

# A CHARGE-BALANCING INCREMENTAL ANALOG TO DIGITAL CONVERTER FOR INSTRUMENTAL APPLICATIONS

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## ABSTRACT

A switched-capacitor technique for realization of one bit serial A/D converter is presented. A conversion accuracy that is higher than 15 bits can be expected from its integrated realization. Results of simulation are presented. It is shown that arithmetic operations on bit serial signals are possible. Using arithmetic operations on delta-modulated signals, it is possible to build inexpensive options necessary in instrumentation.

Key words: switched-capacitor, delta-sigma modulation, delta-full adder.

## INTRODUCTION

The basic circuit diagram of the delta-sigma modulator ( $D\Sigma M$ ) and waveforms at relevant terminal points are shown in Fig. 1a, b, c, d, respectively. The control loop acts in such a way that the average voltage on the comparator input is kept at zero. When no input is applied, the number of positive and negative pulses must be equal. When an input signal is applied, the difference in the symmetrical positive and negative pulses is proportional to the analog signal. This circuit configuration has made a great impact on low-speed precision instrumentation because of its stability, linearity and accuracy. Due to the fact that the time constant of integration of the  $D\Sigma M$  is large, its direct implementation as a continuous time integrator in monolithic form is very difficult. To avoid this problem, Kondoh et al. proposed to use switched-capacitor techniques in dual-slope analog-to-digital converters [1], [2]. We will use similar charge-capacitor strategy to implement a  $D\Sigma M$ .

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## CHARGE BALANCING INCREMENTAL MODULATOR CIRCUIT DESCRIPTION

Fig. 2a shows the circuit diagram of the switched capacitor A/D converter. The operation controlled by the nonoverlapping two phase clocks CL and CL. Switch CLr is used to discharge  $C_2$  in the beginning of conversion period when the modulator is used as an A/D converter. MOS switches are used.  $V_x$  is an analog input signal to be converted into positive-negative pulse train with reference voltage  $V_r$ . Capacitors  $C_2$  and  $C_1$  act as noninverting integrators controlled with the switches. Capacitor  $C_r$  is charged depending on the present value of the output of the integrator which is:

$$V_i(nT) = V_i(nT - T) + C_1/C_2 * V_x + (C_r/C_2) * V_r$$

The offset free and parasitic-insensitive configuration for the integrator is adopted. The simplified block diagram of this A/D converter is shown in Fig. 3. Positive and negative pulses are processed in a  $2^n$  up/down counter. For DC or quasi DC signals, the modulator generates a repetitive pulse pattern. The counter is allowed to count during N periods of the clock. If there are n1 up pulses and n2 down pulses, it is shown in [3] that

$$(n1 - n2) / (n1 + n2) \leq (V_x/V_r) \leq (n1 + 1 - n2) / (n1 + 1 + n2)$$

Above formula is valid if  $C_1 = C_r$ . Total number of the pulses during conversion period is

$$N = n1 + n2$$

Thus conversion speed is  $f_c/N$ , where  $f_c$  is clock frequency and resolution is N. For positive values of  $V_x$ , the conversion counter contains  $n=n1-n2$  pulses. Thus

$$V_x = (n/N) V_r (*)$$

The transfer characteristic of DΣM in Fig. 2b is presented. It is evident that conversion accuracy is dependent on the sampling frequency and length of averager (such as the length of the counter in Fig. 3).

Circuit level implementation of DΣM was carried out using CMOS technology and is shown in Fig. 4. The transient behavior of the circuit was simulated using SPICE simulation program. To achieve the level of simulation accuracy desired, the circuit was simulated in different functional pieces. Fig. 5 shows the transient behavior of the switched-capacitor integrator, which performs the initial processing. As can be seen, the

circuit performs a clocked integration (i.e. integrates and dumps). The ratio of  $C_1/C_2$  determines the time constant. The output of this integrator was fed to a counter using a comparator with hysteresis.

## CONVERSION ACCURACY

The switched capacitor integrator is configured such that the offset voltage of the Op.Amp. and parasitic capacitance have no effect upon its operations. Also the finite open loop gain does not disturb the charge balance. This is the effect of the holding capacitor  $C_3$  in the integrator. The main error source which limits the resolution is the feed through of clock signals through the parasitic capacitors of MOS switches. In an IC realization using advanced MOS technology, the signal to noise charge ratio ( $C_1 V_x / Q_f$ ) as high as  $5 \times 10^4$  can be obtained.

## APPLICATIONS

Besides the application of A/D converter as a digital voltmeter, it can be applied to a wide range of applications which require measuring voltages. When some degree of processing is required to derive the measurement parameter, for example, in a resistance measuring circuit, an analog circuit can be made to produce a proportional voltage. We show a simple example in Fig. 6, that

$$V_{in} = (R_1/R_2) * (R_x/R_r) V_{ref}$$

Therefore, using (\*), we have

$$n = N(R_1/R_2) (R_x/R_r).$$

$R_r$  is a ranging resistor and knowing  $N_1$ ,  $R_1$ ,  $R_2$ ,  $C_1$  and  $C_n$ , the desired scaling can be obtained. This pre-processing of the analog signals is common in low cost instrumentation systems. The accuracy is limited by the component accuracy and the analog network can be unstable. Higher performance systems may choose to digitize the primary analog quantities directly and use digital signal processing to derive the required results. In the resistance measurement example of Fig. 4, such an approach would measure the quantities  $V_A$ ,  $V_B$ , and  $V_C$  and perform the operations  $(V_B - V_C)/(V_A - V_B)$  digitally.

We propose an intermediate solution: Linear operations on the primary analog quantities after conversion to the pulse density format, but before the data are assembled into a binary weighted digital word.

Using arithmetic operations on ordinary LDM signals, it is possible to show that arithmetic operations on DΣM signals are also possible. Fig. 7a shows the case of addition

of analog signals  $x(t)$  and  $y(t)$  using delta full adder [4]. It is possible to conclude that after demodulation, sum of the two analog signals is obtained. It is also possible to conclude from Fig. 7b that this signal is attenuated by factor  $1/2$  [4]. This problem of attenuation is possible to overcome using techniques of averaging [5]. Using delta full adder, it is possible to show the influence of  $V_{ref}$  instability on the accuracy of conversion. Referring to Fig. 8a, it can be seen that when  $V_{ref1} = V_{ref2}$ ,  $X_n = Y_n$ , then  $S_n = 1/2 (X_n - Y_n) = 0$ . If  $Y_{ref2}$  has some additional fluctuation, it is possible to show that it has some DC offset. Fig. 8b shows this offset for a short period of averaging. Larger periods will smooth the oscillation. Using arithmetic operations on D $\Sigma$ M pulse stream it is possible to construct many useful options which can be implemented in various instruments.

## CONCLUSION

A method of one bit analog-to-digital conversion utilizing a switch-capacitor technique is described. This technique allows us to use monolithic IC realization. High tolerance of component is not required. On the basis of our simulation results and preliminary laboratory testing, we expect a conversion accuracy higher than 15 bits.

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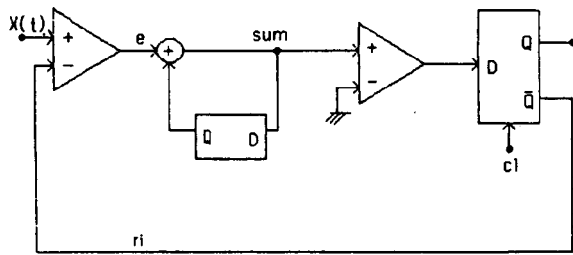


FIG. 1a

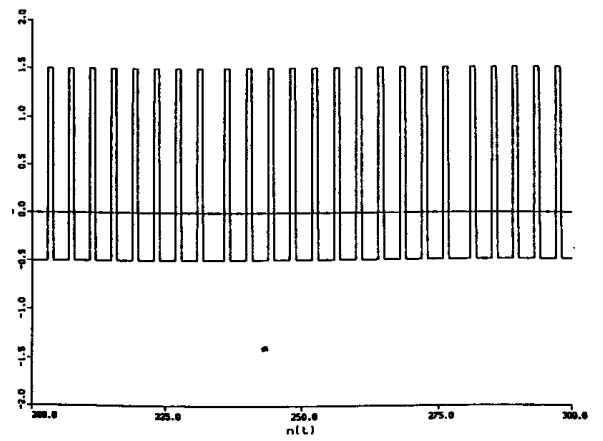


FIG. 1b

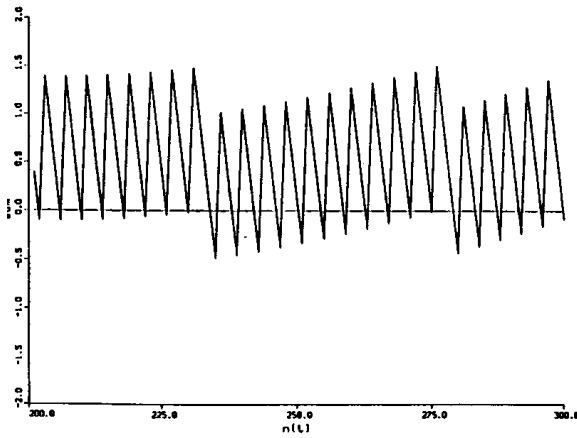


FIG. 1c

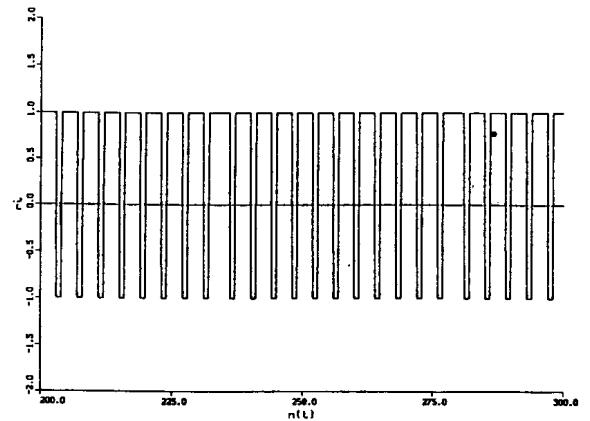


FIG. 1d

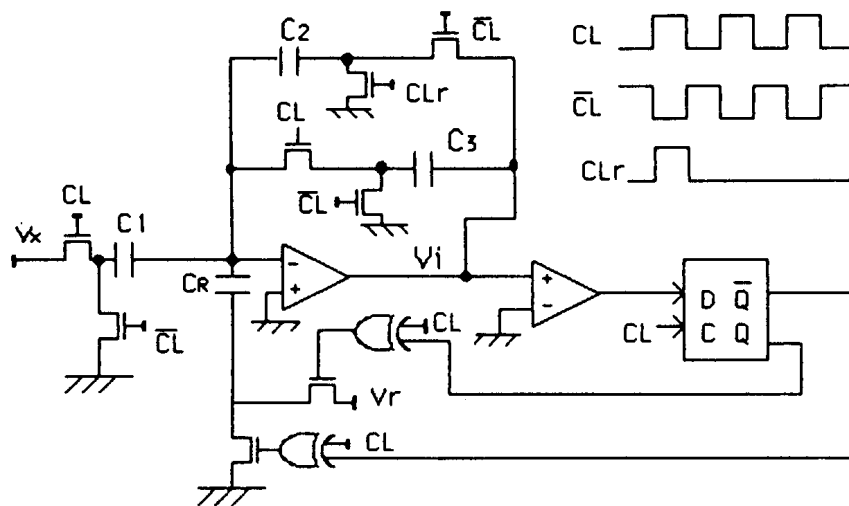


FIG. 2a

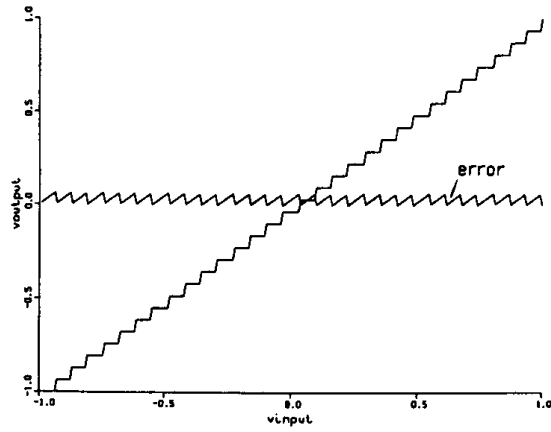


FIG. 2b

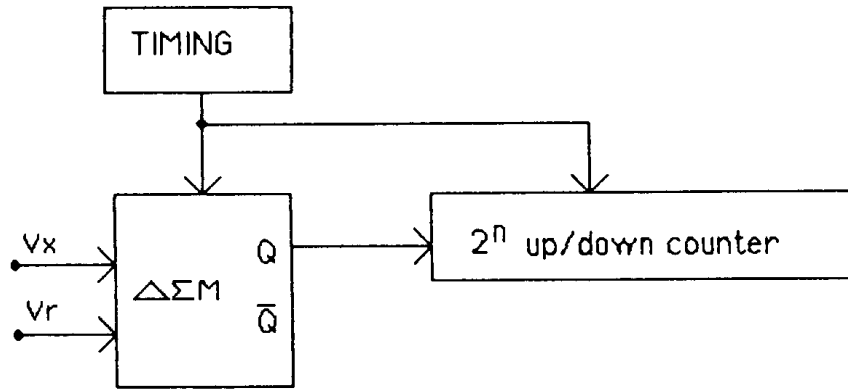


FIG. 3

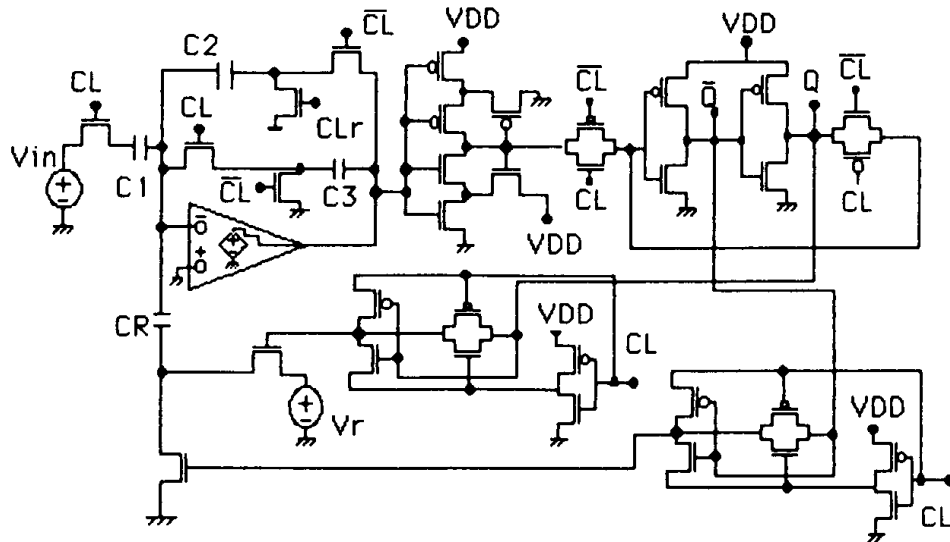


FIG. 4

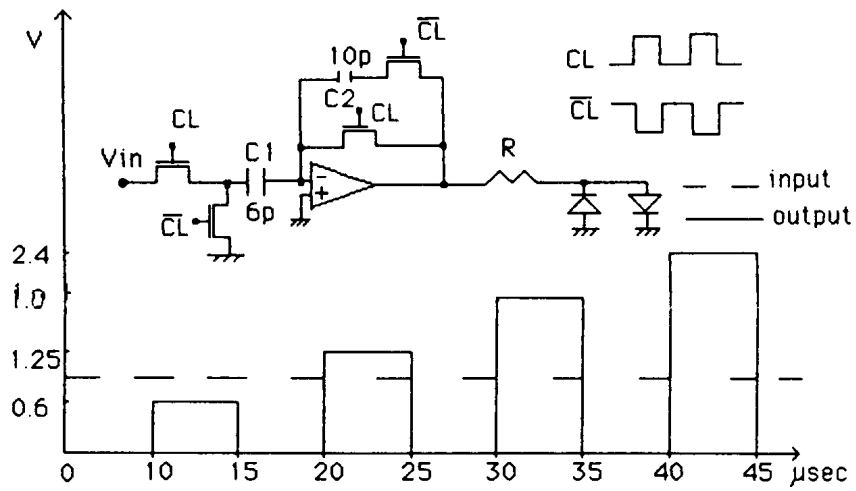


FIG 5

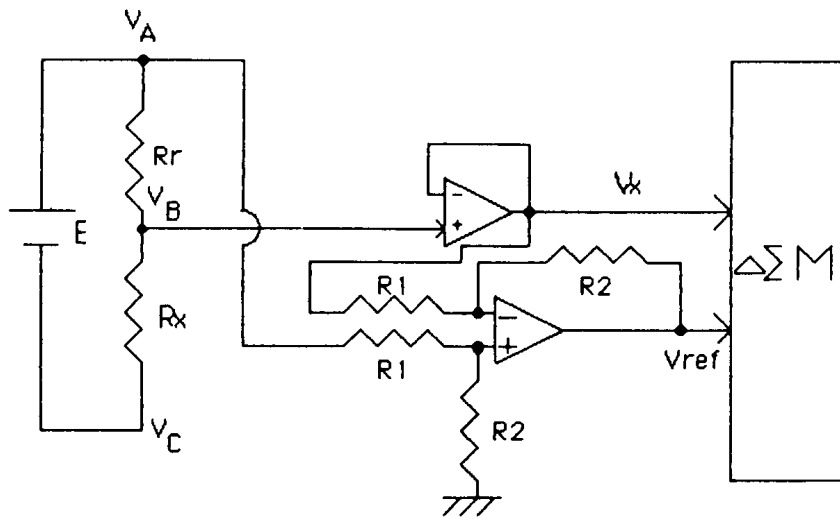


FIG. 6

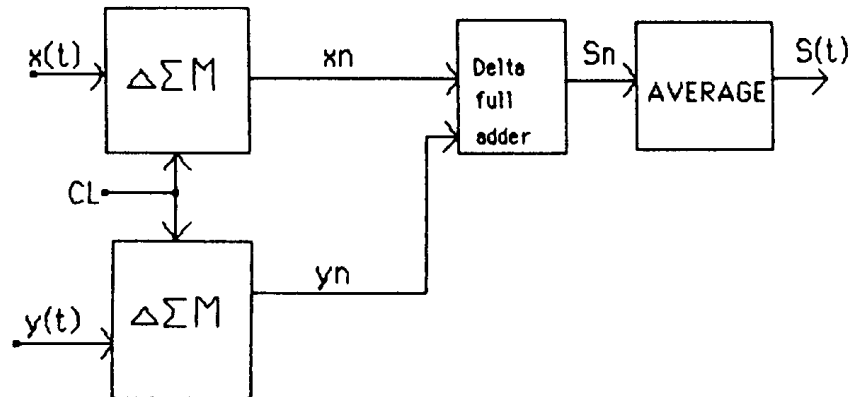


FIG. 7a

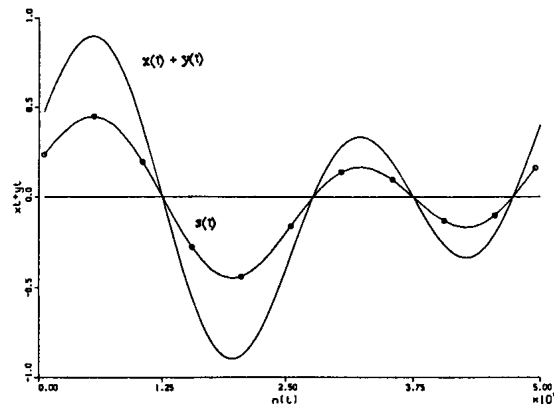


FIG 7b

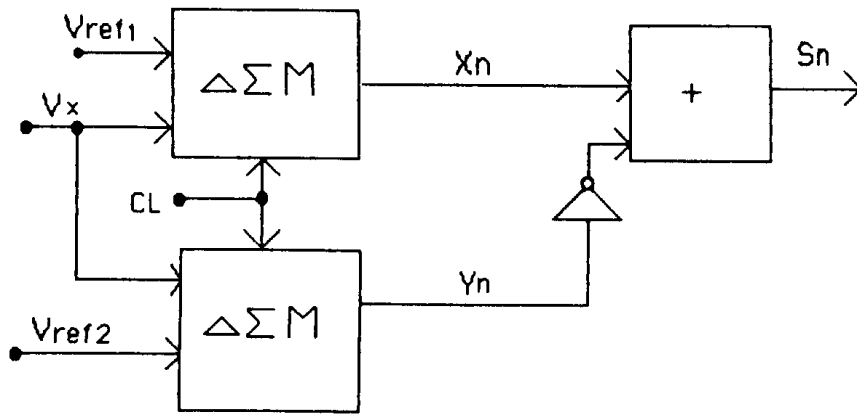


FIG 8a

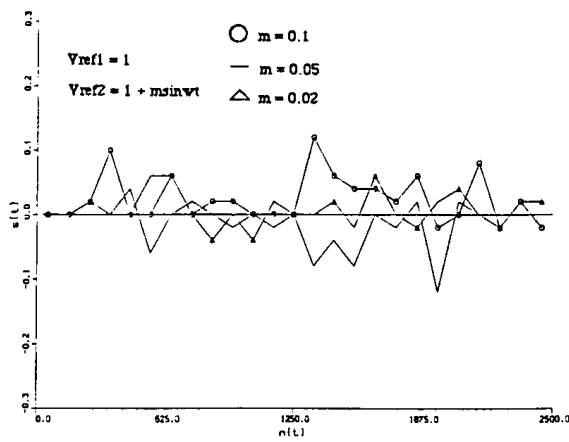


FIG. 8b