X, '****SYSTEM BUS AND GENERATOR SOLUTIONS****'/
  16X, 'ECON. DISPATCH CONVERGENCE IN', I3, ' ITERATIONS' /
  12X, 'ESP1=' , F8.4, ', ESP2=' , F8.4, ', LAMBDA=' , F8.4, /1X, 'SYSTEM
  3LOSSES (PU)=' , F8.4, ', SYSTEM LOAD (PU)=' , F8.4, /
  41X, 'BUS #', 1X, 'BTYPE', 4X, 'IC', 5X, 'IIL', 6X, 'PG', 6X,
  5'QG', 6X, 'PD', 6X, 'QD', 5X, 'VMAG', 4X, 'VANG')

  DO 270 I=1, NBUS
    PG(I)=P(I)+PD(I)
    QG(I)=Q(I)+QD(I)
270 WRITE (N5, 1160) I, BTYPE(I), IC(I), IIL(I), PG(I), QG(I),
  1PD(I), QD(I), VMAG(I), VANG(I)
1160 FORMAT (1X, I3, 1X, I3, F10.4, 7F8.4)
  BGSOL=0
280 CONTINUE
  IF (LPSOL.EQ.0) GO TO 300
  IF (KINV.EQ.0) GO TO 287

C CALCULATING BUS POWER COST
  B=0.0
  C=0.0
  WRITE (N5, 1165)
1165 FORMAT (/1X, '****SYSTEM OPERATING COST****')
  DO 285 I=1, NBUS
    IF (BTYPE(I).GE.0) GO TO 285
    B=ALPHA(I)*PG(I)+(BETA(I)*PG(I)*PG(I))/2
    C=(GAMMA(I)*PG(I)*PG(I)*PG(I))/3
    WRITE (N5, 1170) I, B
1170 FORMAT (1X, 'GEN. #', I3, '=' , F8.2, 'P.U.')
  C=C+B
285 CONTINUE
  WRITE (N5, 1180) C
1180 FORMAT (1X, 'TOTAL SYSTEM OPERATING COST =' , F10.2, 'P.U.')

C CALCULATING LINE POWER FLOW
287 WRITE (N5, 1190)
1190 FORMAT (/1X, '****LINE POWER FLOW****'/1X, 'LINE #', 3X, 'SB', 4X, 'EB',
  14X, 'REAL POWER', 4X, 'REACTIVE POWER')

```



```

DO 300 I=1,LNO
L=SB(I)
M=EB(I)
YH=DSQRT((YSER(I,1)*YSER(I,1))+(YSER(I,2)*YSER(I,2)))
YSHTH=DSQRT((YYSHT(I,1)*YYSHT(I,1))
1+(YYSHT(I,2)*YYSHT(I,2)))
IF(YSER(I,1).EQ.0.0D0)GO TO 302
YA=DATAN2(YSER(I,2),YSER(I,1))
GO TO 306
302 IF(YSER(I,2)) 303,304,305
303 YA=-1.570796326794897
GO TO 306
304 YA=0.0D0
GO TO 306
305 YA=1.570796326794897
306 IF(YYSHT(I,1).EQ.0.0D0)GO TO 308
YSHTA=DATAN2(YYSHT(I,2),YYSHT(I,1))
GO TO 314
308 IF(YYSHT(I,2)) 309,311,312
309 YSHTA=-1.570796326794897
GO TO 314
311 YSHTA=0.0D0
GO TO 314
312 YSHTA=1.570796326794897
314 CONTINUE

JJ=0
310 PLH=VHAG(L)*VHAG(L)*YH*DCOS(YA)
1-VHAG(L)*VHAG(H)*YH*DCOS(VANG(L)-VANG(H)-YA)
2+VHAG(L)*VHAG(L)*YSHTH*DCOS(YSHTA)

QLH=-VHAG(L)*VHAG(L)*YH*DSIN(YA)
1-VHAG(L)*VHAG(H)*YH*DSIN(VANG(L)-VANG(H)-YA)
2-VHAG(L)*VHAG(L)*YSHTH*DSIN(YSHTA)
WRITE(M5,1200)I,L,H,PLH,QLH
1200 FORMAT(1X,I3,4X,I3,3X,I3,F12.4,6X,F12.4)
IF(JJ.EQ.1)GO TO 300
JJ=1
L=EB(I)
M=SB(I)
GO TO 310
300 CONTINUE
LPSOL=0
RETURN
END

```

```

SUBROUTINE ANULT(Z,X,Y,H)
DOUBLE PRECISION Z(50,50),X(50,50),Y(50,50)

```

```

DO 1 I=1,H
DO 1 J=1,H
Z(I,J)=0.0D0
DO 1 K=1,H
Z(I,J)=Z(I,J)+X(I,K)*Y(K,J)
1 CONTINUE
RETURN
END

```

```

SUBROUTINE CHUL(X,Y,A,B,C,D)

```

```

DOUBLE PRECISION X,Y,A,B,C,D
I=A*C-B*D
Y=A*D+B*C
RETURN
END
SUBROUTINE CDIV(X,Y,A,B,C,D)
DOUBLE PRECISION X,Y,A,B,C,D
I=C*C+D*D
Y=(B*C-A*D)/X
I=(A*C+B*D)/X
RETURN
END

```

```

SUBROUTINE CINVT(A,B,C,D)
A=C/(C*C+D*D)
B=-D/(C*C+D*D)
RETURN
END

```

```

FUNCTION CABS(A,B)
DOUBLE PRECISION CABS,A,B,DSQRT
CABS=DSQRT(A*A+B*B)
RETURN
END

```

```

SUBROUTINE DPINVT(A,B,C,D)
DOUBLE PRECISION A,B,C,D
A=C/(C*C+D*D)
B=-D/(C*C+D*D)
RETURN
END

```

```

SUBROUTINE MINV (A,N)
C THIS SUBPROGRAM IS FOR MATRIX INVERSION AND SIMUL
C LINEAR EQUATIONS
C A=THE GIVEN COEFFICIENT MATRIX A;A**--1 WILL BE
C STORED IN THIS MATRIX AT RETURN TO THE MAIN PROGRAM
C
C N=ORDER OF A;N.GE.1
C DIMENSION IPVOT(50),INDEX(50,2)
C DOUBLE PRECISION A(50,50),B(50,50),PIVOT(50),T
C EQUIVALENCE (IBOW,JROW),(ICOL,JCOL)
C
C FOLLOWING 3 STATEMENTS FOR INITIALIZATION
C N=0
C DET=1.0
57 DO 17 J=1,N
C IPVOT(J)=0
C
C DO 135 I=1,N
C
C FOLLOWING 12 STATEMENTS FOR SEARCH FOR
C PIVOT ELEMENT
C

```

```

T=0.000
DO 9 J=1,N
IF (IPVOT(J).EQ.1) GO TO 9
13 DO 23 K=1,N
IF (IPVOT(K)-1) 43,23,81
43 IF (DABS(T).GE.DABS(A(J,K))) GO TO 23
83 IROW=J
ICOL=K
T=A(J,K)
23 CONTINUE
9 CONTINUE
C
IPVOT(ICOL)=IPVOT(ICOL)+1
C
C FOLLOWING 15 STATEMENTS TO PUT PIVOT
C ELEMENT ON DIAGONAL
C
IF (IROW.EQ.ICOL) GO TO 109
73 DET = -DET
DO 12 L=1,N
T=A(IROW,L)
12 A(IROW,L) = A(ICOL,L)
A(ICOL,L) = T
IF (M.LE.0) GO TO 109
33 DO 2 L=1,M
T=B(IROW,L)
B(IROW,L)=B(ICOL,L)
2 B(ICOL,L)=T
109 INDEX(I,1)=IROW
INDEX(I,2)=ICOL
PIVOT(I)=A(ICOL,ICOL)
DET=DET*PIVOT(I)
C
C FOLLOWING 6 STATEMENTS TO DIVIDE PIVCT ROW
C BY PIVOT ELEMENT
C
A(ICOL,ICOL)=1.000
DO 205 L=1,N
205 A(ICOL,L)=A(ICOL,L)/PIVOT(I)
IF (M.LE.0) GO TO 347
66 DO 52 L=1,M
52 B(ICOL,L)=B(ICOL,L)/PIVOT(I)
C
C FOLLOWING 10 STATEMENTS TO REDUCE NON-PIVOT ROWS
C
C
347 DO 135 LI=1,N
IF (LI.EQ.ICOL) GO TO 135
21 T=A(LI,ICOL)
A(LI,ICOL)=0.000
DO 89 L=1,N
89 A(LI,L)=A(LI,L)-A(ICOL,L)*T
IF (M.LE.0) GO TO 135
18 DO 68 L=1,M
68 B(LI,L)=B(LI,L)-B(ICOL,L)*T
135 CONTINUE
C
C FOLLOWING 11 STATEMENTS TO INTERCHANGE COLUMNS
C
222 DO 3 I=1,M
L=N-I+1

```

```
19      IF (INDEX(L,1).EQ.INDEX(L,2)) GO TO 3
        JROW = INDEX(L,1)
        JCOL = INDEX(L,2)
        DO 549 K=1,N
          T = A(K,JROW)
          A(K,JROW)=A(K,JCOL)
          A(K,JCOL)=T
549      CONTINUE
3        CONTINUE
81      RETURN
        END
```

Computer Code EDSP15

```

C ECONOMIC DISPATCH EXECUTIVE PROGRAM
C THIS PROGRAM PROVIDES LOAD FLOW SOLUTIONS AND ECONOMIC
C DISPATCH FOR POWER SYSTEMS WITH A MAXIMUM OF 15
C BUSES AND 30 TRANSMISSION LINES. IT SOLVES FOR SYSTEM
C LOAD, LOSSES, GENERATOR INCREMENTAL COSTS, REAL POWER
C GENERATION, TRANSMISSION LINE REAL & REACTIVE POWER FLOWS.

REAL LNGTH,LAMBDA,IC
INTEGER ABORT,ANS,BDAT,BTYPE,BUSH,CF,CC,CG,CBC,CHB,CHG,CHL,
ICL,CHY,CHZ,EB,GDAT,QDAT,MBUS,BGSOL,LFSC1,SB,ILDAT,IBDAT,TGDAT
DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,EJ2,EJ3,BJ4,
ICALP,CALQ,DQ,DVANG,EVHAG,G,H,ITL,P,Q,VANG,VHAG,
2XX,YANG,YHAG,YY,YYSH,ZANG,ZHAG,YSER
COMMON / AJ1(15,15), AJ2(15,15), AJ3(15,15),
1AJ4(15,15), ALPHA(15), BDAT, FETA(15),
1BGSOL, BJ1(15,15), BJ2(15,15), BJ3(15,15),
1BJ4(15,15), BTYPE(15), BUSH, CALP(15),
1CALQ(15), CB,CC, CG, CHB,
1CHG, CHL, CL, CHY,
1CHZ, DQ(15), DVANG(15), EVHAG(15),
1EB(30), ESP1, ESP2, G(15),
1GANJA(15), GDAT, H(15), IC(15),
1II, ITER, ITL(15), KINV,
1KSOL, LAMBDA, LDAT, LITER,
1LNGTH(30), LNO, LOSS, LPSOL,
1LSET, MBUS, N5, MSVGB,
1P(15), PD(15), PG(15), PGHAI(15),
1PGHIN(15), Q(15), QD(15),QDAT, QG(15),
1QGMAX(15), QGMIN(15), SB(30), YYSH(30,2),
1TOL,TLDAT, TPD,TBDAT, TPL,TGDAT, YANG(15),
1VHAG(15), VSPEC(15), YX(15,15), YANG(15,15),
1YHAG(15,15), YSHT(30,2), YY(15,15), ZANG(15,15),
1ZHAG(15,15), ZSER(30,2), YSER(30,2), ABORT,IBT(15)
DATA
1ABORT/0/, HDAT/0/, BUSH/0/, CB/'N'/.
1CG/'N'/, CHB/'N'/, CBC/'N'/.
1CHG/'N'/, CHL/'N'/, CL/'N'/.
1CHY/'N'/, CHZ/'N'/, ESP1/0.001/.
1ESP2/0.001/, GDAT/0/, ITER/50/, KINV/0/.
1KSOL/0/, LDAT/0/, LITER/5/, LOSS/'N'/.
1TOL/0.0001/, QDAT/0/

CALL ERRSET(0)
10 TYPE 1000
1000 FORMAT(15X'*****ECONOMIC DISPATCH EXECUTIVE PROGRAM*****')

C SYSTEM INITIALIZATION
20 TYPE 1010
1010 FORMAT(/1X,'>>>ENTER TYPE PROBLEM'/8X,'0=LOAD FLOW PROBLEM'/
18X,'1=ECONOMIC DISPATCH PROBLEM')
22 ACCEPT 2000,KINV
2000 FORMAT(I1)
IF((KINV.EQ.0).OR.(KINV.EQ.1)) GO TO 24
TYPE 1012
1012 FORMAT(1X,'WRONG ENTRY, MUST BE 0 OR 1, TRY AGAIN')
GO TO 22
24 IF(KINV)30,30,26
26 TYPE 1014
1014 FORMAT(/1X,'>>>IS SYSTEM LOSSLESS?')
28 ACCEPT 2001,LOSS
2001 FORMAT(1A1)

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```

IF((LOSS.EQ.'N').OR.(LOSS.EQ.'Y'))GO TO 30
TYPE 1013
1013  FORMAT(1X,'WRONG ENTRY, MUST BE "Y" OR "N", TRY AGAIN.')
GO TO 28
TYPE 1018
1018  FORMAT(/1X,'>>ENTER LOAD FLOW SOLUTION METHOD'/8X,
1'0=NEWTON-RAPHSON'/8X,'1=ACCELERATED GAUSS-SEIDEL'/8X,
1'2=PATTERN SEARCH')
32    ACCEPT 2000,KSOL
IF((KSOL.GE.0).AND.(KSOL.LE.2))GO TO 34
TYPE 1017
1017  FORMAT(1X,'WRONG ENTRY,MUST BE 0,1, OR 2,TRY AGAIN.')
GO TO 32
34    IP(KSOL.EQ.2)KSOL=0
IF((KSOL.EQ.1).AND.(LITER.LT.30))LITER=30
IF((LDAT.EQ.1).AND.(BDAT.EQ.1).AND.(GDAT.EQ.1))
1GO TO 70
TYPE 1020
1020  FORMAT(/1X,'>>ENTER TOTAL NUMBER OF (LINES, & BUSES).')
36    ACCEPT 2004,LNO,HBUS
2004  FORMAT(2I)
IF(((LNO.GE.1).AND.(LNO.LE.30)).AND.((HBUS.GE.1)
1.AND.(HBUS.LE.15)))GO TO 40
TYPE 1016
1016  FORMAT(1X,'WRONG ENTRY,TOTAL LINES=1 TO 30 & TOTAL BUSES=1 TO 15,
1TRY AGAIN.')
GO TO 36

C CHECK METHOD OF DATA INPUT (SOS FILE/CRT/TTY)
40    TYPE 1030
1030  FORMAT(/1X,'>>WANT TO TYPE IN NEW (LINE DATA, BUS DATA, OR
1 GENERATOR DATA) ?')
50    ACCEPT 2008,ILDAT,TBDAT,TGDAT
IF(((TLDAT.EQ.'N').OR.(TLDAT.EQ.'Y')).AND.((TBDAT.EQ.'N')
1.OR.(TBDAT.EQ.'Y')).AND.((TGDAT.EQ.'N').OR.(TGDAT.EQ.'Y')))
2GO TO 60
TYPE 1015
1015  FORMAT(1X,'WRONG ENTRY, MUST BE "N" OR "Y" FOR
1EACH DATA GROUP, /1X, 'i.e. "N" means type in bus
1data only, please use CAP N & Y, /1X, 'try again.')
2008  FORMAT(3A1)
GO TO 50

C READ SYSTEM DATA FROM SOS FILE,TTY,OR CRT
60    IF(LDAT.EQ.0)CALL LDATA
IF(ABORT.EQ.1)GO TO 320
80    IF(BDAT.EQ.0)CALL BDATA
IF(ABORT.EQ.1)GO TO 320
90    IF(GDAT.EQ.0)CALL GDATA
IF(ABORT.EQ.1)GO TO 320

C CHECK FOR PRINTOUT OF SYSTEM DATA
70    TYPE 1050
1050  FORMAT(/1X,'>>WANT A COPY OF (LDATA,BDATA,GDATA,
1OR SYSTEM CONVERGENCE CRITERIA) ?')
100  READ(5,2020)CL,CB,CG,CC
2020  FORMAT(4A1)
IF(((CL.EQ.'N').OR.(CL.EQ.'Y')).AND.
1((CB.EQ.'N').OR.(CB.EQ.'Y')).AND.
2((CG.EQ.'N').OR.(CG.EQ.'Y')).AND.

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```

3((CC.EQ.'N').OR.(CC.EQ.'Y'))GO TO 110
TYPE 1019
1019 FORMAT(1X,'WRONG ENTRY, MUST BE "N" OR "Y" FOR
1EACH DATA GROUP.'/1X,'I.E."NMYN" MEANS TYPE OUT
2EUS DATA AND CONVERGENCE CRITERIA ONLY.'/1X, 'TRY AGAIN.')
GO TO 100
110 IF(CL.EQ.'Y')CALL LDATA
120 IF(CB.EQ.'Y')CALL BDATA
130 IF(CG.EQ.'Y')CALL GDATA

C PRINT SYSTEM CONVERGENCE CRITERIA
140 IF(CC.EQ.'N')GO TO 145
142 WRITE(5,1065)LITER,TOL,ITER,ESP1,ESP2
1065 FORMAT(/1X,'**SYSTEM CONVERGENCE CRITERIA**'/10X,
1'LOAD FLOW ITERATIONS=',I3/
110X,'LOAD FLOW TOLERANCE=',E13.5/
210X,'ECON DISP ITERATIONS=',I3/10X,'ESP1=',E13.5/10X,'ESP2=',
3E13.5)

C CHECK FOR CHANGES TO CONVERGENCE CRITERIA OR SYSTEM DATA
145 TYPE 1070
1070 FORMAT(/1X,'>>WANT TO CHANGE
1(LDATA,BDATA,GDATA, OR CONVERGENCE CRITERIA)?')
150 ACCEPT 2040,CCL,CHB,CHG,CHC
2040 FORMAT(4A1)
IF(((CHC.EQ.'N').OR.(CHC.EQ.'Y')).AND.
1((CHL.EQ.'N').OR.(CHL.EQ.'Y')).AND.
1((CHB.EQ.'N').OR.(CHB.EQ.'Y')).AND.
1((CHG.EQ.'N').OR.(CHG.EQ.'Y'))).GO TO 160
TYPE 1021
1021 FORMAT(1X,'WRONG ENTRY, MUST BE "N" OR "Y" FOR EACH DATA
1GROUP, TRY AGAIN.')
GO TO 150
160 IF(CHL.EQ.'Y')CALL LDATA
IF(CHB.EQ.'Y')CALL BDATA
IF(CHG.EQ.'Y')CALL GDATA
IF(CHC.EQ.'N')GO TO 190
TYPE 1090
1090 FORMAT(/1X,'**CONVERGENCE CRITERIA CHANGES**'/
11X,'>>ENTER(VARIABLE #,NEW VALUE THEN "CR")'/
110X,'1-LOAD FLOW ITERATIONS'/10X,'2-LOAD FLOW TOLERANCE'/
210X,'3-ECON DISP ITERATIONS'/10X,'4-ESP1'/10X,'5-ESP2'/
310X,'>>ENTER 0 THEN "CR" WHEN CHANGES CCOMPLETED.')
170 READ(5,2050)NAME,X
2050 FORMAT(I,F)
IF((NAME.GE.0).AND.(NAME.LE.5))GO TO 180
TYPE 1100
1100 FORMAT(1X,'WRONG ENTRY,VARIABLE MUST BE 1-5, TRY AGAIN.')
GO TO 170
180 IF(NAME.EQ.0)GO TO 190
GO TO(181,182,183,184,185)NAME
181 LITER=IPIX(I)
TYPE 1110,LITER
1110 FORMAT(8X,'LOAD FLOW ITERATIONS=',I3)
GO TO 170
182 TOL=X
TYPE 1120,TOL
1120 FORMAT(8X,'LOAD FLOW TOLERANCE=',E13.5)
GO TO 170
183 ITER=IPIX(I)
TYPE 1130,ITER

```

```

1130  FORMAT(8X,'OPT DISP ITERATIONS=',I3)
      GO TO 170
184   ESP1=X
      TYPE 1140,ESP1
1140  FORMAT(8X,'ESP1=',E13.5)
      GO TO 170
185   ESP2=X
      TYPE 1150,ESP2
1150  FORMAT(8X,'ESP2=',E13.5)
      GO TO 170
190   IF ((BUSN.EQ.0).OR.((BUSN.NE.2).AND.(KINV.EQ.1))) CALL YBUSM
222   TYPE 1152
1152  FORMAT(/1X,'>>WANT A COPY OF (YBUS MATRIX, ZBUS MATRIX)?')
223   ACCEPT 2060,CHY,CHZ
223   IF (KINV.EQ.0) CHZ='N'
2060  FORMAT(2A1)
      IF (((CHY.EQ.'N').OR.(CHY.EQ.'Y')).AND.((CHZ.EQ.'N').OR.
1(CHZ.EQ.'Y')))) GO TO 224
      TYPE 1021
      GO TO 223
224   IF ((CHY.EQ.'Y').OR.(CHZ.EQ.'Y')) CALL YBUSM
225   CONTINUE

C SYSTEM INITIALIZED STARTING LOAD FLOW CALCULATIONS
      LSET=0
230   IF (KSOL) 240,240,250

C CALCULATING LOAD FLOW BY NEWTON-RAPHSON
240   CALL NRLF
      GO TO 260

C CALCULATING LOAD FLOW BY GAUSS-SEIDEL
250   CALL GSLF
260   IF (ABORT.EQ.1) GO TO 320
      IF (KINV.EQ.0) GO TO 320

C CALCULATING OPT DISP POWER BALANCE EQUATIONS
      CALL OPT
      GO TO 330

320   ABORT=0
330   TYPE 1210
1210  FORMAT(/1X,'>>TYPE CODE # FOR DESIRED ACTION'/
18X,'1=PRINT BUS & GEN SOLUTIONS ONLY.'/8X,'2=PRINT LINE
2POWERS, BUS & GEN SOLUTIONS'/8X,'3=CREATE SOS FILE OF
2 SOLUTIONS'/8X,'4=CHANGE DATA OR TOLERANCES AND RERUN'/
18X,'5=CHANGE TYPE PROBLEM OR SOLUTION METHOD.'/13X,'RERUN WITH
1EXISTING DATA'/8X,'6=NEW PROBLEM'/8X,'7=TERMINATE')

340   ACCEPT 2000,ANS
      IF ((ANS.GE.1).AND.(ANS.LE.7)) GO TO 350
      TYPE 1220
1220  FORMAT(1X,'WRONG ENTRY, MUST BE 1 TO 7, TRY AGAIN.')
      GO TO 340
350   GO TO (361,362,380,363,365,367,500) ANS
361   N5=5
      BGSOL=1
      LPSOL=0
      CALL SOL
      GO TO 330
362   N5=5
      BGSOL=1

```



```

LPSOL=1
CALL SOL
GO TO 330
363  BDAT=0
      TBDAT='N'
      CALL BDATA
      GO TO 145
365  LSET=0
      BDAT=0
      TBDAT='N'
      CALL BDATA
      GO TO 10
367  LDAT=0
      BDAT=0
      GDAT=0
      QDAT=0
      LSET=0
      GO TO 10

```

C CREATING SOS FILES OF LINE, BUS, GENERATOR DATA,
C YBUS & ZBUS MATRIX, BUS & GENERATOR SOLUTIONS, AND
C LINE POWER FLOW, AND COMMAND FILE FOR TRANSFER OF DATA
C TO TAPE.

```

380  OPEN(UNIT=1,DEVICE='DSK',ACCESS='SEQOUT',
      1DISPOSE='SAVE',FILE='SOL.DAT')
      N5=1
      BGSOL=1
      LPSOL=1
      CALL SOL
      CLOSE(UNIT=1)
      N5=5

445  OPEN(UNIT=24,DEVICE='DSK',ACCESS='SEQOUT',
      1DISPOSE='SAVE',FILE='YBUSH.DAT')
      WRITE(24,3030)
3030  FORMAT(15X,'**YBUS MATRIX**')
      DO 450 I=1,NBUS
      WRITE(24,3040) I
3040  FORMAT(1X,'ROW',I3)
450  WRITE(24,3050) (YHAG(I,J),YANG(I,J),J=1,NBUS)
3050  FORMAT(6E12.5)

      IF(KINV.EQ.0) GO TO 465
      WRITE(24,3060)
3060  FORMAT(15X,'**ZBUS MATRIX**')
      DO 460 I=1,NBUS
      WRITE(24,3040) I
460  WRITE(24,3070) (ZHAG(I,J),ZANG(I,J),J=1,NBUS)
3070  FORMAT(6E12.5)
465  CLOSE(UNIT=24)
      GO TO 330
500  CONTINUE
      STOP
      END

```

SUBROUTINE LDATA
C SUBROUTINE TO READ, WRITE, AND CHANGE LINE DATA

```

REAL LENGH
INTEGER ABORT,BUSH,CL,CHL,EB,SB,TLDAT
DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,EJ3,BJ4,
1CALP,CALQ,DC,DVANG,DVHAG,G,H,ITL,P,Q,VANG,VHAG,
2XX,YANG,YMAG,YY,YYSHT,ZANG,ZHAG,YSER
COMMON / AJ1(15,15), AJ2(15,15), AJ3(15,15),
1AJ4(15,15), ALPHA(15), BDAT, BETA(15),
1BGSOL, BJ1(15,15), BJ2(15,15), BJ3(15,15),
1BJ4(15,15), BTYPE(15), BUSH, CALP(15),
1CALQ(15), CB,CC, CG, CHB,
1CHG, CHL, CL, CHY,
1CHZ, DQ(15), DVANG(15), DVHAG(15),
1EB(30), ESP1, ESP2, G(15),
1GAMMA(15), GDAT, H(15), IC(15),
1II, ITER, ITL(15), KINV,
1KSOL, LAMBDA, LDAT, LITER,
1LNGTH(30), LNO, LOSS, LPSOL,
1LSET, MBUS, N5, NSWGB,
1P(15), PD(15), PG(15), PGMAX(15),
1PGHIN(15), Q(15), QD(15), QDAT, QG(15),
1QGHAX(15), QGHIN(15), SB(30), YSHT(30,2),
1TOL,TLDAT, TPD,TBDAT, TPL,TGDAT, YANG(15),
1VHAG(15), VSPEC(15), IX(15,15), YANG(15,15),
1YHAG(15,15), YSHT(30,2), YY(15,15), ZANG(15,15),
1ZHAG(15,15), ZSER(30,2), YSER(30,2), ABORT

```

```

ILD=0
IF(LDAT.EQ.1)GO TO 50
IF(TLDAT.EQ.'Y')GO TO 20

```

```

C READ LINE DATA FOR SOS FILE FOR20.DAT
OPEN(UNIT=20,DEVICE='DSK',ACCESS='SEQIN',DISPOSE='SAVE',
1FILE='FOR20.DAT')
20 DO 5 I=1,LNO
5 READ(20,*)K,SB(I),EB(I),LNGTH(I),YSHT(I,1),YSHT(I,2),
1ZSER(I,1),ZSER(I,2)
CLOSE(UNIT=20)
2000 FORMAT(3I,5F)
IF(K.EQ.LNO)GO TO 40
TYPE 8
8 FORMAT(1X,'TOTAL NUMBER OF LINES ENTERED DOES NOT EQUAL
1NUMBER OF DATA LINES IN FOR20.DAT')
AEORT=1
LDAT=0
RETURN

```

```

C READ LINE DATA FROM CRT/TTY
20 OPEN(UNIT=20,DEVICE='DSK',ACCESS='SEQOUT',DISPOSE='SAVE',
1FILE='FOR20.DAT')
IF(ILD.EQ.1)GO TO 21
TYPE 1000
1000 FORMAT(/1X,'**SYSTEM LINE DATA**'/1X,'>>ENTER (LINE #,
1SB #,EB #, LINE LENGTH, YSHUNT G,YSHUNT B,
2ZSERIES R,ZSERIES X)')
21 DC 30 I=1,LNO
IF(ILD.EQ.1)GO TO 25
22 ACCEPT 2002,K,SB(I),EB(I),LNGTH(I),YSHT(I,1),YSHT(I,2),
1ZSER(I,1),ZSER(I,2)
2002 FORMAT(3I,5F)

```

```

IF (K.EQ.1) GO TO 25
TYPE 1002,I
1002  FORMAT(1X,'WRONG ENTRY, LINE # SHOULD=',I3,', TRY AGAIN')
      GC TO 22
25    WRITE(20,1004) I,SB(I),EB(I),LNTH(I),YSHT(I,1),YSHT(I,2),
      1ZSER(I,1),ZSER(I,2)
1004  FORMAT(3I3,5E12.5)
30    CONTINUE
      CLOSE(UNIT=20)
      IF (ILD.EQ.1) GO TO 180
40    BUSH=0
      LDAT=1

C CHECK FOR LINE DATA PRINT OUT
50    IF (CL.EQ.'N') GO TO 70
      TYPE 1010
1010  FORMAT(/1X,'**SYSTEM LINE DATA**'/1X,'LINE #',I3,
      1'SB',I3,'EB',I3,'LENGTH',I3,'Y SHUNT',I3,'Z SERIES')
      DO 60 I=1,LNO
60    TYPE 1020,I,SB(I),EB(I),LNTH(I),YSHT(I,1),YSHT(I,2),
      1ZSER(I,1),ZSER(I,2)
1020  FORMAT(1X,I3,2X,2I3,1X,E12.5,2(1X,2E12.5))
      CL='N'

IF (ILD.EQ.1) GO TO 80
C CHECK FOR LINE DATA CHANGES
70    IF (CHL.EQ.'N') GO TO 180
      TYPE 1030
1030  FORMAT(/1X,'** LINE DATA CHANGES**'/
      11X,'>>ENTER (VARIABLE #, LINE #, NEW VALUE THEN "CE")'/
      110X,'1=STARTING BUS #'/10X,'2=ENDING BUS #'/10X,'3=LINE
      1LENGTH'/10X,'4=Y SHUNT G'/10X,'5=Y SHUNT B'/10X,'6=Z SERIES R'/
      210X,'7=Z SERIES X'/10X,'8=RETYPE COPY OF ALL LINE DATA'/10X,'
      19=CHANGE TOTAL NUMBER OF LINES'/10X,'>>ENTER 0 THEN
      1"CR" WHEN CHANGES COMPLETED')
80    READ(5,2010) NAME,I,X
2010  FORMAT(2I,F)
      IF (NAME.EQ.0) GO TO 175
      IF (NAME.EQ.8) GO TO 172
      IF (NAME.EQ.9) GO TO 173
      IF (((NAME.GE.1).AND.(NAME.LE.7)).AND.((I.GE.0).AND.(I.LE.LNO)))
      1GO TO 100
      TYPE 1040,LNO
1040  FORMAT(1X,'WRONG ENTRY, VARIABLE # MUST BE 1-7,/'
      11X,'LINE # MUST BE 1 TO',I3,', TRY AGAIN')
      GC TO 80
100    BUSH=0
      GO TO(110,120,130,140,150,160,170) NAME
110    SB(I)=IPIX(I)
      TYPE 1060,I,SB(I)
1060  FORMAT(1X,'SB(LINE #',I3,')=',I3)
      GO TO 80
120    EB(I)=IPIX(I)
      TYPE 1070,I,EB(I)
1070  FORMAT(1X,'EB(LINE #',I3,')=',I3)
      GO TO 80
130    LNTH(I)=I
      TYPE 1080,I,LNTH(I)
1080  FORMAT(1X,'LENGTH(LINE #',I3,')=',E12.5)
      GO TO 80
140    YSHT(I,1)=I

```

```

1090 TYPE 1090,I,YSHT(I,1)
      FORMAT(IX,'YSHT G (LINE #',I3,')-',F12.5)
      GO TO 80
150   YSHT(I,2)=X
      TYPE 1100,I,YSHT(I,2)
1100 FORMAT(IX,'YSHT B (LINE #',I3,')-',F12.5)
      GO TO 80
160   ZSER(I,1)=X
      TYPE 1110,I,ZSER(I,1)
1110 FORMAT(IX,'ZSER R (LINE #',I3,')-',F12.5)
      GO TO 80
170   ZSER(I,2)=X
      TYPE 1120,I,ZSER(I,2)
1120 FORMAT(IX,'ZSER X (LINE #',I3,')-',F12.5)
      GO TO 80
172   ILD=1
      CL='Y'
      GO TO 50
173   LNO=X
      BUSH=0
      TYPE 1130,I
1130 FORMAT(IX,'TOTAL NUMBER OF LINES =',I3)
      GO TO 80
175   CHL='X'
      ILD=1
      GO TO 20
180   ILD=0
      RETURN
      END

```

```

SUBROUTINE BDATA
C SUBROUTINE TO READ,WRITE,AND CHANGE BUS DATA
  INTEGER ABORT,BDAT,BTYPE,CB,CHE,MBUS,TBDAT
  DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,EJ2,EJ3,EJ4,
  1CALP,CALQ,DQ,DVANG,DVHAG,G,H,ITL,P,Q,VANG,VHAG,
  2XX,YANG,YHAG,YY,YYSH,ZANG,ZHAG,YSER
  COMMON / AJ1(15,15), AJ2(15,15), AJ3(15,15),
  1AJ4(15,15), ALPHA(15), BDAT, BETA(15),
  1BGSOL, BJ1(15,15), BJ2(15,15), BJ3(15,15),
  1BJ4(15,15), BTYPE(15), BUSH, CALP(15),
  1CALQ(15), CB,CC, CG, CHE,
  1CHG, CHL, CL, CHY,
  1CHZ, DQ(15), DVANG(15), DVHAG(15),
  1EB(30), ESP1, ESP2, G(15),
  1GAMMA(15), GDAT, H(15), IC(15),
  1II, ITER, ITL(15), KINV,
  1KSOL, LAMBDA, LDAT, LITER,
  1LENGTH(30), LNO, LOSS, LPSOL,
  1LSET, MBUS, M5, MSWGB,
  1P(15), PD(15), PG(15), PGMAX(15),
  1PGMIN(15), Q(15), QD(15),QDAT, QG(15),
  1QGHAY(15), QGMIN(15), SB(30), YSHT(30,2),
  1TOL, TLDAT, TPD, TBDAT, TPL, TGDAT, YANG(15),
  1VHAG(15), VSPEC(15), XX(15,15), YANG(15,15),
  1YHAG(15,15), YSHT(30,2), YY(15,15), ZANG(15,15),
  1ZHAG(15,15), ZSER(30,2), YSER(30,2), ABORT

  IBD=0
  IP(BDAT.EQ.1)GO TO 50

```

```

IF (TBDAT.EQ.'Y') GO TO 20
C READ BUS DATA FROM SOS FILE FOR21.DAT
OPEN(UNIT=21,DEVICE='DSK',ACCESS='SEQIN',DISPOSE='SAVE',
1 FILE='FOR21.DAT')
10 DO 15 I=1,MBUS
15 READ(21,*)K,BTYPE(I),PG(I),QG(I),PD(I),QD(I),VSPEC(I)
2000 FORMAT(2I,5F)
CLOSE(UNIT=21)
IF(K.EQ.MBUS)GO TO 45
TYPE 500
500 FORMAT(1X,'TOTAL NUMBER OF BUSES ENTERED DOES NOT
EQUAL NUMBER OF DATA LINES IN FOR21.DAT')
BDAT=0
ABORT=1
RETURN

C READ BUS DATA FROM CRT/TTY
19 OPEN(UNIT=21,DEVICE='DSK',ACCESS='SEQOUT',DISPOSE='SAVE',
1 FILE='FOR21.DAT')
IF (IBD.EQ.1)GO TO 21
20 TYPE1000
1000 FORMAT(/1X,'**SYSTEM BUS DATA**'/1X,'>>ENTER (BUS#,
1 BUS TYPE,PG,QG,PD,QD,VSPEC)')
21 DO 30 I=1,MBUS
IF (IBD.EQ.1)GO TO 25
22 ACCEPT 2000,K,BTYPE(I),PG(I),QG(I),PD(I),QD(I),VSPEC(I)
IF(K.EQ.I)GO TO 25
TYPE 1005,I
1005 FORMAT(1X,'WRONG ENTRY, BUS # SHOULD=',I3,', TRY AGAIN.')
GO TO 22
25 WRITE(21,1010)I,BTYPE(I),PG(I),QG(I),PD(I),QD(I),VSPEC(I)
1010 FORMAT(2I3,5F12.5)
30 CONTINUE
CLOSE(UNIT=21)
BDAT=1
45 IF (IBD.EQ.1)GO TO 170

C CHECK FOR PRINTOUT OF BUS DATA
50 IF (CB.EQ.'N')GO TO 70
TYPE 1020
1020 FORMAT(/1X,'**SYSTEM BUS DATA**'/2X,'BUS',3X,'TYPE',
15X,'PG',8X,'QG',8X,'PD',8X,'QD',7X,'VSPEC')
DO 60 I=1,MBUS
TYPE 1030,I,BTYPE(I),PG(I),QG(I),PD(I),QD(I),VSPEC(I)
1030 FORMAT(1X,I3,4X,I3,5F10.5)
60 CONTINUE
CB='N'
IF (IBD.EQ.1)GO TO 80

C CHECK FOR BUS DATA CHANGES
70 IF (CB.EQ.'N')GO TO 170
TYPE 1040
1040 FORMAT(/1X,'**BUS DATA CHANGES**'/
11X,'>>ENTER (VARIABLE #, BUS #, NEW VALUE THEN "CR"/
110X,'1=BUS TYPE'/10X,'2=PG'/10X,'3=QG'/10X,'4=PD'
1/10X,'5=QD'/10X,'6=VSPEC'/10X,'7=RETYPE COPY OF ALL BUS DATA'
1/10X,'8=CHANGE TOTAL NUMBER OF BUSES'/10X,

```

```

1'>>ENTER 0 THEN "CH" WHEN CHANGES COMPLETED.')
80 READ(5,2010) NAME,I,X
2010 FORMAT(2I,F)
IF (NAME.EQ.0) GO TO 165
IF (NAME.EQ.8) GO TO 163
IF ((NAME.GE.1).AND.(NAME.LE.7)).AND.
1((I.GE.0).AND.(I.LE.MBUS)) GO TO 100
TYPE 1050,MBUS
1050 FORNAT(1X,'WRONG ENTRY, VARIABLE NAME MUST BE 1-7, '/
11X,'BUS # MUST BE 1 TO',I3,', TRY AGAIN.')
GO TO 80
100 GO TO(110,120,130,140,150,160,162) NAME
110 BTYPE(I)=IPIX(X)
TYPE 1060,I,BTYPE(I)
1060 FORNAT(1X,'BUS TYPE(BUS #',I3,')=',I3)
GO TO 80
120 PG(I)=X
TYPE 1070,I,PG(I)
1070 FORNAT(1X,'PG(BUS #',I3,')=',Z12.5)
GO TO 80
130 QG(I)=X
TYPE 1080,I,QG(I)
1080 FORNAT(1X,'QG(BUS #',I3,')=',Z12.5)
GO TO 80
140 PD(I)=X
TYPE 1090,I,PD(I)
1090 FORNAT(1X,'PD(BUS #',I3,')=',Z12.5)
GO TO 80
150 QD(I)=X
TYPE 1100,I,QD(I)
1100 FORNAT(1X,'QD(BUS #',I3,')=',Z12.5)
GO TO 80
160 VSPEC(I)=X
TYPE 1110,I,VSPEC(I)
1110 FORNAT(1X,'VSPEC(BUS #',I3,')=',Z12.5)
GO TO 80
162 CB='Y'
IBD=1
GO TO 50
163 MBUS=I
TYPE 1120,I
1120 FORNAT(1X,'TOTAL NUMBER OF BUSES =',I3)
GO TO 80
165 CHB='N'
IBD=1
GO TO 19
170 IBD=0
RETURN
END

```

SUBROUTINE GDATA
C SUBROUTINE TO READ,WRITE,AND CHANGE GENERATOR DATA

```

INTEGER BTYPE,CG,CHG,GDAT,GNO,MBUS,IGDAT,QDAT
DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,BJ3,BJ4,
1CALP,CALQ,DC,DVANG,DVHAG,G,R,ITL,P,Q,YANG,VHAG,
2XX,YANG,YHAG,YY,YYSHT,ZANG,ZHAG,YSER
COMMON / AJ1(15,15), AJ2(15,15), AJ3(15,15),

```

1AJ4 (15, 15),	ALPHA (15),	BDAT,	BETA (15),
1BGSOL,	BJ1 (15, 15),	BJ2 (15, 15),	BJ3 (15, 15),
1BJ4 (15, 15),	BTYPE (15),	BUS#,	CALP (15),
1CALQ (15),	CB, CC,	CG,	CHB,
1CHG,	CHL,	CL,	CHY,
1CHZ,	DQ (15),	DYANG (15),	DVHAG (15),
1EB (30),	ESP1,	ESP2,	G (15),
1GAMMA (15),	GDAT,	H (15),	IC (15),
1II,	ITER,	ITL (15),	KINV,
1KSOL,	LAMBDA,	LDAT,	LITER,
1LNGTH (30),	LNO,	LOSS,	LPSOL,
1LSET,	MBUS,	MS,	MSWGB,
1P (15),	PD (15),	PG (15),	PGHAX (15),
1PGHIN (15),	Q (15),	QD (15), QDAT,	QG (15),
1QGHAX (15),	QGHIN (15),	SB (30),	YYSHT (30, 2),
1TOL, TLDAT,	TPD, TBDAT,	TPL, TGDAT,	YANG (15),
1VHAG (15),	VSPEC (15),	YX (15, 15),	YANG (15, 15),
1YHAG (15, 15),	YSHT (30, 2),	YY (15, 15),	ZANG (15, 15),
1ZHAG (15, 15),	ZSER (30, 2),	YSER (30, 2),	ABORT

```

IGB=0
IF (GDAT.EQ.1) GO TO 56
IF (KINV.EQ.0) GO TO 25
IF (TGDAT.EQ.'Y') GO TO 20

```

```

C READ GENERATOR DATA FROM SOS FILE POR22.DAT
OPEN (UNIT=22, DEVICE='DSK', ACCESS='SEQIN', DISPOSE='SAVE',
      1 FILE='POR22.DAT')
GNO=0
10 DO 15 I=1, MBDS
   IF ((BTYPE(I)).GE.0) GO TO 15
   READ (22, *) K, ALPHA (I), BETA (I), GAMMA (I)
2000 FORMAT (I, 3F)
   GNO=GNO+1
15 CONTINUE
   CLOSE (UNIT=22)
   GO TO 40

C READ GENERATOR DATA FROM CRT/TTY
20 OPEN (UNIT=22, DEVICE='DSK', ACCESS='SEQOUT', DISPOSE='SAVE',
      1 FILE='POR22.DAT')
   IF (IGB.EQ.1) GO TO 29
   TYPE 1000
1000 FORMAT (/1X, '**GENERATOR DATA**'/1X, '>>ENTER (BUS#, ALPHA,
      1 BETA, GAMMA) ')
29 DO 30 I=1, MBUS
   IF (BTYPE (I) .GE.0) GO TO 30
   IF (IGB.EQ.1) GO TO 33
32 ACCEPT 2002, K, ALPHA (I), BETA (I), GAMMA (I)
2002 FORMAT (I, 3F)
   IF (K.EQ.I) GO TO 31
   TYPE 1010, I
1010 FORMAT (1X, 'WRONG ENTRY, BUS # SHOULD=', I3, ', TRY AGAIN.')
   GO TO 32
31 GNO=GNO+1
33 WRITE (22, 2003) I, ALPHA (I), BETA (I), GAMMA (I)
2003 FORMAT (I3, 3F)
30 CONTINUE
   CLOSE (UNIT=22)
   IF (IGB.EQ.1) GO TO 48
40 GDAT=1

```

```

C-INITIALIZING GENERATOR AND Q CONSTRAINTS
25   IF (QDAT.EQ.1) GO TO 56
     IF (TGDAT.EQ.'N') GO TO 50

C READ CONSTRAINT DATA FROM TTY/CRT
     TYPE 1006
1006  FORMAT(1X,'**GENERATOR CONSTRAINT DATA**'/1X,'>>>ENTER FOR
      1TYPE -1 & -3 BUS (BUS #,PGHAX,PGHIN)'/9X,'PCR TYPE -2 BUS
      1 (BUS #,PGHAX,FGHIN,QGHAX,QGHIN)'/5X,'PCR TYPE +2 BUS
      1 (BUS #,QGHAX,QGHIN)')
     DO 36 I=1,MBUS
35   IF (BTYPE(I).GE.0) GO TO 38
     IF (BTYPE(I).EQ.-2) GO TO 37
     ACCEPT 2005,K,PGHAX(I),PGHIN(I)
2005  FORMAT(I,2F)
     GO TO 39
37   ACCEPT 2020,K,PGHAX(I),PGHIN(I),QGHAX(I),QGHIN(I)
2020  FORMAT(I,4F)
     GO TO 39
38   IF (BTYPE(I).NE.2) GO TO 36
     ACCEPT 2005,K,QGHAX(I),QGHIN(I)
39   IF (K.EQ.I) GO TO 36
     TYPE 1015,I
1015  FORMAT(1X,'WRONG ENTRY,BUS # SHOULD BE=',I3,', TRY AGAIN.')
     GO TO 35
36   CONTINUE

C ENTER CONSTRAINT DATA INTO SOS FILE FOR23.DAT
48   OPEN (UNIT=23,DEVICE='DSK',ACCESS='SEQOUT',DISPOSE='SAVE',
      1FILE='FOR23.DAT')

     DO 52 I=1,MBUS
     IF (BTYPE(I).GE.0) GO TO 53
     IF (BTYPE(I).EQ.-2) GO TO 51
     WRITE(23,2007)I,PGHAX(I),PGHIN(I)
2007  FORMAT(1X,I3,2F11.4)
     GO TO 52
51   WRITE(23,2006)I,PGHAX(I),PGHIN(I),QGHAX(I),QGHIN(I)
2006  FORMAT(1X,I3,4F11.4)
     GO TO 52
53   IF (BTYPE(I).NE.2) GO TO 52
     WRITE(23,2009)I,QGHAX(I),QGHIN(I)
2009  FORMAT(1X,I3,22X,2F11.4)
52   CONTINUE
     CLOSE (UNIT=23)
     IF (IGB.EQ.1) GO TO 180
     GO TO 54

C READ CONSTRAINT DATA FROM SOS FILE FOR23.DAT
50   OPEN (UNIT=23,DEVICE='DSK',ACCESS='SEQIN',DISPOSE='SAVE',
      1FILE='FOR23.DAT')
     DO 46 I=1,MBUS
     IF (BTYPE(I).GE.0) GO TO 42
     IF (BTYPE(I).EQ.-2) GO TO 41
     READ(23,*) K,PGHAX(I),PGHIN(I)
     GO TO 46
41   READ(23,2020) K,PGHAX(I),PGHIN(I),QGHAX(I),QGHIN(I)
     GO TO 46
42   IF (BTYPE(I).NE.2) GO TO 46
     READ(23,2005) K,QGHAX(I),QGHIN(I)

```



```

.46 CONTINUE
CLOSE(UNIT=23)
54 QDAT=1

C CHECK FOR PRINTOUT OF GENERATOR DATA
56 IF(CG.EQ.'N') GO TO 70
IF(KINV.EQ.0) GO TO 61
TYPE 1020,GNO
1020 FORMAT(/1X,'**SYSTEM GENERATOR DATA**'/1X,'NUMBER
10F GENERATORS =',I3/1X,'BUS#',4X,
1'ALPHA',4X,'BETA',6X,'GAMMA')
DO 60 I=1,MBUS
IF((BTYPE(I).GE.0)) GO TO 60
TYPE 1030,I,ALPHA(I),BETA(I),GAMMA(I)
1030 FORMAT(1X,I3,3F10.5)
60 CONTINUE

C PRINT GENERATOR CONSTRAINTS
61 WRITE(5,1032)
1032 FORMAT(/1X,'**GENERATOR CONSTRAINTS**'/1X,'BUS #',
13X,'PGHAX',5X,'PGHIN',7X,'QGHAX',6X,'QGHIN')
DO 65 I=1,MBUS
IF((BTYPE(I)).GE.0) GO TO 64
IF(BTYPE(I).EQ.-2) GO TO 62
WRITE(5,1034)I,PGHAX(I),PGHIN(I)
1034 FORMAT(1X,I3,2F11.4)
GO TO 65
62 WRITE(5,1036)I,PGHAX(I),PGHIN(I),QGHAX(I),QGHIN(I)
1036 FORMAT(1X,I3,4F11.4)
GO TO 65
64 IF(BTYPE(I).NE.2) GO TO 65
WRITE(5,1038)I,QGHAX(I),QGHIN(I)
1038 FORMAT(1X,I3,22X,2F11.4)
65 CONTINUE
66 CG='N'
IF(IGB.EQ.1) GO TO 80

C CHECK FOR GENERATOR DATA CHANGES
70 IF(CHG.EQ.'N') GO TO 180
TYPE 1040
1040 FORMAT(/1X,'**GENERATOR DATA CHANGES**'/
11X,'>>ENTER (VARIABLE #, BUS #, NEW VALUE THEN "CR")'/
110X,'1=ALPHA'/10X,'2=BETA'/10X,'3=GAMMA'/10X,'4=PGHAX'/10X,'
25=PGHIN'/10X,'6=QGHAX'/10X,'7=QGHIN'/10X,'8=BTYPE ALL
1GENERATOR DATA'/10X,'>>ENTER 0 THEN "CR"
3WHEN CHANGES COMPLETED. ')
80 READ(5,2010)NAME,I,X
2010 FORMAT(2I,F)
IF(NAME.EQ.0) GO TO 175
IF(((NAME.GE.1).AND.(NAME.LE.8)).AND.((I.GE.0).AND.
1(I.LE.MBUS)))
2GO TO 90
TYPE 1050,MBUS
1050 FORMAT(1X,'WRONG ENTRY, VARIABLE MUST BE 1-8, '/
11X,'BUS # MUST BE 0 TO',I3,'CHECK BUS TYPE IS'/
11X,'NEGATIVE, AND TRY AGAIN. ')
GO TO 80
90 CONTINUE
100 GO TO(110,120,130,140,150,160,170,172) NAME
110 ALPHA(I)=X
TYPE 1060,I,ALPHA(I)

```

```

1060  FORMAT(1X,'ALPHA(BUS #',I3,')=' ,E12.5)
      GO TO 80
120   BETA(I)=X
      TYPE 1070,I,BETA(I)
1070  FCRHAT(1X,'BETA(BUS #',I3,')=' ,E12.5)
      GO TO 80
130   GAMMA(I)=X
      TYPE 1080,I,GAMMA(I)
1080  FCRHAT(1X,'GAMMA(BUS #',I3,')=' ,E12.5)
      GO TO 80
140   PGHAI(I)=X
      TYPE 1090,I,PGHAI(I)
1090  FCRHAT(1X,'PGHAI(BUS #',I3,')=' ,E12.5)
      GO TO 80
150   PGMHI(I)=X
      TYPE 1100,I,PGMHI(I)
1100  FCRHAT(1X,'PGMHI(BUS #',I3,')=' ,E12.5)
      GO TO 80
160   QGHAI(I)=X
      TYPE 1110,I,QGHAI(I)
1110  FCRHAT(1X,'QGHAI(BUS #',I3,')=' ,E12.5)
      GO TO 80
170   QGMHI(I)=X
      TYPE 1120,I,QGMHI(I)
1120  FCRHAT(1X,'QGMHI(BUS #',I3,')=' ,E12.5)

      GO TO 80
172   CG='Y'
      IGB=1
      GO TO 56

175   CHG='N'
      IGB=1
      IF(KINV.EQ.0)GO TO 48
      GO TO 20

180   IGB=0
      RETURN
      END

```

SUBROUTINE YBUS
C SUBROUTINE TO CALCULATE YBUS AND ZBUS MATRIX

```

REAL LGTH
INTEGER BUSH,CHY,CHZ,EB,EBUS,SB
DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,BJ3,BJ4,
1CALP,CALQ,DQ,DVANG,DVHAG,G,H,ITL,P,Q,VANG,VHAG,
2XI,YANG,YHAG,YY,YYSH,ZANG,ZHAG,YSER,D

COMMON /      AJ1(15,15),  AJ2(15,15),  AJ3(15,15),
1AJ4(15,15),  ALPHA(15),    BDAT,      BETA(15),
1BGSOL,      BJ1(15,15),  BJ2(15,15),  BJ3(15,15),
1BJ4(15,15),  BTYPE(15),  BUSH,      CALP(15),
1CALQ(15),   CB,CC,      CG,        CHB,
1CHG,        CHL,        CL,        CHY,
1CHZ,        DQ(15),     DVANG(15),  DVHAG(15),
1EB(30),     ESP1,      ESP2,      G(15),
1GAMMA(15),  GDAT,      H(15),    IC(15),

```

```

111,          ITER,          ITL(15),          KINV,
1KSOL,        LASBDA,        LDAT,          LITER,
1LNGTH(30),   LNO,          LOSS,         LPSOL,
1LSET,        MBUS,          M5,          M5EGB,
1P(15),       PD(15),        PG(15),        PGMAX(15),
1PGMIN(15),   Q(15),          QD(15),QDAT,   QG(15),
1QGMAX(15),   QGHIN(15),      SB(30),        YYSHT(30,2),
1TOL,TLDAT,   TPD,TBDAT,      TPL,TGDAT,     YANG(15),
1VMAG(15),    VSPEC(15),      XI(15,15),     YANG(15,15),
1VMAG(15,15), YSHT(30,2),     YI(15,15),     ZANG(15,15),
1ZMAG(15,15), ZSEB(30,2),    YSER(30,2),    ABOFT

```

IF ((BUSH.EQ.2).OR.((KINV.EQ.0).AND.(BUSH.EQ.1))) GO TO 90
TYPE 1000

1000 FORMAT(/1X,***GENERATING YBUS MATBIX***)

C CALCULATING LINE SHUNT AND SERIES ADEITTANCE
DO 15 I=1,LNO
YYSHT(I,1)=(DBLE(YSHT(I,1))*DBLE(LNGTH(I)))/2.000
YYSHT(I,2)=(DBLE(YSHT(I,2))*DBLE(LNGTH(I)))/2.000
D=(DBLE(LNGTH(I))*((DBLE(ZSER(I,1))*DBLE(ZSER(I,1)))
1+(DBLE(ZSER(I,2))*DBLE(ZSER(I,2))))
IF(D.EQ.0.000) GO TO 20
YSER(I,1)=DBLE(ZSER(I,1))/D
YSER(I,2)=-DBLE(ZSER(I,2))/D
GO TO 15
20 YSER(I,1)=0.000
15 YSER(I,2)=0.000
 continue

C CALCULATING YBUS MATRIX
DO 30 I=1,MBUS
DO 30 J=1,MBUS
YMAG(I,J)=0.000
YANG(I,J)=0.000
AJ1(I,J)=0.000
AJ2(I,J)=0.000
IF(J.EQ.I) GO TO 60

C OFF DIAGONAL ELEMENTS(I.NE.J)
DO 40 L=1,LNO
IF(((SB(L).EQ.I).AND.(EB(L).EQ.J)).OR.((SB(L).EQ.J)
1.AND.(EB(L).EQ.I))) GO TO 42
GO TO 40
42 YMAG(I,J)=DSQRT((YSER(L,1)*YSER(L,1))+(YSER(L,2)*YSER(L,2)))
IF(YSER(L,1).EQ.(0.000)) GO TO 22
YANG(I,J)=DATAN2(-YSER(L,2),-YSER(L,1))
GO TO 29
22 IF(YSER(L,2)) 24,26,28
24 YANG(I,J)=1.570796326794897
GO TO 29
26 YANG(I,J)=0.000
GO TO 29
28 YANG(I,J)=-1.570796326794897
29 IF(KINV.EQ.0) GO TO 40
AJ1(I,J)=-YSER(L,1)
AJ2(I,J)=-YSER(L,2)
40 CONTINUE
GO TO 30

```

C ON DIAGONAL ELEMENTS(I-EQ-J)
60   DO 45 L=1,LNO
      IF ((SB(L).EQ.I).OR.(EB(L).EQ.I)) GO TO 46
      GO TO 45
46   AJ1(I,J)=AJ1(I,J)+YYSHT(L,1)+YSER(L,1)
      AJ2(I,J)=AJ2(I,J)+YYSHT(L,2)+YSER(L,2)
45   CONTINUE
      YEAG(I,J)=DSQRT(AJ1(I,J)*AJ1(I,J)+AJ2(I,J)*AJ2(I,J))
      IF (AJ1(I,J).EQ.(0.0D0)) GO TO 31
      YANG(I,J)=DATAN2(AJ2(I,J),AJ1(I,J))
      GO TO 30
31   IF (AJ2(I,J)) 32,33,34
32   YANG(I,J)=-1.570796326794897
      GO TO 30
33   YANG(I,J)=0.0D0
      GO TO 30
34   YANG(I,J)=+1.570796326794897
30   CONTINUE
35   BUSH=1
      IF (KINV.EQ.0) GO TO 90

C CALCULATING ZBUS MATRIX
      TYPE 1005
1005  FORMAT(15X,'**CALCULATING ZBUS MATRIX**')
      DO 50 I=1,NBUS
      DO 50 J=1,NBUS
      BJ1(I,J)=AJ1(I,J)
50     BJ2(I,J)=AJ2(I,J)
      BJ3(I,J)=0.0D0
      BJ4(I,J)=0.0D0
      CALL CTRI(BJ1,BJ2,BJ3,BJ4,NBUS)
      CALL CTRIY(BJ3,BJ4,BJ1,BJ2,NBUS)
      DO 80 I=1,NBUS
      DO 80 J=1,NBUS
      ZHAG(I,J)=DSQRT(BJ1(I,J)*BJ1(I,J)+BJ2(I,J)*BJ2(I,J))
      IF (BJ1(I,J).EQ.0.0D0) GO TO 82
      ZANG(I,J)=DATAN2(BJ2(I,J),BJ1(I,J))
      GO TO 81
82     IF (BJ2(I,J)) 83,84,85
83     ZANG(I,J)=-1.570796326794897
      GO TO 81
84     ZANG(I,J)=0.0D0
      GO TO 81
85     ZANG(I,J)=1.570796326794897
81     BUSH=2/

C PRINTOUT OF YBUS AND ZBUS MATRIX
90     IF (CHY.EQ.'N') GO TO 105
      TYPE 4000
4000  FORMAT(/1X,'**CALCULATED SYSTEM LINE DATA**'/1X,
1'LINE #',15X,'Y SHUNT',23X,'Y SERIES')
      DO 95 I=1,LNO
      TYPE 4100,I,YYSHT(I,1),YYSHT(I,2),YSER(I,1),YSER(I,2)
4100  FORMAT(I4,4X,2E14.6,2X,2E14.6)
95     CONTINUE
      TYPE 1010
1010  FORMAT(/1X,'**YBUS MATRIX**')
      DO 100 I=1,NBUS
      TYPE 1020,I
1020  FORMAT(1X,'ROW',I3)

```

```

1030 TYPE 1030, (YHAG(I,J),YANG(I,J),J=1,MBUS)
      FORMAT(6E12.5)
100  CONTINUE
      CHY='N'
105  IF (KINV.EQ.0)GO TO 120
      IF (CHZ.EQ.'N')GO TO 120
      TYPE 1040
1040 FORMAT(/1X,'**ZBUS MATRIX**')
      DO 110 I=1,MBUS
      TYPE 1020,I
      TYPE 1030, (ZHAG(I,J),ZANG(I,J),J=1,MBUS)
110  CONTINUE
      CHZ='N'

120  RETURN
      END

SUBROUTINE MBLF
C   CALCULATES P,Q,V,AND ANGLE AT EACH BUS
      INTEGER ABORT,BTYPE, MBUS
      DIMENSION DP(15)

      DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,EJ2,BJ3,BJ4,
      1CALP,CALQ,DQ,DVANG,DVHAG,G,H,ITL,P,C,VANG,VHAG,
      2XX,YANG,YHAG,YY,YYSH,ZANG,ZHAG,YSER,CHX,HHX,DP

COMMON /      AJ1(15,15),  AJ2(15,15),  AJ3(15,15),
1AJ4(15,15),  ALPHA(15),  BDAT,        BETA(15),
1BGSOL,      BJ1(15,15),  BJ2(15,15),  BJ3(15,15),
1BJ4(15,15),  BTYPE(15),  BUSH,       CALP(15),
1CALQ(15),   CB,CC,      CG,         CHB,
1CHG,       CHL,        CL,         CHY,
1CMZ,       DQ(15),    DVANG(15),  DVHAG(15),
1EB(30),    ESP1,      ESP2,      G(15),
1GAMMA(15), GDAT,      H(15),     IC(15),
1II,        ITER,     ITL(15),   KINV,
1KSOL,      LAMBDA,   LDAT,     LITER,
1LENGTH(30), LNO,     LOSS,     LPSOL,
1LSET,      MBUS,     M5,       NSWGB,
1P(15),     PD(15),   PG(15),   PGMX(15),
1PGMIN(15), Q(15),   QD(15),QDAT,  QG(15),
1QGMX(15),  QGHIN(15), SB(30),  YYSHT(30,2),
1IOL,TLDAT, TPD,TBDAT, TPL,TGEAT, VANG(15),
1VHAG(15),  VSPEC(15), XI(15,15), YANG(15,15),
1YHAG(15,15), YSHT(30,2), YI(15,15), ZANG(15,15),
1ZHAG(15,15), ZSER(30,2), YSER(30,2), ABORT,IBT(15)

LL=0
TYPE 100
100  F0BHAT(/1X,'**SOLVING LOAD FLOW EQUATIONS BY NR**')

C   CALCULATING G AND H AT EACH BUS
      IF (LSET.EQ.1)GO TO 13
      DO 1 I=1,MBUS
      VHAG(I)=DBLE(VSPEC(I))
      VANG(I)=0.000
      P(I)=DBLE(PG(I))-DBLE(PD(I))
      Q(I)=DBLE(QG(I))-DBLE(QD(I))
1    CONTINUE

```

```

13  CONTINUE
    DO 7 I=1,MBUS
      CALP(I)=0.000
      CALQ(I)=0.000

      DO 4 J=1,MBUS
        CALP(I)=CALP(I)+VMAG(I)*VMAG(J)*YHAG(I,J)
        1*DCOS(YANG(I,J)-VANG(I)+VANG(J))
        CALQ(I)=CALQ(I)-VMAG(I)*VMAG(J)*YHAG(I,J)
        1*DSIN(+YANG(I,J)-VANG(I)+VANG(J))
4    CONTINUE

      G(I)=P(I)-CALP(I)
      H(I)=Q(I)-CALQ(I)

7    CONTINUE
C    CHECK FOR CONVERGENCE(GHAX &HMAX.LT.TOL)

      GHAX=0.000
      HMAX=0.000

      DO 5 I=1,MBUS
        IF(GHAX.LT.DABS(G(I))) GHAX=DABS(G(I))
        IF(HMAX.LT.DABS(H(I))) HMAX=DABS(H(I))
5    CONTINUE
      IF((GHAX.LE.TOL).AND.(HMAX.LE.TOL)) GO TO 56

C*****GENERATING JACOBIAN AJ1
      DO 6 I=1,MBUS
        DO 8 J=1,MBUS
          IF(IABS(BTYPE(J)).EQ.3) GO TO 10.
          IF(J.EQ.I) GO TO 9
          AJ1(I,J)=-VMAG(I)*VMAG(J)*YHAG(I,J)
          1*DSIN(YANG(I,J)-VANG(I)+VANG(J))
          GO TO 8
9        AJ1(I,J)=0.000

          DO 12 K=1,MBUS
            IF(K.EQ.I) GO TO 12
            AJ1(I,J)=AJ1(I,J)+VMAG(I)*VMAG(K)*YHAG(I,K)
            1*DSIN(YANG(I,K)-VANG(I)+VANG(K))
12       CONTINUE

          GO TO 8
10      IF(J.EQ.I) GO TO 11
          AJ1(I,J)=0.000
          GO TO 8
11      -AJ1(I,J)=-1.000

8    CONTINUE
6    CONTINUE

C*****GENERATING JACOBIAN AJ2
      DO 14 I=1,MBUS

        DO 17 J=1,MBUS
          IF(IABS(BTYPE(J)).GT.1) GO TO 18
          IF(J.EQ.I) GO TO 15
          AJ2(I,J)=VMAG(I)*YHAG(I,J)
          1*DCOS(YANG(I,J)-VANG(I)+VANG(J))

```

```

GO TO 17
15  AJ2(I,J)=0.0D0
    DO 19 K=1,MBUS
    IF (K.NE.I) GO TO 16
    AJ2(I,J)=AJ2(I,J)+2*VHAG(I)*YHAG(I,I)
    1*DCOS(+YANG(I,I))
    GO TO 19
16  CONTINUE
    AJ2(I,J)=AJ2(I,J)+VHAG(K)*YHAG(I,K)
    1*DCOS(YANG(I,K)-VANG(I)+VANG(K))
19  CONTINUE
    GO TO 17

18  AJ2(I,J)=0.0D0
17  CONTINUE
14  CONTINUE

C*****GENERATING JACOBIAN AJ3
    DO 20 I=1,MBUS

    DO 24 J=1,MBUS
    IF(IABS(BTYPE(J)).EQ.3) GO TO 22
    IF(J.EQ.I) GO TO 23
    AJ3(I,J)=-VHAG(I)*YHAG(J)*YHAG(I,J)
    1*DCOS(YANG(I,J)-VANG(I)+VANG(J))

23  GO TO 24
    AJ3(I,J)=0.0D0

    DO 21 K=1,MBUS
    IF(K.EJ.J) GO TO 21
    AJ3(I,J)=AJ3(I,J)+VHAG(I)*VHAG(K)*YHAG(I,K)
    1*DCOS(YANG(I,K)-VANG(I)+VANG(K))
21  CONTINUE
    GO TO 24

22  AJ3(I,J)=0.0D0
24  CONTINUE
20  CONTINUE

C***** GENERATING JACOBIAN AJ4
    DO 29 I=1,MBUS

    DO 25 J=1,MBUS
    IF(IABS(BTYPE(J)).GT.1) GO TO 27
    IF(J.EQ.I) GO TO 28
    AJ4(I,J)=-VHAG(I)*YHAG(I,J)
    1*DSIN(YANG(I,J)-VANG(I)+VANG(J))
    GO TO 25

28  AJ4(I,J)=0.0D0

    DO 26 K=1,MBUS
    IF (K.NE.I) GO TO 30
    AJ4(I,J)=AJ4(I,J)-2*VHAG(I)*YHAG(I,I)
    1*DSIN(+YANG(I,I))
    GO TO 26
30  CONTINUE

```

```

      AJ4(I,J)=AJ4(I,J)-VMAG(K)*YMAG(I,K)
      1*DSIN(YANG(I,K)-VANG(I)+VANG(K))
26      CONTINUE
      GO TO 25
27      IF(J.EQ.I)GO TO 31
      AJ4(I,J)=0.0D0
      GC TO 25

31      AJ4(I,J)=-1.0D0
25      CONTINUE
29      CONTINUE

C      INVERTING JACOBIAN AJ4
      CALL MINV(AJ4,MBUS)

C*****GENERATING INVERSE SUBMATRIX EJ1,EJ2,EJ3,BJ4
C      BJ1=[AJ1-AJ2(AJ4***-1)AJ3]***-1

      CALL AMULT(YX,AJ2,AJ4,MBUS)
      CALL AMULT(YX,XX,AJ3,MBUS)
      DO 37 I=1,MBUS

      DC 39 J=1,MBUS
      BJ1(I,J) =AJ1(I,J)-YY(I,J)
39      CONTINUE
37      CONTINUE

C      INVERTING JACOBIAN BJ1
      CALL MINV(BJ1,MBUS)

C*****GENERATING JACOBIAN BJ2
C      BJ2=-BJ1*AJ2*(AJ4***-1)

      CALL AMULT(YY,BJ1,AJ2,MBUS)
      CALL AMULT(BJ2,YY,AJ4,MBUS)
      DO 44 I=1,MBUS
      DO 45 J=1,MBUS
      BJ2(I,J)=-1.0D0*(BJ2(I,J))
45      CONTINUE
44      CONTINUE

C*****GENERATING JACOBIAN BJ3
C      BJ3=-(AJ4***-1)*AJ3*BJ1
      CALL AMULT(YY,AJ3,BJ1,MBUS)
      CALL AMULT(BJ3,AJ4,YY,MBUS)

      DO 47 I=1,MBUS

      DO 48 J=1,MBUS
      BJ3(I,J)=-1.0D0*BJ3(I,J)

48      CONTINUE
47      CONTINUE

C*****GENERATING JACOBIAN BJ4
C      BJ4=(AJ4***-1)-(AJ4***-1)*AJ3*BJ2
      CALL AMULT(YY,AJ4,AJ3,MBUS)

```



```

CALL ABULT(XX,YY,BJ2,MBUS)
DO 51 I=1,MBUS
DC 50 J=1,MBUS
BJ4(I,J)=AJ4(I,J)-XX(I,J)
50 CONTINUE
51 CONTINUE

C CALCULATING DELTA P,Q,VHAG,ANGLE
DO 52 I=1,MBUS
DP(I)=0.000
DQ(I)=0.000
DVMAG(I)=0.000
DVANG(I)=0.000
IF(IABS(BTYPE(I)).EQ.3)GO TO 54
IF(IABS(BTYPE(I)).EQ.2)GO TO 55
DC 53 J=1,MBUS
DVMAG(I)=DVMAG(I)+BJ3(I,J)*G(J)+BJ4(I,J)*H(J)
53 DVANG(I)=DVANG(I)+BJ1(I,J)*G(J)+BJ2(I,J)*H(J)
GO TO 52
DO 64 J=1,MBUS
DP(I)=DP(I)+BJ1(I,J)*G(J)+BJ2(I,J)*H(J)

64 DQ(I)=DQ(I)+BJ3(I,J)*G(J)+BJ4(I,J)*H(J)
GO TO 52
DO 65 J=1,MBUS
DQ(I)=DQ(I)+BJ3(I,J)*G(J)+BJ4(I,J)*H(J)
65 DVANG(I)=DVANG(I)+BJ1(I,J)*G(J)+BJ2(I,J)*H(J)
52 CONTINUE

C CALCULATING NEW P,Q,V,ANGLE
DO 62 I=1,MBUS
P(I)=P(I)+DP(I)
Q(I)=Q(I)+DQ(I)
VMAG(I)=VMAG(I)+DVMAG(I)
VANG(I)=VANG(I)+DVANG(I)
IF(IABS(BTYPE(I)).NE.2)GO TO 62
QMAX=QMAX(I)-QD(I)
QMIN=QMIN(I)-QD(I)
IF(Q(I).LT.DBLE(QMAX))GO TO 58
Q(I)=DBLE(QMAX)
BTYPE(I)=ISIGN(1,BTYPE(I))
IBT(I)=2
TYPE 3000,I
3000 FORMAT(1X,'BUS #',I3,2X,'EXCEEDS QMAX,
1BUS CHANGED TO TYPE 1')
GO TO 62
58 IF(Q(I).GT.DBLE(QMIN))GO TO 62
Q(I)=DBLE(QMIN)
BTYPE(I)=ISIGN(1,BTYPE(I))
IBT(I)=2
TYPE 3001,I
3001 FORMAT(1X,'BUS #',I3,2X,'EXCEEDS QMIN,
1BUS CHANGED TO TYPE 1')
62 CONTINUE
LL=LL+1
IF(LL.LT.LITER)GO TO 13

TYPE 2300,LL
2300 FORMAT(1X,'****WILL NOT CONVERGE IN',I3,2X,' ITERATIONS')
ABORT=1

```

```

GC TO 60
C      PRINT OUT SOLUTIONS
56     TYPE 2400,LL
2400   PCFMAT(1X,'***** CONVERGENCE IN ',I3,' ITERATIONS')
      DO 70 I=1,NBUS
      PG(I)=P(I)+PD(I)
70     QG(I)=Q(I)+QD(I)
      RETURN
      END

SUBROUTINE GSLP
CSUBROUTINE TO CALCULATE LOAD FLOW EQUATIONS BY GAUSS-SEIDEL

INTEGER MBUS,ABORT,BTYPE
DIMENSION AI(15),BI(15,15)

DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,EJ3,BJ4,
ICALP,CALQ,DQ,DVANG,DVHAG,G,H,ITL,P,Q,VANG,VHAG,
ZXX,YANG,YHAG,YY,YYSH,ZANG,ZHAG,YSER,
3SHAG(15),SANG(15),AI,BI,VI,VII,VNEV,DELV,DVHAX,WANG
COMMON / / AJ1(15,15), AJ2(15,15), AJ3(15,15),
1AJ4(15,15), ALPHA(15), BDAT, BETA(15),
1BGSOL, BJ1(15,15), BJ2(15,15), BJ3(15,15),
1BJ4(15,15), BTYPE(15), BUSH, CALP(15),
ICALQ(15), CB,CC, CG, CHH,
1CHG, CHL, CL, CHY,
1CHZ, DQ(15), DVANG(15), DVHAG(15),
1EN(30), ESP1, ESP2, G(15),
1GAMMA(15), GDAT, H(15), IC(15),
1II, ITER, ITL(15), KINV,
1KSCL, LAMBDA, LOAT, LITER,
1LNTH(30), LNO, LOSS, LPSOL,
1LSET, MBUS, NS, NSWGB,
1P(15), PD(15), PG(15), PGMAX(15),
1PGHIN(15), Q(15), QD(15),QDAT, QG(15),
1QGHAX(15), QGHIN(15), SB(30), YYSHT(30,2),
1TOL, TLDAT, TPD, TBDA, TPL, TGDAT, YANG(15),
1VHAG(15), VSPEC(15), XI(15,15), YANG(15,15),
1VHAG(15,15), YSHT(30,2), YY(15,15), ZANG(15,15),
1ZHAG(15,15), ZSER(30,2), YSEB(30,2), ABORT,IBT(15)

TYPE=1000
1000   FORMAT(/1X,'**SOLVING LOAD FLOW EQUATIONS BY GS**')

C CALCULATING COMPLEX BUS POWER AND VARIABLES A & B
DC 10 I=1,MBUS
IF (LSET.EQ.1) GO TO 5
VHAG(I)=DBLE(VSPEC(I))
VANG(I)=0.000
5     IF (IABS(BTYPE(I)).NE.3) GO TO 12
      NSWGB=I
      GO TO 10
12    P(I)=DBLE(PG(I))-DBLE(PD(I))
      IF (IABS(BTYPE(I)).EQ.2) GO TO 25
      Q(I)=DBLE(QG(I))-DBLE(QD(I))
      SHAG(I)=DSQRT(P(I)*P(I)+Q(I)*Q(I))
      IF (P(I).EQ.(0.000)) GO TO 14
      SANG(I)=DATAN2(Q(I),P(I))

```

```

14      GO TO 22
16      IF (Q(I)) 16, 18, 20
16      SANG(I) = -1.570796326794897
16      GO TO 22
18      SANG(I) = 0.000
18      GO TO 22
20      SANG(I) = +1.570796326794897
22      AI(I) = SHAG(I)/YHAG(I,I)
25      DO 10 J=1, MBUS
10      BI(I, J) = YHAG(I, J)/YHAG(I, I)
10      CONTINUE

28      L=0
28      DVHAX=0.000

C CALCULATING BUS VOLTAGES
DO 30 I=1, MBUS
40      IF (IABS(BTYPE(I)) .EQ. 3) GO TO 30
40      IF (IABS(BTYPE(I)) .NE. 2) GO TO 80

C TYPE 2 BUS VHAG IS RESET TO VSPEC, Q IS COMPUTED AND
C VARIABLES AI & AII ARE RECOMPUTED.
Q(I) = 0.000
QHAX = QGMAX(I) - QD(I)
QHIN = QGHIN(I) - QD(I)
DO 60 J=1, MBUS
60      Q(I) = Q(I) - DBLE(VSPEC(I)) * VHAG(J) * YHAG(I, J) *
1DSIN(YANG(I, J) - VANG(I) + VANG(J))
IF (Q(I) .LE. DBLE(QHAX)) GO TO 70
Q(I) = DBLE(QHAX)
BTYPE(I) = ISIGN(1, BTYPE(I))
IBT(I) = 2
TYPE 3000, I
3000    FORMAT(1X, 'BUS #', I3, 2X, 'EXCEEDS QGMAX,
1BUS CHANGED TO TYPE 1')
GO TO 72
70      IF (Q(I) .GE. DBLE(QHIN)) GO TO 72
Q(I) = DBLE(QHIN)
BTYPE(I) = ISIGN(1, BTYPE(I))
IBT(I) = 2
TYPE 3001, I
3001    FORMAT(1X, 'BUS #', I3, 2X, 'EXCEEDS QGHIN,
1BUS CHANGED TO TYPE 1')
72      SHAG(I) = DSQRT(P(I)*P(I) + Q(I)*Q(I))
IF (P(I) .EQ. (0.000)) GO TO 74
SANG(I) = DATAN2(Q(I), P(I))
GO TO 84
74      IF (Q(I)) 76, 78, 82
76      SANG(I) = -1.570796326794897
GO TO 84
78      SANG(I) = 0.000
GO TO 84
82      SANG(I) = +1.570796326794897
84      AI(I) = SHAG(I)/YHAG(I, I)

C CALCULATING COMPLEX BUS VOLTAGES
80      VI = (AI(I)/VHAG(I)) * DCOS(VANG(I) - YANG(I, I) - SANG(I))
VII = (AI(I)/VHAG(I)) * DSIN(VANG(I) - YANG(I, I) - SANG(I))
DO 90 J=1, MBUS

```

```

IF(J.EQ.I)GO TO 90
VI=VI-BI(I,J)*VMAG(J)*DCOS(VANG(J)
1+YANG(I,J)-YANG(I,I))
VII=VII-BI(I,J)*VMAG(J)*DSIN(VANG(J)
1+YANG(I,J)-YANG(I,I))
90 CONTINUE
VNEW=DSQRT((VI*VI)+(VII*VII))
IF(VNEW.EQ.0.000)GO TO 92
IF(VI.EQ.(0.000))GO TO 86
NANG=DATAN2(VII,VI)
GO TO 95
86 IF(VII)88,92,94
88 NANG=-1.570796326794897
GO TO 95
92 NANG=0.000
GO TO 95
94 NANG=+1.570796326794897

C CALCULATING VOLTAGE MAGNITUDE DIFFERENCE BETWEEN ITERATIONS
C AND MULTIPLY BY ACCELERATION FACTOR OF 1.5
95 VNEW=VMAG(I)+1.500*(VNEW-VMAG(I))
NANG=VANG(I)+1.500*(NANG-VANG(I))
DELV=VNEW-VMAG(I)
IF(DABS(DELV).GT.DVMAX)DVMAX=DABS(DELV)
IF(XABS(BTYPE(I)).EQ.2)GO TO 96
VMAG(I)=VNEW
96 VANG(I)=NANG
30 CONTINUE
IF(DVMAX.LE.TOL)GO TO 100
L=L+1
IF(L.LE.LITER)GO TO 28
TYPE 1010,L
1010 FORMAT(11X,'NO CONVERGENCE IN ',I3,2X,'ITERATIONS')
ABORT=1
RETURN

C COMPUTE SWING BUS POWER
100 I=MSVGB
P(I)=0.000
Q(I)=0.000
DO 110 J=1,MBUS
P(I)=P(I)+VMAG(I)*VMAG(J)*YHAG(I,J)*
1DCOS(YANG(I,J)-VANG(I)+VANG(J))
Q(I)=Q(I)-VMAG(I)*VMAG(J)*YHAG(I,J)*
1DSIN(YANG(I,J)-VANG(I)+VANG(J))
110 CONTINUE
TYPE 1020,L
1020 FORMAT(11X,'GSLF CONVERGENCE IN ',I3,2X,'ITERATIONS')
DO 120 I=1,MBUS
PG(I)=P(I)+PD(I)
120 QG(I)=Q(I)+QD(I)
RETURN
END

SUBROUTINE OPT
C SUBROUTINE TO CALCULATE ITL,IC, AND POWER FOR EACH GENERATOR
C CALCULATES OPTIMUM LAMBDA FOR SYSTEM

REAL IC,LAMBDA

```

```

INTEGER ABORT,BTYPE,MBUS
DIMENSION PGSAV(15)

```

```

DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,EJ2,EJ3,EJ4,
1CALP,CALQ,DQ,DYANG,DVHAG,G,H,ITL,P,Q,YANG,VHAG,
2XX,YANG,YHAG,YY,YISHT,ZANG,ZHAG,ZSER,A,E
COMMON / AJ1(15,15), AJ2(15,15), AJ3(15,15),
1AJ4(15,15), ALPHA(15), BDAT, EETA(15),
1EGSOL, BJ1(15,15), BJ2(15,15), BJ3(15,15),
1BJ4(15,15), BTYPE(15), BUSH, CALP(15),
1CALQ(15), CB,CC, CG, CHB,
1CHG, CHL, CL, CHY,
1CHEZ, DQ(15), DVANG(15), DVHAG(15),
1EB(30), ESP1, ESP2, G(15),
1GAMMA(15), GDAT, H(15), IC(15),
1II, ITER, ITL(15), KINV,
1KSOL, LAMBDA, LDAT, LITER,
1LNGTH(30), LNO, LOSS, LPSOL,
1LSET, MBUS, N5, NSWGB,
1P(15), PD(15), PG(15), PGMAX(15),
1PGMIN(15), Q(15), QD(15), QDAT, QG(15),
1QGMAX(15), QGMIN(15), SB(30), YISHT(30,2),
1TOL, TLDAT, TPD, TBDAT, TPL, TGDAT, YANG(15),
1VHAG(15), VSPEC(15), YX(15,15), YANG(15,15),
1YHAG(15,15), YSHT(30,2), YY(15,15), ZANG(15,15),
1ZHAG(15,15), ZSER(30,2), YSER(30,2), ABORT,IBT(15)

```

```

5 II=0
L=0
TPD=0.0
TPL=0.0
TPGCC=0.0

```

```

C COMPUTE TOTAL POWER DEMAND & LOSS AND TOTAL POWER
C GENERATED AT CONSTANT COST

```

```

DO 10 I=1,MBUS
TPD=TPD+PD(I)
TPL=TPL+P(I)
IF(BTYPE(I).GE.0)GO TO 10
IF((ALPHA(I).EQ.0.0).AND.(BETA(I).EQ.0.0).AND.
1(GAMMA(I).EQ.0.0).EQ.0.0)TPGCC=TPGCC+PGMAX(I)
10 CONTINUE

```

```

C CHECK FOR NEGATIVE TOTAL POWER LOSS
IF(TPL.GE.0.0)GO TO 20

```

```

1000 TYPE 1000
FORNAT(11X,'SYSTEM POWER LOSS IS NEGATIVE.'/11X,' CHECK
1TOTAL SYSTEM POWER GENERATION')
RETURN

```

```

20 IF(LOSS.EQ.'Y')TPL=0.0
IF(TPGCC.LT.(TPD+TPL))GO TO 30
TYPE 1010

```

```

1010 FORNAT(11X,'MAX CONSTANT COST POWER NOT USED.'/11X,
1'LOAD FLOW PROBLEM ONLY')
RETURN

```

```

C DETERMINE INITIAL LAMBDA

```

```

30 IF(LSET.EQ.1)GO TO 40
LAMBDA=5000.0
DO 50 I=1,MBUS

```

```

IF ((BTYPE(I).GE.0).OR.(ALPHA(I).EQ.0)) GO TO 50
IF (ALPHA(I).LT.LAMBDA) LAMBDA=ALPHA(I)
PGSAV(I)=PG(I)
50 CONTINUE
DLAM=0.8*LAMBDA
LSET=1
40 TYPE 1020
1020 FORMAT(5X,'***OPTIMIZING COST FUNCTIONS***')

C SKIP ITL CALCULATIONS IF LOSSLESS SYSTEM
IF (LOSS.EQ.'Y') GO TO 60

C CALCULATING ITL'S
DO 70 I=1,NBUS
IF (BTYPE(I).GE.0) GO TO 70
ITL(I)=0.000
DO 80 J=1,NBUS
IF (BTYPE(J).GE.0) GO TO 80
A=((ZHAG(I,J)*DCOS(ZANG(I,J)))/(VHAG(I)*VHAG(J)))*
1DCOS(VANG(I)-VANG(J))
B=((ZHAG(I,J)*DCOS(ZANG(I,J)))/(VHAG(I)*VHAG(J)))*
1DSIN(VANG(I)-VANG(J))
ITL(I)=ITL(I)+(P(J)*A-Q(J)*B)
80 CONTINUE
ITL(I)=ITL(I)+ITL(I)
70 CONTINUE

C OPTIMIZING LAMBDA
60 DPSAV=0.0
85 CONTINUE
TPG=0.0
DO 90 I=1,NBUS
IF (BTYPE(I).GE.0) GO TO 90
IF ((ALPHA(I).EQ.0.0).AND.(BETA(I).EQ.0.0).AND.
1(GAMMA(I).EQ.0.0)) GO TO 100
IF (LOSS.EQ.'N') GO TO 110
IC(I)=LAMBDA
GO TO 120
110 IC(I)=LAMBDA*(1.0-ITL(I))
IF (IC(I).GE.ALPHA(I)) GO TO 120
PG(I)=0.0
GO TO 89

C COMPUTE PG'S FROM COST FUNCTIONS
120 IF (GAMMA(I).NE.0.0) GO TO 130
PG(I)=(IC(I)-ALPHA(I))/BETA(I)
GO TO 89
130 C=BETA(I)*BETA(I)-4.0*(ALPHA(I)-IC(I))*GAMMA(I)
IF (C.GE.0.0) GO TO 140
C TYPE 1030,I
1030 FORMAT(1X,'COST CURVE COEFFICIENTS GIVE NEGATIVE
1DETERMINANT,GENERATOR',I3,2X,'SET TO ZERO')
135 PG(I)=0.0
GO TO 89
140 C=SQR(C)
PG(I)=(-BETA(I)+C)/(2.0*GAMMA(I))
IF (PG(I).GE.PGMIN(I)) GO TO 89
PG(I)=(-BETA(I)-C)/(2.0*GAMMA(I))
IF (PG(I).GE.PGMIN(I)) GO TO 89
PG(I)=PGMIN(I)
C TYPE 1032,I

```

```

1032  PCHMAT(IX,I3,IX,'PG NEG, GEN. SET TO 0.0')
      GO TO 89
100   PG(I)=PGHAX(I)
      IF((ALPHA(I).EQ.0.0).AND.(BETA(I).EQ.0.0).AND.
1(GAMMA(I).EQ.0.0))GO TO 150
89    CCNTINUE

C CHECK FOR PGHAX CCNSTRANTS
      IF(PG(I).LE.PGHAX(I))GO TO 105
      PG(I)=PGHAX(I)
C     TYPE 1036,I,PGHAX(I)
1036  FORMAT(IX,I3,'PG EXCEEDS PGEAX, GEN RESET TC',F12.7)
      GO TO 165
105   IF(PG(I).GE.PGHIN(I))GO TO 150
      PG(I)=PGHIN(I)
C     TYPE 1038,I,PGHIN(I)
1038  FORMAT(IX,I3,IX,'PG EXCEEDS PGHIN, GEN RESET TO',F12.5)
165   IF(GAMMA(I).NE.0.0)GO TO 160
      IC(I)=ALPHA(I)+BETA(I)*PG(I)
      GO TO 150
160   IC(I)=ALPHA(I)+BETA(I)*PG(I)+GAMMA(I)*PG(I)*PG(I)
150   TPG=TPG+PG(I)
90    CONTINUE

C CHECK POWER BALANCE LESS THAN ESP1
      DP=TPG-TPD-TPL
      IF(ABS(DP).LE.ESP1)GO TO 210
      L=L+1
      IF(L.LE.ITER)GO TO 170
      TYPE 1040,L
1040  FORMAT(11X,'POWER BALANCE EQUATIONS NOT SATISFIED IN '
1,I3,2X,'ITERATIONS, '/11X,'CHECK COST CURVES AND
2TOLERANCES')
      RETURN

C ADJUST LAMBDA IN COMPARISON TO PREVIOUS ITERATION
170   IF((DPSAV.GE.0.0).AND.(DP.GT.0.0))GO TO 160
      IF((DPSAV.LE.0.0).AND.(DP.LT.0.0))GO TO 190
      IF((DPSAV.GE.0.0).AND.(DP.LT.0.0))GO TO 200
      DLAM=0.5*DLAM
180   LAMBDA=LAMBDA-DLAM
      DPSAV=DP
      GO TO 85
200   DLAM=0.5*DLAM
190   LAMBDA=LAMBDA+DLAM
      DPSAV=DP
      GO TO 85
210   II=II+1
      TYPE 1050,L
1050  FORMAT(11X,'LAMBDA DETERMINED IN ',I3,2X,'ITERATIONS')

C CHECK PG(I) CONVERGENCE .LE. ESP2
      DO 220 I=1,NBUS
      IF(BTYPE(I).GE.0)GO TO 220
      IF(ABS(PG(I)-PGSAV(I)).GT.ESP2)GO TO 230
220   CONTINUE
      RETURN

230   DO 240 I=1,NBUS
      PGSAV(I)=PG(I)
      P(I)=DBLE(PG(I))-DBLE(PD(I))

```

```

      IF (IBT(I) .NE. 2) GO TO 240
      BTYPE(I) = ISIGN(2, BTYPE(I))
      VMAG(I) = 1.0
      IBT(I) = 0
240   CONTINUE
      IF (KSOL .EQ. 1) GO TO 260
250   CALL NRLP
      GO TO 5
260   CALL GSLP
      GO TO 5
      END

```

```

SUBROUTINE CTRI(A,B,C,D,N)
DOUBLE PRECISION A(15,15),B(15,15),C(15,15),D(15,15),T(2),SUM(2)

```

```

C TRIANGULARIZE A INTO B (LOWER) AND
C B UPPER TRIANG MATRIX

```

```

      DO 100 I=1,N
      C(I,1) = A(I,1)
      D(I,1) = B(I,1)
100   DO 105 J=2,N
      CALL CDIV(T(1),T(2),A(1,J),
      1B(1,J),A(1,1),B(1,1))
      C(1,J) = T(1)
105   D(1,J) = T(2)

      DO 275 IJ=2,N
      DO 250 J=IJ,N
      DO 250 I=IJ,N
      IF (I.LT.J) GO TO 205
      JM1=J-1
      SUM(2) = 0.0D0
      SUM(1) = SUM(2)
      DO 200 K=1,JM1
      CALL CHUL(T(1),T(2),C(I,K),
      1D(I,K),C(K,J),D(K,J))
      SUM(1) = SUM(1) + T(1)
200   SUM(2) = SUM(2) + T(2)
      C(I,J) = A(I,J) - SUM(1)
      D(I,J) = B(I,J) - SUM(2)
      GO TO 250
205   CONTINUE
      CALL CDIV(T(1),T(2),C(J,I),
      1D(J,I),C(I,I),D(I,I))
      C(I,J) = T(1)
      D(I,J) = T(2)
250   CONTINUE
275   CONTINUE

      DO 280 I=1,N
      DO 280 J=1,N
      IF (I.GE.J) GO TO 280
      D(I,J) = 0.0D0
      C(I,J) = D(I,J)
280   CONTINUE
      RETURN
      END

```



```

SUBROUTINE CTRIV (A,B,C,D,N)
DOUBLE PRECISION A(15,15),B(15,15),C(15,15),D(15,15),
1SUM(2),T(2),AI
I=N
10 CONTINUE
K=I
20 CONTINUE
SUM(2)=0.0D0
SUM(1)=SUM(2)
AI=SUM(1)
IF(K-I) 25,22,25
22 AI=1.0D0
25 J=K+1
IF(J.GT.N) GO TO 40
DO 30 JJ=J,N
CALL CMUL(T(1),T(2),A(JJ,K),
1 B(JJ,K),C(I,JJ),D(I,JJ))
SUM(1)=SUM(1)+T(1)
30 SUM(2)=SUM(2)+T(2)
40 T(1)=AI-SUM(1)
T(2)=-SUM(2)
CALL CDIV(SUM(1),SUM(2),T(1),T(2))
1,A(K,K),B(K,K))
C(K,I)=SUM(1)
C(I,K)=C(K,I)
D(K,I)=SUM(2)
D(I,K)=D(K,I)
K=K-1
IF(K.EQ.0) GO TO 50
GO TO 20
50 I=I-1
IF(I.EQ.0) GO TO 60
GO TO 10
60 CONTINUE
RETURN
END

```

SUBROUTINE SOL

C SUBROUTINE TO CALCULATE AND PRINT BUS & GENERATOR SOLUTIONS
C AND LINE POWER FLOW

```

REAL LAMBDA,IC
INTEGER BTYPE,BGSOL,EB,SB
DOUBLE PRECISION AJ1,AJ2,AJ3,AJ4,BJ1,BJ2,EJ3,EJ4,
1CALP,CALQ,DQ,DVANG,DVHAG,G,H,ITL,P,Q,VANG,VHAG,
2XX,YANG,YHAG,YY,YSBT,ZANG,ZHAG,YSER,
3YA,YB,YSHTA,YSHTB,PLH,QLH

```

```

COMMON/ / AJ1(15,15), AJ2(15,15), AJ3(15,15),
1AJ4(15,15), ALPHA(15), BDAT, BETA(15),

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1BGSOL,      BJ1(15,15),  BJ2(15,15),  BJ3(15,15),
1BJ4(15,15), BTYPE(15),  BUSH,        CALF(15),
1CALQ(15),   CB,CC,      CG,          CHB,
1CHG,        CHL,        CL,          CHY,
1CHZ,        DQ(15),   DVANG(15),  EVHAG(15),
1EB(30),     ESP1,      ESP2,        G(15),
1GAMMA(15),  GDAT,          H(15),      IC(15),
1II,         ITER,      ITL(15),    KINV,
1KSOL,       LAMBDA,    LDAT,       LITER,
1LENGTH(30), LNO,          LOSS,       LPSCL,
1LSET,       MBUS,     NS,         NSWGB,
1P(15),      PD(15),   PG(15),     PGMAX(15),
1PGMIN(15),  Q(15),         QD(15), QDAT,  QG(15),
1QGMAX(15),  QGMIN(15),    SB(30),     YSET(30,2),
1TOL, TLDAT, TPD, TEDAT,  TPL, TGDAT,  VANG(15),
1VHAG(15),   VSPEC(15), IX(15,15),  YANG(15,15),
1VEAG(15,15), YSHT(30,2), YY(15,15),  ZANG(15,15),
1ZHAG(15,15), ZSER(30,2),  YSER(30,2),  ABORT

IF (BGSOL.EQ.0) GO TO 280
IF (KINV.EQ.1) GO TO 265
TPD=0.0
TPL=0.0
DO 275 I=1,MBUS
  TPD=TPD+PD(I)
  TPL=TPL+P(I)
275 CONTINUE
  WRITE(N5,1157) TPL,TPD
1157 FORMAT(/1X,'****SYSTEM BUS AND GENERATOR SOLUTIONS****'/
  11X,'SYSTEM LOSSES (PU)=' ,F8.4,' , SYSTEM LOAD (PU)=' ,F8.4,/
  21X,'BUS #',1X,'BTYPE',6X,'PG',6X,'QG',6X,'PD',6X,
  3'QD',5X,'VHAG',4X,'VANG')
  DO 277 I=1,MBUS
    PG(I)=P(I)+PD(I)
    QG(I)=Q(I)+QD(I)
277 WRITE(N5,1158) I,BTYPE(I),PG(I),QG(I),PD(I),QD(I),
  1VHAG(I),VANG(I)
1158 FORMAT(1X,I3,3X,I3,4X,6F8.4)
  BGSOL=0
  GO TO 280
265 WRITE(N5,1155) II,ESP1,ESP2,LAMBDA,TPL,TPD
1155 FORMAT(/1X,'****SYSTEM BUS AND GENERATOR SOLUTIONS****'/
  16X,'ECON. DISPATCH CONVERGENCE IN',I3,' ITERATIONS'/
  12X,'ESP1=' ,F8.4,' , ESP2=' ,F8.4,' , LAMBDA=' ,F8.4,/1X,'SYSTEM
  3LOSSES (PU)=' ,F8.4,' , SYSTEM LOAD (PU)=' ,F8.4,/
  41X,'BUS #',1X,'BTYPE',4X,'IC',5X,'ITL',6X,'PG',6X,
  5'QG',6X,'PD',6X,'QD',5X,'VHAG',4X,'VANG')

  DO 270 I=1,MBUS
    PG(I)=P(I)+PD(I)
    QG(I)=Q(I)+QD(I)
270 WRITE(N5,1160) I,BTYPE(I),IC(I),ITL(I),PG(I),QG(I),
  1PD(I),QD(I),VHAG(I),VANG(I)
1160 FORMAT(1X,I3,1X,I3,F10.4,7F8.4)
  BGSOL=0
280 CONTINUE
  IF (LPSOL.EQ.0) GO TO 300

C CALCULATING LINE POWER FLOW
  WRITE(N5,1190)

```

```

1190  PCRHAT(/1X,'****LINE POWER FLOW****'/1X,'LINE',3X,'SB',4X,'EB',
      14X,'REAL POWER',4X,'REACTIVE POWER')
      DO 300 I=1,LNO
      L=SB(I)
      M=EB(I)
      YH=DSQRT((YSER(I,1)*YSER(I,1))+(YSER(I,2)*YSER(I,2)))
      YSHTH=DSQRT((YYSHT(I,1)*YYSHT(I,1))
      1+(YYSHT(I,2)*YYSHT(I,2)))
      IF(YSER(I,1).EQ.0.0D0)GO TO 302
      YA=DATAN2(YSER(I,2),YSER(I,1))
      GO TO 306
302  IF(YSER(I,2))303,304,305
303  YA=-1.570796326794897
      GO TO 306
304  YA=0.0D0
      GO TO 306
305  YA=1.570796326794897
306  IF(YYSHT(I,1).EQ.0.0D0)GO TO 308
      YSHTA=DATAN2(YYSHT(I,2),YYSHT(I,1))
      GO TO 314
308  IF(YYSHT(I,2))309,311,312
309  YSHTA=-1.570796326794897
      GO TO 314
311  YSHTA=0.0D0
      GO TO 314
312  YSHTA=1.570796326794897
314  CCNTINUE

      JJ=0
310  P1H=VMAG(L)*VMAG(I)*YH*DCOS(YA)
      1-VMAG(L)*VMAG(M)*YH*DCOS(VANG(L)-VANG(M)-YA)
      2+VMAG(L)*VMAG(I)*YSHTH*DCOS(YSHTA)

      Q1H=-VMAG(L)*VMAG(L)*YH*DSIN(YA)
      1-VMAG(L)*VMAG(M)*YH*DSIN(VANG(L)-VANG(M)-YA)
      2-VMAG(L)*VMAG(L)*YSHTH*DSIN(YSHTA)
      WRITE(NS,1200)I,L,M,P1H,Q1H
1200  PCRHAT(1X,I3,4X,I3,3X,I3,F12.4,6X,F12.4)
      IF(JJ.EQ.1)GO TO 300
      JJ=1
      L=EB(I)
      M=SB(I)
      GO TO 310
300  CONTINUE
      IPSOL=0
      RETURN
      END

SUBROUTINE ANULT(Z,X,Y,M)
DOUBLE PRECISION Z(15,15),X(15,15),Y(15,15)

DO 1 I=1,M
DO 1 J=1,M
Z(I,J)=0.0D0
DO 1 K=1,M
Z(I,J)=Z(I,J)+X(I,K)*Y(K,J)
1  CONTINUE
RETURN
END

```

```

SUBROUTINE CMUL(X,Y,A,B,C,D)
DOUBLE PRECISION X,Y,A,B,C,D
X=A*C-B*D
Y=A*D+B*C
RETURN
END
SUBROUTINE CDIV(X,Y,A,B,C,D)
DOUBLE PRECISION X,Y,A,B,C,D
X=C*C+D*D
Y=(B*C-A*D)/X
Y=(A*C+B*D)/X
RETURN
END

```

```

SUBROUTINE CINVT(A,B,C,D)
A=C/(C*C+D*D)
B=-D/(C*C+D*D)
RETURN
END

```

```

FUNCTION CABS(A,B)
DOUBLE PRECISION CABS,A,B,DSQRT
CABS=DSQRT(A*A+B*B)
RETURN
END

```

```

SUBROUTINE DPINVT(A,B,C,D)
DOUBLE PRECISION A,B,C,D
A=C/(C*C+D*D)
B=-D/(C*C+D*D)
RETURN
END

```

```

SUBROUTINE MINV (A,N)
C THIS SUBPROGRAM IS FOR MATRIX INVERSION AND SIMUL
C LINEAR EQUATIONS
C A=THE GIVEN COEFFICIENT MATRIX A;A**-1 WILL BE
C STORED IN THIS MATRIX AT RETURN TO THE MAIN PROGRAM
C
C N=ORDER OF A;N.GE.1
C DIMENSION IPVOT(15),INDEX(15,2)
C DOUBLE PRECISION A(15,15),B(15,15),PIVOT(15),T
C EQUIVALENCE (IBOW,JROW),(ICOL,JCOL)
C
C FOLLOWING 3 STATEMENTS FOR INITIALIZATION
C M=0
57 DET=1.0
C DO 17 J=1,N
17 IPVCI(J)=0
C
C DO 135 I=1,N
C

```

```

C      FOLLOWING 12 STATEMENTS FOR SEARCH FOR
C      PIVOT ELEMENT
C
      T=0.0D0
      DO 9 J=1,N
      IF (IPVOT(J).EQ.1) GO TO 9
13     DO 23 K=1,N
      IF (IPVOT(K)-1) 43,23,81
43     IF (DABS(T)-GE.DABS(A(J,K))) GO TO 23
83     IROW=J
      ICOL=K
      T=A(J,K)
23     CONTINUE
9      CONTINUE
C
      IPVOT(ICOL)=IPVOT(ICOL)+1
C
C      FOLLOWING 15 STATEMENTS TO PUT PIVOT
C      ELEMENT ON DIAGONAL
C
      IF (IROW.EQ.ICOL) GO TO 109
23     DET = -DET
      DO 12 L=1,N
      T=A(IROW,L)
12     A(IROW,L) = A(ICOL,L)
      A(ICOL,L) = T
      IF (M.LE.0) GO TO 109
33     DO 2 L=1,M
      T=B(IROW,L)
      B(IROW,L)=B(ICOL,L)
2     B(ICOL,L)=T
109    INDEX(I,1)=IROW
      INDEX(I,2)=ICOL
      PIVOT(I)=A(ICOL,ICOL)
      DET=DET*PIVOT(I)
C
C      FOLLOWING 6 STATEMENTS TO DIVIDE PIVOT ROW
C      BY PIVOT ELEMENT
C
      A(ICOL,ICOL)=1.0D0
205    DO 205 L=1,N
      A(ICOL,L)=A(ICOL,L)/PIVOT(I)
      IF (M.LE.0) GO TO 347
66     DO 52 L=1,M
52     B(ICOL,L)=B(ICOL,L)/PIVOT(I)
C
C      FOLLOWING 10 STATEMENTS TO REDUCE NON-PIVOT ROWS
C
C
347    DO 135 LI=1,N
      IF (LI.EQ.ICOL) GO TO 135
21     T=A(LI,ICOL)
      A(LI,ICOL)=0.0D0
      DO 89 L=1,N
89     A(LI,L)=A(LI,L)-A(ICOL,L)*T
      IF (M.LE.0) GO TO 135
18     DO 68 L=1,M
68     B(LI,L)=B(LI,L)-B(ICOL,L)*T
135    CONTINUE
C
C      FOLLOWING 11 STATEMENTS TO INTERCHANGE COLUMNS

```

```
C
222 DO 3 I=1,N
      L=N-I+1
      IF(INDEX(L,1).EQ.INDEX(L,2)) GO TO 3
19   JROW = INDEX(L,1)
      JCOL = INDEX(L,2)
      DO 549 K=1,N
        T = A(K,JROW)
        A(K,JROW)=A(K,JCOL)
        A(K,JCOL)=T
549   CCNTINUE
      3   CONTINUE
      61  RETURN
        END
```

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