

1 Title: Reactive Responses of the Arms Increase the Margins of Stability and Decrease Center of
2 Mass Dynamics During a Slip Perturbation

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Abstract

Although reactive arm motions are important in recovering from a slip event, the biomechanical influences of upper extremity motions during slipping are not clear. The purpose of the current study was to determine whether reactive arm motions during slip recovery leads to increased margins of stability (MoS), and decreased center of mass (CoM) velocity and excursion. Thirty-two participants were randomized into 2 conditions: arms free and arms constrained. Participants traversed a 10-meter walkway and were exposed to an unexpected slip while wearing a protective harness. Anterior-posterior and medial-lateral MoS, as well as the CoM excursion and velocity during the slip perturbation was quantified using a three-dimensional motion capture system. In the frontal plane, individuals with their arms unconstrained demonstrated greater MoS (0.06 ± 0.03 vs -0.01 ± 0.02 m, $p = 0.003$), decreased CoM excursion (0.05 ± 0.02 vs 0.08 ± 0.01 m, $p = 0.016$), and a reduced CoM velocity (0.07 ± 0.03 vs. 0.14 ± 0.02 m/s, $p = 0.002$) compared to individuals with their arms constrained. In the sagittal plane, individuals with their arms unconstrained demonstrated, decreased CoM excursion (0.83 ± 0.13 vs 1.14 ± 0.20 m, $p = 0.001$) reduced CoM velocity (1.71 ± 0.08 vs. 1.79 ± 0.07 m/s, $p = 0.027$), but no differences in margins of stability (0.89 ± 0.13 vs 0.94 ± 0.10 m, $p = 0.32$). Our findings demonstrate that arm motions during a slip perturbation act to restore balance by minimizing displacement and velocity of the body CoM during a slip event in the frontal plane.

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Introduction

67 Successful recovery from a slip event involves coordinated corrective responses of the
68 upper and lower extremities (Cham and Redfern, 2001; Marigold et al., 2003). With respect to the
69 upper extremities, previous research has shown that the arms exhibit bilateral flexion in the sagittal
70 plane (Marigold et al., 2003; Merrill et al., 2017; Troy et al., 2009) and abduction of the arm
71 contralateral to the slipping foot (Lee-Confer et al., 2022a). Furthermore, Lee-Confer and others
72 (2022b) revealed that the reactive motion of the arm contralateral to the slipping foot is most
73 important in regaining balance once a slip has been initiated.

74 Although reactive arm motions are important in recovering from a slip event, the
75 underlying biomechanical mechanisms are not entirely clear. With respect to sagittal plane motions
76 during slipping, the arms have been postulated to shift the center of mass anteriorly to counter a
77 backwards loss of balance induced from a slip perturbation (Marigold et al., 2003). In addition,
78 sagittal plane arm motions during slipping have been shown to reduce the trunk extension velocity
79 (Troy et al., 2009). In contrast to sagittal plane arm motions during slipping, little is known about
80 how frontal plane arm motions aid in recovery from a slip. This is important given that the largest
81 arm motion during slipping occurs in the frontal plane of the arm contralateral to the slipping foot
82 (Lee-Confer et al., 2022a).

83 One construct that can be used to understand how arm responses aid in the recovery of a
84 slip event is the Margin of Stability (MoS). The MoS represents the dynamic relationship between
85 the body center of mass (CoM) and the base of support in the medio-lateral and antero-posterior
86 directions (Golyski et al., 2022; Hof et al., 2005; Watson et al., 2021; Young et al., 2012). When
87 a slip occurs during walking, the body CoM is posterior and medial to the slipping foot and anterior
88 and medial to the trailing foot. During a slip, the CoM shifts posteriorly and laterally with respect

89 to the leading limb, reducing the MoS and increasing the risk of losing balance. To limit the
90 reduction in the MoS and improve the chance of recovery, the excursion and velocity of the body
91 CoM needs to be reduced in the posterior and lateral directions. Since the arms represent
92 approximately 10% of the total body mass (Winter, 2009), reactive motions during a slip incident
93 could act to increase the MoS by reducing CoM excursion and velocity in both the sagittal and
94 frontal planes.

95 Using the MoS construct, the purpose of the current study was to determine how use of the
96 arms aids in the recovery of balance during a slip event. To accomplish the aim, we compared
97 MoS, CoM velocity and CoM excursion between persons who slipped with the arms unconstrained
98 and with the arms constrained. It was hypothesized that the individuals with their arms free would
99 demonstrate significantly greater MoS, and significantly less peak CoM velocity and excursion in
100 both the frontal and sagittal planes compared to the individuals with their arms constrained.

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102 Methods

103 *Participants*

104 Thirty-two healthy individuals between the ages of 21 and 35 participated in this study (13
105 males and 19 females). Prior to participation, volunteers were informed of the nature of the study,
106 and signed a written informed consent form approved by the University of Southern California
107 Health Science Campus Institutional Review Board. After providing informed consent,
108 participants completed a medical questionnaire to screen for possible conditions that could
109 jeopardize their safety by participating in this study. Specifically, individuals were excluded from
110 participation if they reported any of the following: neurological or orthopedic conditions that

111 would affect gait, current muscle strains or joint sprains, recent bone fractures, previous back
112 injuries, or individuals who had the potential to be pregnant.

113 *Instrumentation*

114 All gait trials were conducted on a 10-meter walkway. A Teflon coated floor tile (California
115 Technical Plating, San Fernando, CA, US) was imbedded into the walkway, secured on top of an
116 AMTI force plate (Model OR6-6 1000, Advanced Mechanical Technology, Inc., Watertown, MA)
117 and camouflaged such that the coloring of the tile matched the non-teflon tiles. Mineral oil was
118 placed on the tile to reduce the coefficient of friction to induce slipping (see below for details).

119 Three-dimensional motion analysis was performed using an 11-camera motion analysis
120 system (Oqus 5 series, Qualisys, Gothenburg, Sweden) collecting at 150 Hz. 76 reflective markers
121 were placed over specific anatomical locations and used to quantify upper and lower extremity
122 kinematics. To prevent falls during testing, a fall-arresting body harness (Miller Model 550-64,
123 Dalloz Fall Protection, Franklin, PA, USA) secured with an 8 mm climbing rope was attached to
124 an overhead low-friction trolley. An Omega S-beam load cell (Omega Engineering Inc., Norwalk,
125 CT, US) connected the climbing rope to the trolley system and was used to measure the amount
126 of supported bodyweight during the slip perturbation trials. To control for the potential influence
127 of footwear on slip severity, participants were fitted with a pair of oxford dress shoes with a
128 standard rubber outer sole (Bates Footwear, Richmond, IN, US).

129

130 *Procedures*

131 Prior to testing, participants were fit to the adjustable fall arresting harness. The safety
132 harness was adjusted to a height where a participant's hip would not drop below 35% of their
133 height (Yang and Pai, 2011). Participants were then instrumented with a full body marker set

134 (Figure 1). Reflective spherical markers were placed on the L5S1, Xyphoid Process, and C7, and
135 bilaterally on the: second toe, fifth metatarsal head, first metatarsal head, lateral and medial
136 malleolus, lateral and medial epicondyles of the femur, greater trochanter, anterior superior iliac
137 spine, iliac crest, acromioclavicular joint, anterior and posterior glenohumeral joint, greater
138 tubercle, lateral and medial epicondyle of the humerus, radial and ulnar styloid processes, and the
139 third metacarpal head. Additionally, a headband fitted with four markers were used to track the
140 head, and marker tracking clusters were placed bilaterally on the: heel, shank, thigh, upper arm
141 and forearm.

142 Participants were randomly assigned into one of two potential arm constraint conditions:
143 both arms free ($n = 16$) or both arms bound ($n = 16$)(Table 1). Participants in the arms bound group
144 had an adjustable polypropylene strap wrapped around their thorax and upper arm, approximately
145 2-3 inches above the elbow (Fig. 2). Additionally, both wrists were securely fastened to the harness
146 through padded wrist restraints. The lighting in the laboratory was dimmed so the light
147 measurement over the Teflon surface was four foot-candles. This level of lighting ensured that the
148 participants had ample lighting to walk safely while also providing additional concealment of the
149 Teflon surface. Participants were permitted 10 practice walking trials to adjust to the harness
150 system and dimmed lighting conditions and to achieve a consistent walking speed of 1.35-1.5 m/s
151 as determined via photoelectric switch. The participants' starting location was adjusted between
152 each practice trial so their right foot would strike the concealed Teflon tile to initiate the slip.
153 Participants were unaware of the location of the Teflon tile to avoid anticipatory gait changes to a
154 potential perturbation (Heiden et al., 2006; Siegmund et al., 2006).

155 Following the practice trials, force plate data were obtained during four non-slip walking
156 trials. Between each trial, participants faced away from the walkway for one minute such that they

157 would be uncertain as to the trial in which a slip would occur. Loud music was played during
158 testing to act as an additional distraction. The mineral oil contaminate was placed on the Teflon
159 tile after obtaining the four non-slip walking trials.

160 Following the slip trial, participants were asked if they had anticipated the slip or if they
161 had seen the contaminant following the slip trial. Any anticipation or observation of the
162 contaminant resulted in the individual being excluded from the study. All participants slipped on
163 their right foot and were only exposed to one slip for the entire study.

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165 *Data Analysis*

166 Slip outcomes were classified as a fall if participants required more than 30% support of
167 their body weight after slip initiation (Yang and Pai, 2011). Only participants that recovered from
168 a slip were analyzed for this study. Kinematic data were filtered using a second order, 6 Hz, low
169 pass Butterworth filter with zero-lag compensation.

170 Utilized coefficient of friction (uCOF) was quantified for the arms free and arms bound
171 groups using ground reaction forces on the dry walking trial prior to the slip trial. uCOF was
172 calculated as the ratio of resultant horizontal forces over the vertical force. To avoid high uCOF
173 from division of small numbers, peak uCOF was determined between the first 5% and 50% of
174 stance phase for analysis.

$$175 \quad uCOF = \frac{HorizontalGRFs}{VerticalGRF} = \frac{\sqrt{(F_{anteroposterior})^2 + (F_{mediolateral})^2}}{F_{vertical}}$$

176 Fifteen body segments (head, pelvis, thorax, and bilateral feet, shank, thigh, upper arm,
177 forearm, and hand) were created through a custom designed model template using Visual 3D
178 software (Version 5, C-Motion, Inc., Germantown, MD, USA). Individual marker data, trunk
179 kinematics and whole-body CoM were exported for subsequent analysis in Matlab (Mathworks,

180 Natick, MA, USA). For all variables, the start of the analysis was defined at the time point of slip
181 initiation and the end of the analysis was defined at the time point when the trunk reached maximal
182 right trunk lean. To determine slip initiation, the integrated sum of the vertical force data during
183 the four non-slip trials were calculated and averaged. The onset of the slip was defined as the time
184 point when the integrated-sum of the vertical force during the slip trial deviated more than two
185 standard deviations from the averaged integrated-sum of the vertical force of the non-slip trials.
186 (Lee-Confer et al., 2022a). Maximal right trunk lean was selected as the final time point as
187 maximal right trunk lean would serve as the furthestmost position of the upper body in the lateral
188 direction during a slip perturbation.

189 We computed MoS in the AP and ML directions using methodology reported previously
190 (Hof et al., 2005; Sivakumaran et al., 2018). The edge of the base of support in the frontal plane
191 was defined by the right 5th metatarsal head marker. The posterior edge of the base of support in
192 the sagittal plane was defined as the left posterior heel marker as it represented the most posterior
193 position of the foot of the trailing leg. The MoS in the frontal plane was calculated by taking the
194 medio-lateral position of the right 5th metatarsal head and subtracting the medio-lateral position of
195 the extrapolated CoM (Fig. 3). The extrapolated CoM was adapted from previous research (Hof et
196 al., 2005). The extrapolated center of mass (XCoM) was calculated as follows:

$$197 \quad XCoM = x + \frac{\dot{x}}{\omega_0}$$

198 where x was the CoM position, \dot{x} was the CoM velocity and

$$199 \quad \omega_0 = \sqrt{\frac{g}{l}}$$

200 where $g = 9.81 \text{ m/s}^2$ was the gravitational constant and l was the equivalent pendulum length
201 defined in this study as the distance between the lateral heel marker to the greater trochanter on
202 the ipsilateral limb.

203 MoS in the sagittal plane was calculated by subtracting the position of the left posterior
204 heel marker from the fore-aft position of the extrapolated CoM (Fig. 3). Values nearing zero for
205 the MoS are indicative of a higher risk of falling as the extrapolated CoM is reaching the limits of
206 the base of support. We computed CoM excursion relative to the laboratory coordinate system
207 with the anterior (AP) and right (ML) assigned as positive directions (Fig. 3). Peak CoM frontal
208 plane excursion was calculated by taking the rightmost position of the CoM at maximal right trunk
209 lean and subtracting that from the medio-lateral CoM position at slip initiation. Peak CoM velocity
210 in the frontal plane was obtained from the derivative of the medio-lateral CoM position between
211 slip initiation and maximal right trunk lean (Fig. 4). Peak CoM excursion in the sagittal plane was
212 calculated by taking the greatest antero-posterior position of the CoM between slip initiation and
213 maximal right trunk lean, and subtracting that from the initial antero-posterior CoM position at the
214 time of slip initiation. Peak CoM velocity in the sagittal plane was obtained from the derivative of
215 the antero-posterior CoM position between slip initiation and maximal right trunk lean.

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217 *Statistical Analysis*

218 A Mann-Whitney nonparametric test was used to compare uCOF, minimal MoS, peak
219 CoM velocity and CoM excursion between the arms free and arms constrained groups. This
220 analysis was repeated for both the frontal and sagittal planes. Analyses were performed using SPSS
221 16.0 statistical software (SPSS, Chicago, IL, USA) and significance levels were set at $p < 0.05$.

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Results

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In the arms free group, 13 of the 16 participants recovered from the slip perturbation while only 6 of the 16 participants in the arms constrained group recovered. As such, the data below (mean \pm SD) represent a comparison of 13 individuals in the arm free group and 6 in the arm constrained group.

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The uCOF of the individuals with their arms free were not significantly different from the uCOF of the individuals with their arms bound (0.194 ± 0.027 vs. 0.193 ± 0.026 , $p = 0.92$).

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The individuals who recovered with their arms free had a significantly larger MoS in the frontal plane compared to the individuals who recovered with their arms constrained (0.06 ± 0.03 m vs. -0.01 ± 0.02 m, $p = 0.003$, Fig. 5 & Fig. 6). In contrast, there was no significant difference in the sagittal plane MoS between the arms free and arms bound groups (0.89 ± 0.13 m vs. 0.94 ± 0.10 m respectively, $p = 0.32$, Fig. 5 & Fig. 6).

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The individuals who recovered with their arms free had a significantly reduced CoM excursion in the frontal plane compared to the individuals who recovered with their arms bound (0.05 ± 0.02 m vs. 0.08 ± 0.01 m, $p = 0.016$, Fig. 7). Similarly, the CoM excursion in the sagittal plane was significantly less in the individuals who recovered with their arms free compared to those who recovered with the arms bound (0.83 ± 0.13 m vs. 1.14 ± 0.20 m, $p = 0.001$, Fig. 7). Compared to individuals who recovered with the arms bound, those who recovered with their arms free had a significantly reduced CoM velocity in the frontal plane (0.07 ± 0.03 m/s vs. 0.14 ± 0.02 m/s, $p = 0.002$, Fig. 8) and sagittal plane (1.71 ± 0.08 m/s vs. 1.79 ± 0.07 m/s, $p = 0.027$, Fig. 8).

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Discussion

245 The purpose of the current study was to quantify the biomechanical contributions of the
246 upper extremities in regaining balance during a slip perturbation. In partial support of our
247 hypothesis, the individuals who recovered with their arms free demonstrated a significantly
248 increased MoS than those with their arms constrained. This difference however only was observed
249 in the frontal plane. Increased MoS in the frontal plane in the arms free group was achieved by
250 limiting CoM velocity and excursion.

251 The findings of our study suggest that arm motions are useful for controlling the
252 displacement of the CoM in the frontal plane. This finding is consistent with previous research
253 from our group that found the contralateral arm to the slipping foot exhibited significantly more
254 motion in the frontal plane (abduction) compared to the sagittal plane (flexion) (Lee-Confer et al.,
255 2022a) Additionally, our findings are consistent with studies that have shown that contralateral
256 arm abduction reduces the CoM excursion in individuals subjected to moving platform
257 perturbations (Grin et al., 2007). The greater MoS observed in the individuals who recovered with
258 their arms free was the result of a significantly lower CoM velocity and lower CoM excursion in
259 the medio-lateral direction. On average, these values were about half that of the arm constrained
260 group. Our data suggest that frontal plane motion of the upper extremities is acting to reduce the
261 CoM excursion and the CoM velocity.

262 The potential influence of frontal plane arm motion on the MoS can be visualized in Figure
263 8. As the individual slips on their right foot (with both arms free), the body begins to rotate towards
264 the right (right trunk lean in the frontal plane). The right lateral flexion of the trunk observed in
265 Figure 9 is similar to what is described in other research that reports lateral disturbances during a

266 slip incident (Allin et al., 2018; Rasmussen and Hunt, 2021; Smeesters et al., 2001). To counter
267 the CoM excursion, it is possible that abduction of the contralateral arm to the slipping foot (left
268 arm) would have the effect of minimizing CoM velocity and excursion to the right. This is aligned
269 with the idea that the arms may assist in changing the orientation of the body into a position that
270 reduces the likelihood of losing balance (Van Leeuwen et al., n.d.).

271 Interestingly, there were no significant differences in the MoS between the arms free and
272 arms bound group within the sagittal plane. This suggests that the ability to recover from a slip
273 event is more dependent on the ability to maintain balance in the frontal plane. In previous studies,
274 the arms were reported to perform bilateral flexion during a slip perturbation (Marigold et al.,
275 2003; Troy et al., 2009). It was proposed that the bilateral flexion response acted to shift the CoM
276 anteriorly in response to a slip perturbation and this premise was supported by the results of the
277 current study. Given that reactive arm flexion in the sagittal plane have been reported to be about
278 one-third of the motion in the frontal plane, (Lee-Confer et al., 2022a) suggests that the magnitude
279 of motion was not sufficient to lower the MoS.

280 Despite the finding of no significant difference in MoS in the sagittal plane, center of mass
281 excursion and the CoM velocity was significantly lower in individuals who recovered with their
282 arms free compared to those with their arms constrained. This finding is counter intuitive as a
283 lower CoM excursion and lower CoM velocity would be expected to contribute to a reduced MoS
284 as the center of mass would be further posterior and closer to the BoS. However, when interpreting
285 the results of the sagittal plane MoS, the position of the trail foot (i.e. base of support) needs to be
286 considered. It is possible that the individuals with their arms constrained compensated by shifted
287 their trailing foot (the non-perturbed foot) further anterior, as to reposition the base of the support
288 under the center of mass.

289 The current study highlights the importance of arm motions in the recovery of balance
290 during a slip perturbation. This was illustrated by the fact that a greater percentage of participants
291 fell when the arms were constrained compared to the arms free group (62.5% vs. 18%,
292 respectively) during the slip perturbation (Lee-Confer et al., 2022b). The increases in fall rates
293 observed in the arms constrained group cannot be due to increased challenges from an arm
294 constrain condition as uCOF was the same between groups during dry walking trials. The uCOF
295 represents the overall distributions of forces, influenced by kinematics, to affect slip severity and
296 both groups exhibited similar uCOF. Furthermore, the arms are reported to reduce the angular
297 momentum during a slip perturbation in the sagittal plane (Nazifi et al., 2020) and it is likely the
298 arms have a similar effect in the frontal plane. The clinical implications of our findings are readily
299 apparent as many fall prevention programs focus primarily on lower extremity strengthening and
300 balance training (Karinkanta et al., 2010). However, a recent study demonstrated that upper
301 extremity responses may be trained to exhibit shorter reaction times (Arnold et al., 2022). To date,
302 no studies have investigated the efficacy of interventions that focus on strengthening/reactive
303 training of the upper extremities. It is possible that upper extremity training could lead to a decrease
304 in fall risk if individuals are able to effectively utilize the mechanical benefits of arm motions
305 during a slip perturbation.

306 A potential limitation of any laboratory-based slip study is the potential for anticipatory
307 gait changes that may influence slip outcome. It has been established that individuals change their
308 gait patterns and walk more “safely” when they are aware that they may encounter a perturbation
309 (Heiden et al., 2006). A more protective gait could impact the results reported above and may not
310 reflect the true arm responses or fall frequencies that might be observed if the slip perturbation
311 occurred naturally in the environment (ie. wet floor, etc.). Another potential limitation to this study

312 is the age of our study participants. This study only included younger and healthy adults, and as
313 such, our results cannot be generalized to other populations who may be a higher risk of falling
314 (i.e. older adults).

315

316 Summary

317 Upper extremity responses during a slip response significantly increase the MoS and
318 reduce the CoM velocity and excursion, but only in the frontal plane. Within the sagittal plane,
319 reduced CoM excursion and velocity was evident in the arms free group and was not sufficient to
320 alter the MoS. The arm motions observed during a slip, particularly in the frontal plane, result in
321 individuals reducing their likelihood of falling by modulating center of mass kinematics. This
322 finding provides a more comprehensive view of the role of the upper extremities in recovering
323 from a slip perturbation while walking.

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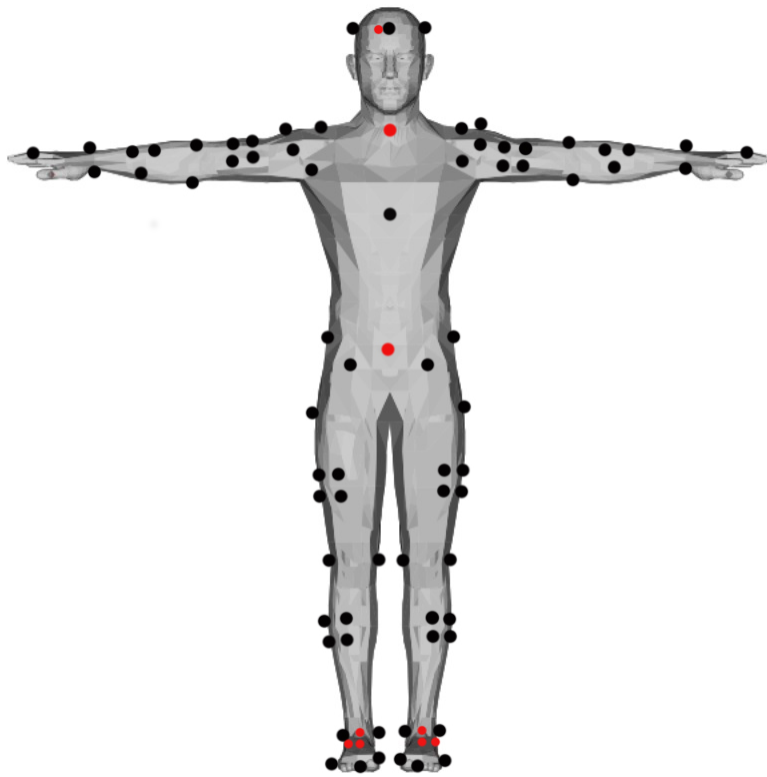
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Table 1. Participant characteristics for the two arm constraint conditions.

	Arms Constrained (N=16)	Arms Free (N=16)	P=value
Age (years)	26.1 ± 2.7	25.2 ± 1.2	p = 0.23
Height (m)	1.67 ± 0.1	1.72 ± 0.1	p = 0.16
Weight (kg)	65.5 ± 11.7	66.2 ± 9.8	p = 0.86
Shoe Size (EU)	41.9 ± 2.4	41.7 ± 1.5	p = 0.78
Sex (M/F)	6/10	6/10	p = 0.99

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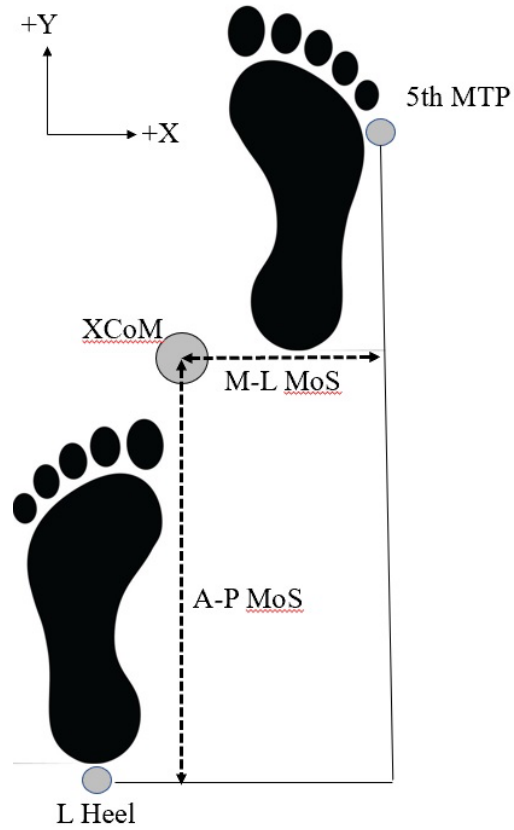
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Figure 1. A schematic of the full-body marker set. Black markers indicate markers visible from an anterior view. Red markers indicate markers on the posterior side of the body.



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Figure 2. Arm constraint positioning used in the current study with both arms constrained (left) and no arms constrained (right).

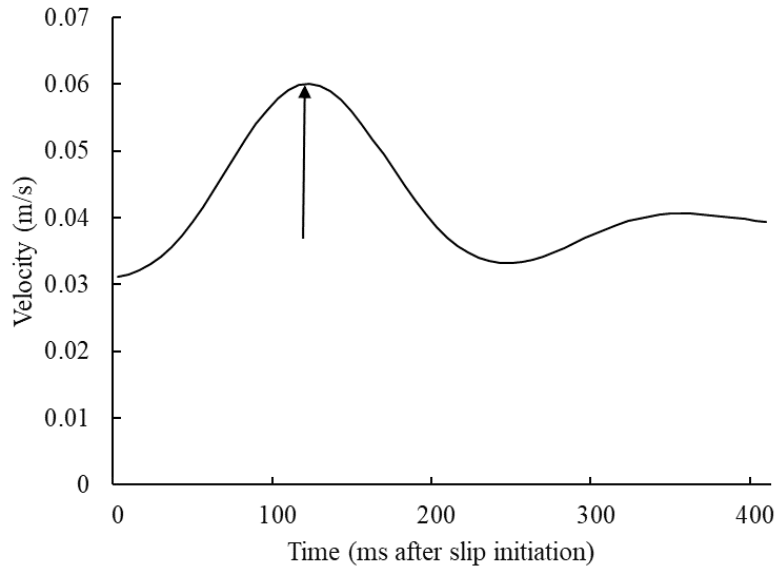


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Figure 3. Schematic illustrating the M-L and A-P Margins of Stability (MoS) calculation.

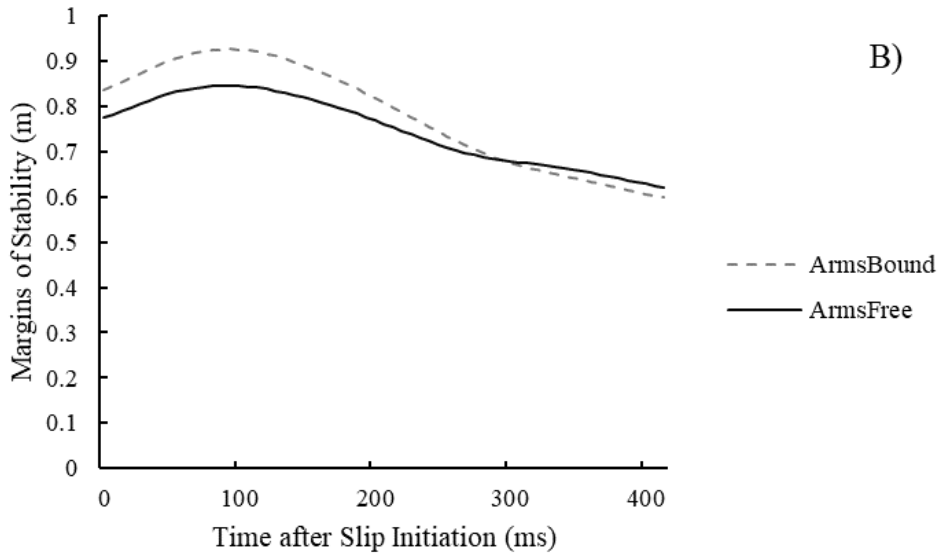
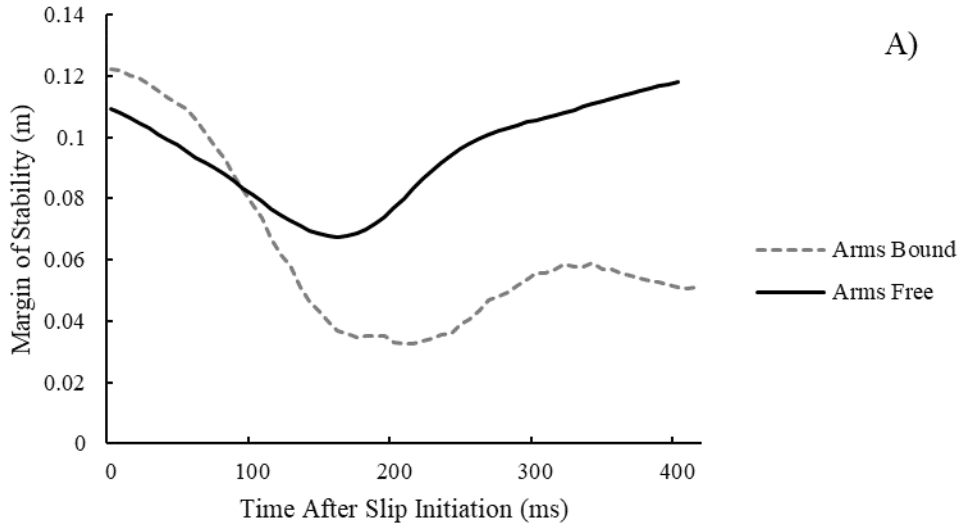
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Figure 4. Center of mass velocity of a representative slip trial from a single participant. The black arrow indicates the peak center of mass velocity.



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517 Figure 5. A) Time series data for the Margins of Stability (m) for the arms free (n = 13) and the
518 arms bound (n = 6) condition in the frontal plane. B) Time series data for the Margins of Stability
519 (m) for the arms free (n = 13) and the arms bound (n = 6) condition in the sagittal plane. The solid
520 black line represents the average Margin of Stability for the individuals with their arms free. The
521 dashed gray line represents the average Margin of Stability for individuals with their arms
522 constrained.
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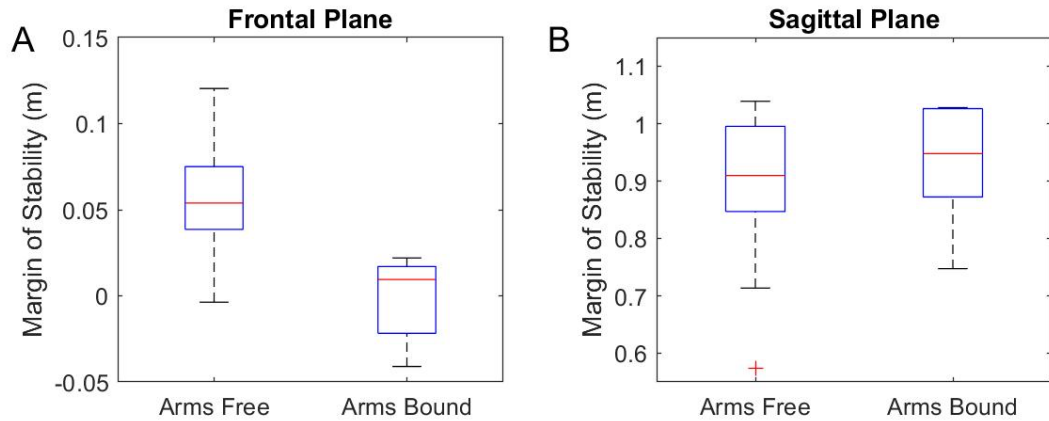
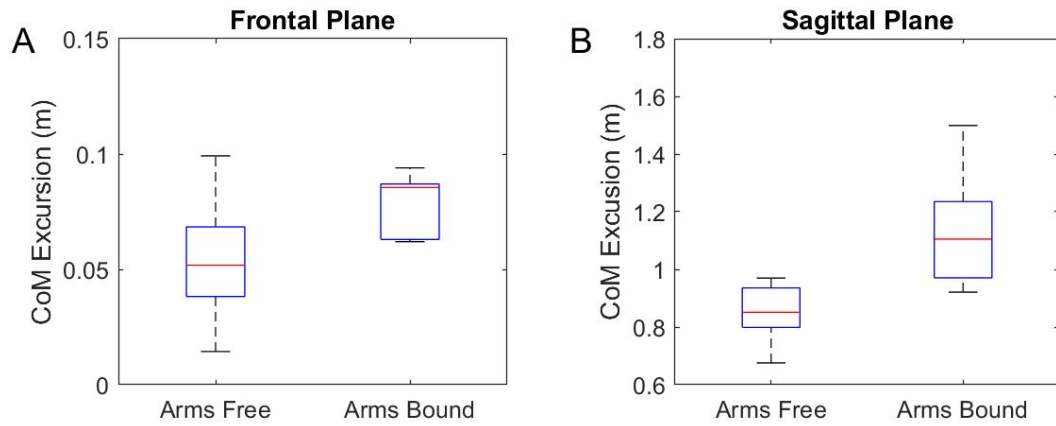


Figure 6. Margins of Stability between the arms free (n = 13) and arms bound (n = 6) groups in the frontal (A) and sagittal (B) plane. The arms free condition exhibited a larger Margin of Stability in the frontal plane indicating an increase safety margin compared to the arms bound group. No differences were found in the sagittal plane. + denotes outlier. For both box plots, the horizontal red line indicates the median, the horizontal black lines indicate maximum and minimum values, and the horizontal portions of the blue box define the interquartile range.

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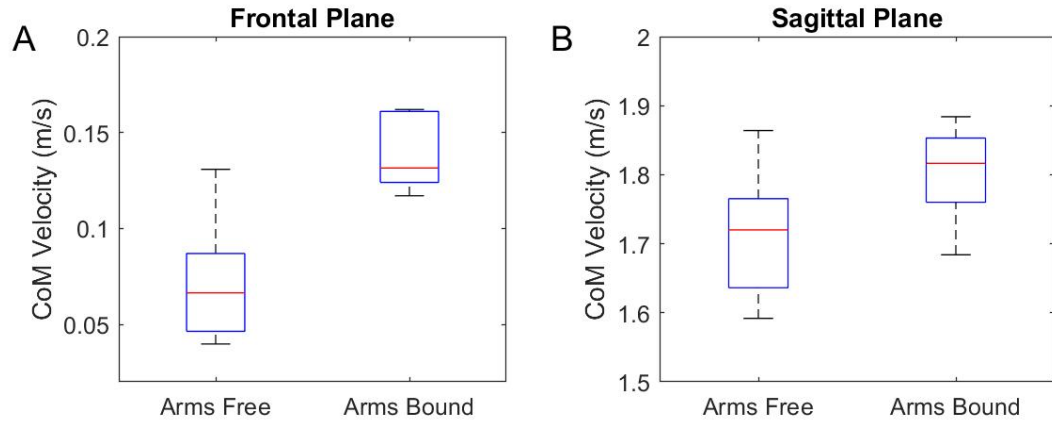
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567 Figure 7. Whole-body center of mass excursion between the arms free (n = 13) and arms
568 bound (n = 6) groups in the frontal (A) and sagittal (B) plane. The arms free group
569 exhibited significantly reduced center of mass excursions in the frontal and sagittal plane
570 compared to the arms bound group. For both box plots, the horizontal red line indicates
571 the median, the horizontal black lines indicate maximum and minimum values, and the
572 horizontal portions of the blue box define the interquartile range.
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600 Figure 8. Whole-body center of mass velocity between the arms free (n = 13) and arms
601 bound (n = 6) groups in the frontal (A) and sagittal (B) plane. The arms free group exhibited
602 significantly lower center of mass velocity directed in the ML and AP directions compared
603 to the arms bound group. For both box plots, the horizontal red line indicates the median,
604 the horizontal black lines indicate maximum and minimum values, and the horizontal
605 portions of the blue box define the interquartile range.
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623 Figure 9. An example of a participant experiencing a slip. As the slip is initiated, the body, thus
624 the center of mass, shifts towards the perturbed foot (white solid arrow). The contralateral arm to
625 the slipping foot actively performs abduction which opposes the lateral-directed center of mass
626 (white dashed arrow) to effectively reduce center of mass excursion and velocity during a slip.

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